

# Turbulent disruption of density staircases in stratified shear flows

Nicolaos Petropoulos<sup>1,†</sup>, Ali Mashayek<sup>2</sup> and Colm-cille P. Caulfield<sup>1,3</sup>

<sup>1</sup>Department of Applied Mathematics and Theoretical Physics, University of Cambridge, Cambridge CB3 0WA, UK

<sup>2</sup>Department of Earth Sciences, University of Cambridge, Cambridge CB2 3EQ, UK

<sup>3</sup>Institute for Energy and Environmental Flows, University of Cambridge, Cambridge CB3 0EZ, UK

(Received 19 July 2022; revised 30 January 2023; accepted 17 March 2023)

The formation of step-like ‘density staircase’ distributions induced by stratification and turbulence has been widely studied, and can be explained by the ‘instability’ of a sufficiently strongly stably stratified turbulent flow due to the decrease of the turbulent density flux with increasing stratification via the ‘Phillips mechanism’ (Phillips, *Deep Sea Research and Oceanographic Abstracts*, vol. 19, 1972, pp. 79–81. Elsevier). However, such density staircases are not often observed in ocean interiors, except in regions where double-diffusion processes are important, leading to thermohaline staircases. Using reduced-order models for the evolution of velocity and density gradients, we analyse staircase formation in stratified and sheared turbulent flows. Under the assumption of inertial scaling  $\epsilon \sim U^3/L$  for the kinetic energy dissipation rate  $\epsilon$ , where  $U$  and  $L$  are characteristic velocity and length scales, we determine ranges of bulk Richardson numbers  $Ri_b$  and turbulent Prandtl numbers  $Pr_T$  for which staircases can potentially form and show that the Phillips mechanism only survives in the limit of sufficiently small turbulent Prandtl numbers. For relevant oceanic parameters, a range of turbulent Prandtl numbers above which the system is not prone to staircases is found to be  $Pr_T \simeq 0.5\text{--}0.8$ . Since several studies indicate that the turbulent Prandtl number in stably stratified turbulence and in ocean interiors is usually above this threshold, this result supports the empirical observation that staircases are not favoured in ocean interiors in the presence of relatively homogeneous and sustained turbulence. We also show that our analysis is robust to other scalings for  $\epsilon$  (such as the more strongly stratified scaling  $\epsilon \sim U^2 N_c$ , where  $N_c$  is a characteristic value of the buoyancy frequency), supporting our results in both shear-dominated and buoyancy-dominated turbulent regimes as well as in weakly and strongly stratified regimes.

† Email address for correspondence: [np546@cam.ac.uk](mailto:np546@cam.ac.uk)

© The Author(s), 2023. Published by Cambridge University Press. This is an Open Access article, distributed under the terms of the Creative Commons Attribution licence (<http://creativecommons.org/licenses/by/4.0>), which permits unrestricted re-use, distribution and reproduction, provided the original article is properly cited.

**Key words:** stratified flows, turbulent mixing, stratified turbulence

## 1. Introduction

The spontaneous formation of step-like ‘density staircases’ distributions – made up of a series of relatively deep and well-mixed ‘layers’ separated by relatively thin ‘interfaces’ of enhanced density gradient – induced by stratification and turbulence has been postulated and studied by many authors (Phillips 1972; Posmentier 1977) and has been observed in a number of contexts. Experimentally, density staircases form when dragging a rod or a grid through a stable salt gradient (Linden 1980; Thorpe 1982; Ruddick, McDougall & Turner 1989; Park, Whitehead & Gnanadeskian 1994) or in stratified turbulent Taylor–Couette flows (Ogletorpe, Caulfield & Woods 2013). In the oceans they have been detected in regions where double diffusion is important (in polar regions for example) and leads to the development of thermohaline staircases (Timmermans *et al.* 2008; Radko 2016). In the Arctic their presence is crucial, not least because they act as a barrier to mixing, protecting the Arctic ice from the heat input inflowing from the Atlantic ocean (Rippeth & Fine 2022). In astrophysical stratified flows density staircases could potentially form in regions with a sufficiently large molecular Prandtl number ( $O(10^{-3})$  or larger; in white dwarf interiors for example) thanks to fingering convection (Garaud *et al.* 2015). The formation of such structures is due to the interaction between small-scale turbulence and larger-scale stratification. Such turbulence is inherently anisotropic as stratification tends to inhibit vertical motions, and inhomogeneous due to the inevitable presence of sharp density interfaces.

Although stratified turbulence is thus inevitably difficult to analyse, insight has been gained using flux-gradient parameterisations. Using such models, Phillips (1972) and Posmentier (1977) reduced the dynamics of the staircase formation problem (with a single stratification agent) to the following nonlinear diffusion equation for the horizontally averaged buoyancy  $\bar{b}$ :

$$\partial_t \bar{b} = \partial_z [F(\partial_z \bar{b})]. \quad (1.1)$$

Here, importantly, the turbulent buoyancy flux  $F$  is a non-monotonic function of the buoyancy gradient (Linden 1979). Using this formulation, staircase formation can be explained by an ‘instability’ of a sufficiently strongly stably stratified turbulent flow due to the decrease of the turbulent buoyancy flux with increasing stratification, through what is now commonly referred to as the ‘Phillips mechanism’. Flux-gradient parameterisations have, however, some drawbacks. Firstly, they are antidiffusive when the flux is a decreasing function of the gradient, leading to mathematically ill-posed problems, and it is this ill-posedness that manifests itself as the ‘instability’ of the Phillips mechanism. Secondly, they are not valid at all scales and tend to break down when the size of the phenomenon of interest (the layers in our case) is of the order of magnitude or smaller than the turbulent microstructures that such models try to parameterise (Radko 2014). These issues can both be resolved using the recently developed multiscale analysis introduced by Radko (2019) in the context of thermohaline staircase formation. Carefully introducing the interplay between different scales into the flux-gradient parameterisations, this method corrects the models at small scales and generates mathematically well-posed systems. Other regularisation techniques have also been proposed. Barenblatt *et al.* (1993) used a time-delayed flux-gradient model to construct a mathematically well-posed model of mixing in stratified turbulent flows, whereas Balmforth, Llewellyn Smith & Young (1998)

considered the evolution of both buoyancy gradients and turbulent kinetic energy to analyse staircase dynamics in stratified turbulent flows.

The above reduced-order model predicts staircase formation for sufficiently strongly stratified flows. Furthermore, Billant & Chomaz (2001) identified a strongly stratified regime (in the sense that the horizontal Froude number  $Fr_h = U/L_h N_c$  is small, where  $U$  is a characteristic horizontal velocity scale,  $L_h$  is a typical horizontal length scale and  $N_c$  is a characteristic value of the buoyancy frequency) for which the (full) equations of motion are self-similar with respect to  $zN_c/U$ , suggesting a layered structure with characteristic vertical length scale  $U/N_c$ . These vertical staircases offer a route for turbulence to grow and be sustained in strongly stratified flows and, hence, mix strong density gradients. Indeed, whereas sufficiently weakly stratified flows are prone to shear instabilities that can overturn density gradients, strongly stratified flows prevent such instabilities from growing. However, they are prone to staircase formation that reduces (locally) the stratification inside the layers, creating a favourable environment for shear instabilities to develop (Cope, Garaud & Caulfield 2020). The subsequent turbulence is inevitably spatially and temporally intermittent and is characterised by scouring dynamics near the relatively sharp density interfaces rather than overturns, emphasizing the qualitatively different mixing expected in relatively weakly or strongly stratified flows (Woods *et al.* 2010; Caulfield 2021).

Oceanic flows are indeed often strongly stratified in the sense that an appropriate gradient Richardson number  $Ri$  (defined here as the square of the ratio of the background buoyancy frequency and background vertical shear) is large enough so that the Richardson number falls on the right flank of the turbulent buoyancy flux curve (Linden 1979). As an example, figure 1, reproduced from (Mashayek *et al.* 2022), shows emergence of turbulence in the otherwise quiescent ocean interior when shear (from internal waves, mesoscale instabilities or boundary processes for instance; see figure 1b) increases sufficiently for the Richardson number to drop below critical values. In the close vicinity of the top and bottom boundaries turbulence is less intermittent. Such turbulent patches in the interior, sufficiently far from the boundaries, typically correspond to buoyancy gradients on the decreasing flank of the aforementioned turbulent buoyancy flux curve. Layering should on the face of it play an important role in formation and erosion of density gradients. However, figure 1(c) shows that turbulent patches in the interior do not leave the density structure layered. This behaviour seems generic in many parts of the ocean interior, of course excluding regions where thermohaline diffusive processes (e.g. double diffusion) can play a prominent role such as in the Arctic Ocean or the Mediterranean Sea (Timmermans *et al.* 2008; Radko 2016). Crucially, the shear and its spatiotemporal variability are key to turbulent mixing, yet absent from the theoretical framework that forms the basis for the Phillips mechanism.

Motivated by these observations, in this work we analyse staircase formation (or lack thereof) in density stratified turbulence in the presence of velocity shear (e.g. the interior turbulent patches mentioned above), and assess in which regime(s) it is possible for the Phillips mechanism – defined here as the instability with respect to small perturbations of linear buoyancy profiles in a turbulent flow far from boundaries (Phillips 1972) – to survive. Using reduced-order models for the evolution of velocity and density gradients based on flux-gradient parameterisations of the turbulent fluxes (corrected using a simpler version of Radko (2019) multiscale analysis) and under various scalings for the rate of dissipation of the kinetic energy  $\epsilon$  (specifically  $\epsilon \sim U^3/L$  and  $\epsilon \sim U^2 N_c$ , where  $L$  is a characteristic length scale of our problem), we determine ranges of bulk Richardson numbers  $Ri_b$  and turbulent Prandtl numbers  $Pr_T$  (defined more precisely below, effectively

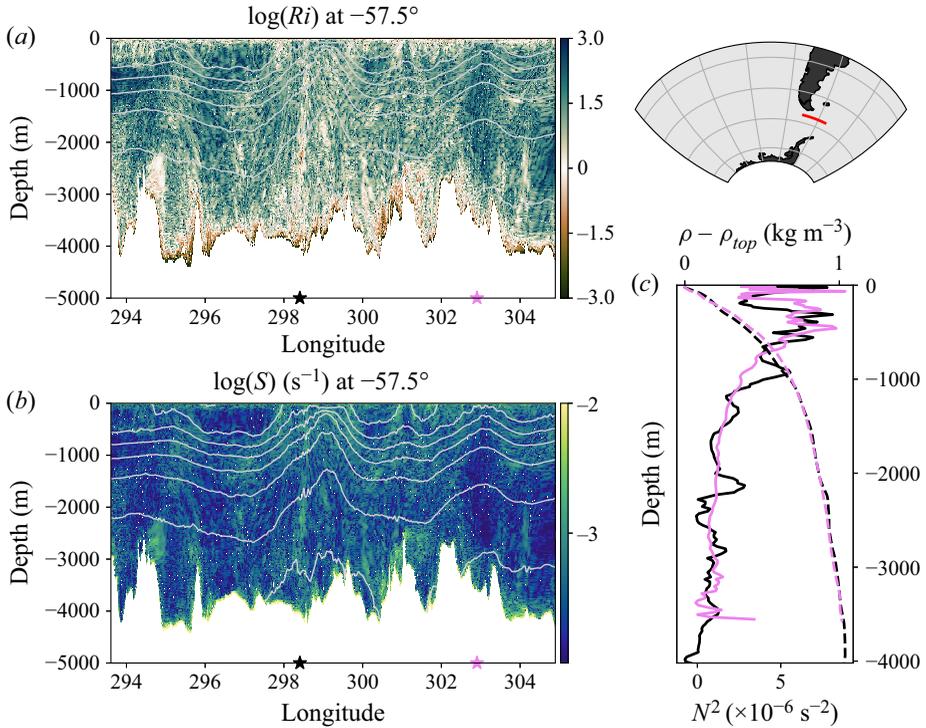


Figure 1. (a) The Richardson number on a slice in the Drake Passage of the Southern Ocean, corresponding to the red line in the inset at the top right corner. Buoyancy levels are overlaid in the form of grey lines. (b) Same as (a) but for velocity shear. (c) Density (dashed lines) and stratification (solid lines) profiles corresponding to the longitudes marked by stars in (a) and (b). Reproduced from (Mashayek *et al.* 2022).

quantifying the relative strength of velocity shear to the buoyancy frequency and the ratio of turbulent diffusivity of momentum to turbulent diffusivity of buoyancy, respectively) for which staircases can potentially form.

We demonstrate that the Phillips mechanism for staircase formation in strongly stratified flows remains viable in the presence of shear only in the limit  $Pr_T \ll 1$  but breaks down otherwise. Specifically, for sufficiently large  $Ri_b \gtrsim 1$ , there exists a limiting value of the turbulent Prandtl number  $Pr_T$  above which staircase formation via this mechanism ceases to be possible. For relevant oceanic parameters, this value is found around 0.5–0.8. Even though it is still challenging to measure the turbulent Prandtl number in the oceans, several studies of direct numerical simulation of stably stratified turbulence indicate that  $Pr_T$  is typically non-trivially above this threshold (Shih *et al.* 2005; Venayagamoorthy & Stretch 2010) and, therefore, our result supports and explains the empirical observation that staircases are not favoured in ocean interiors in the presence of relatively homogeneous and sustained turbulence driven by velocity shears.

To demonstrate this key result, the rest of the paper is organised as follows. In § 2 we introduce the theoretical model used throughout the paper to analyse staircase formation in both density (stably) stratified and sheared turbulent flows, through extending the work of Phillips (1972) and Posmentier (1977) to take into account the evolution of shear, and define relevant dimensionless parameters. In § 3 we describe the regions in the parameter space that are prone to staircase instabilities through a linear stability analysis of the governing equations. In § 4 we present some properties of the various instabilities, while

in § 5 we compare the nonlinear dynamics leading to staircase formation and the stability analyses. Finally, we draw brief conclusions in § 6.

## 2. Formulation

Except when stated otherwise, the following notations will be used throughout this work.

- (i) a star  $\cdot^*$  denotes a dimensional variable. The star is dropped for dimensionless quantities.
- (ii) An overbar  $\bar{\cdot}$  denotes an horizontally averaged quantity.
- (iii) A tilde  $\tilde{\cdot}$  denotes a deviation from a background quantity.
- (iv) A prime  $\prime$  denotes a derivative with respect to an argument (always in fact being  $Ri_b$ ).

### 2.1. Dimensional form

The Navier–Stokes equations in the Boussinesq approximation (with a background density  $\rho_0^*$ ) are

$$\left. \begin{aligned} \partial_{t^*} u^* + \mathbf{u}^* \cdot \nabla^* u^* &= \nu^* \nabla^{*2} u^* - \frac{1}{\rho_0} \partial_{x^*} p^*, & \partial_{t^*} v^* + \mathbf{u}^* \cdot \nabla^* v^* &= \nu^* \nabla^{*2} v^* - \frac{1}{\rho_0} \partial_{y^*} p^*, \\ \partial_{t^*} w^* + \mathbf{u}^* \cdot \nabla^* w^* &= \nu^* \nabla^{*2} w^* - \frac{1}{\rho_0} \partial_{z^*} p^* + b^*, & \partial_{t^*} b^* + \mathbf{u}^* \cdot \nabla^* b^* &= \kappa^* \nabla^{*2} b^*, \\ \nabla^* \cdot \mathbf{u}^* &= 0, \end{aligned} \right\} \quad (2.1)$$

where  $\mathbf{u}^* = (u^*, v^*, w^*)$  is the velocity field,  $b^* := -(g^*/\rho_0^*)\rho^*$  is buoyancy (where  $\rho^*$  is density and  $g^*$  is the gravitational acceleration),  $p^*$  is pressure and  $\kappa^*$  and  $\nu^*$  are the (molecular) diffusivity and viscosity of the fluid. The differential operators are taken with respect to dimensional quantities. Averaging in the horizontal and assuming that  $\mathbf{u}^* = (\bar{u}^*(z, t), 0, 0) + \tilde{\mathbf{u}}^*$  and  $b^* = \bar{b}^*(z, t) + \tilde{b}^*$ , where  $\bar{u}^*$  and  $\bar{b}^*$  are the horizontally averaged velocity and buoyancy profiles, respectively, we obtain

$$\left. \begin{aligned} \partial_{t^*} \bar{b}^* &= \kappa^* \partial_{z^*}^2 \bar{b}^* - \partial_{z^*} F_b^*, & F_b^* &= \overline{\tilde{b}^* \tilde{w}^*}, \\ \partial_{t^*} \bar{u}^* &= \nu^* \partial_{z^*}^2 \bar{u}^* - \partial_{z^*} F_u^*, & F_u^* &= \overline{\tilde{u}^* \tilde{w}^*}, \end{aligned} \right\} \quad (2.2)$$

where  $F_b^*$  and  $F_u^*$  are respectively the vertical buoyancy and momentum turbulent fluxes, with overbars denoting horizontal averages. Using flux-gradient models to parameterise these fluxes in terms of the mean buoyancy and velocity gradients, we obtain implicit definitions for the turbulent diffusivities of buoyancy  $\kappa_T^*$  and momentum  $\nu_T^*$ ,

$$F_b^* = -\kappa_T^* \partial_{z^*} \bar{b}^*, \quad F_u^* = -\nu_T^* \partial_{z^*} \bar{u}^*. \quad (2.3a,b)$$

Our goal is to understand how an ambient shear influences the formation of density (or equivalently buoyancy) staircases. Therefore, we choose to model these fluxes only in terms of the gradient Richardson number  $Ri_g$ , defined in terms of the background shear  $S^*$  and buoyancy frequency  $N^*$ ,

$$Ri_g := \frac{N^{*2}}{S^{*2}}; \quad S^* := \partial_{z^*} \bar{u}^*, \quad N^{*2} := \partial_{z^*} \bar{b}^*. \quad (2.4)$$

It is important to remember that common parameterisations of the turbulent diffusivities rely also on the buoyancy Reynolds number  $Re_b := \epsilon^*/\nu^* N^{*2}$ , where  $\epsilon^*$  is the dissipation

rate of turbulent kinetic energy (Shih *et al.* 2005; Bouffard & Boegman 2013; Mashayek *et al.* 2017). We can however express the buoyancy flux as

$$F_b^* = -\Gamma \epsilon^*, \tag{2.5}$$

where  $\Gamma$  is the turbulent flux coefficient (Osborn 1980) and reduce the modelling of the turbulent diffusivities  $\kappa_T^*$  and  $\nu_T^*$  to the modelling of this coefficient. Parameterisations of  $\Gamma$  in terms of  $Ri_g$  have been presented in Wells, Cenedese & Caulfield (2010) for instance. At  $Ri_g = 0$ , there is no buoyancy to mix and, therefore, it seems reasonable to assume  $\Gamma(Ri_g = 0) = 0$ . As  $Ri_g$  increases, there is more and more scalar to mix and  $\Gamma$  should therefore increase. However, as stratification becomes more significant, it is reasonable to suppose that it will suppress vertical motion because of restoring buoyancy forces, possibly leading to less efficient mixing. Whether  $\Gamma$  decreases towards 0 or saturates for  $Ri_g$  large enough is still an open question (Caulfield 2021). However, the analysis presented in the following sections depends most strongly on the monotonicity of the flux coefficient in terms of the Richardson number, and not the specific functional form of  $\Gamma(Ri_g)$  and, hence, the two cases can be studied, as we will see later.

Written in terms of the flux coefficient  $\Gamma$ , the mean buoyancy and velocity equations (2.2) are

$$\left. \begin{aligned} \partial_{t^*} N^{*2} &= \kappa^* \partial_{z^*}^2 N^{*2} + \partial_{z^*}^2 [\Gamma \epsilon^*], \\ \partial_{t^*} S^* &= \nu^* \partial_{z^*}^2 S^* + Pr_T \partial_{z^*}^2 \left[ \frac{\Gamma \epsilon^*}{S^* Ri_g} \right], \quad Pr_T := \frac{\nu_T^*}{\kappa_T^*}. \end{aligned} \right\} \tag{2.6}$$

For the sake of simplicity and because our goal is to understand how this coupling parameter affects the formation of staircases, we consider the turbulent Prandtl number  $Pr_T$  as a free constant parameter that does not depend on the stratification nor on the shear. The above equations are coupled through the dependence of the flux coefficient  $\Gamma$  on the Richardson number  $Ri_g$ . Moreover, since the system is invariant under the mapping  $S^* \rightarrow -S^*$ , we will assume without loss of generality that  $S^* \geq 0$ . Since we are considering statically stable buoyancy profiles, we also have  $N^{*2} \geq 0$ .

## 2.2. Dimensionless system

In order to scale the system (2.6) we need to make some assumptions regarding the relevant time scale of our problem as well as on the dissipation rate of turbulent kinetic energy  $\epsilon^*$ . Using data from various sources, Mater & Venayagamoorthy (2014) show that stably stratified shear-flow turbulence could be interpreted in terms of three time scales: the buoyancy time scale  $T_b^* := 1/N^*$ , the shear time scale  $T_s^* := 1/S^*$  and the turbulence time scale  $T_T^* := \mathcal{K}^*/\epsilon^*$ , where  $\mathcal{K}^*$  is the turbulent kinetic energy density. In the following, we propose three different scalings that depend on the relative size of these time scales. These scalings are summarized in figure 2.

### 2.2.1. Inertial scaling

We first propose to scale the system (2.6) under the assumption that the dissipation rate of turbulent kinetic energy  $\epsilon^*$  scales ‘inertially’ like  $U^{*3}/L^*$ , where  $U^*$  is a characteristic velocity scale and  $L^*$  is a characteristic length scale of our problem. This scaling has been justified in many experimental and observational settings (Ivey & Imberger 1991; Ivey, Imberger & Koseff 1998; Kay & Jay 2003; Shih *et al.* 2005). It is relevant, for instance, in sufficiently weakly stratified or shear-dominated turbulent flows where the

## Turbulent disruption of density staircases

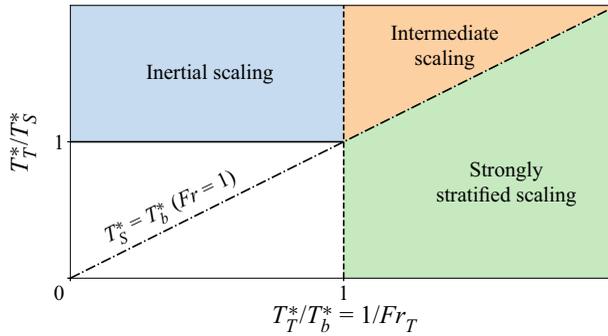


Figure 2. Scaling used depending on the relative size of  $T_b^*$  (buoyancy time scale),  $T_S^*$  (shear time scale) and  $T_T^*$  (turbulent time scale). The solid horizontal line corresponds to  $T_T^*/T_S^* = 1$ . The dashed vertical line corresponds to  $T_T^*/T_b^* = 1$ . The dash-dotted line corresponds to  $T_b^*/T_S^* = 1$ .

turbulent Froude number  $Fr_T := \epsilon^*/N^*\mathcal{K}^*(= T_b^*/T_T^*)$  as well as  $T_T^*/T_S^*$  are sufficiently large (implying  $Fr := S^*/N^*(= T_b^*/T_S^*)$  sufficiently large) (Mater & Venayagamoorthy 2014). Then, the relevant time scale of dissipation of turbulent kinetic energy is set by the shear and  $\epsilon^*$  scales inertially.

Therefore, we consider the following scaling (the star is dropped for dimensionless quantities):

$$u^* = U^*u, \quad z^* = L^*z, \quad t^* = \frac{L^*}{U^*}t, \quad S^* = \frac{U^*}{L^*}S, \quad N^{*2} = N_c^{*2}N^2, \quad \epsilon^* = \frac{U^{*3}}{L^*}\epsilon. \quad (2.7)$$

Here the relevant time scale has been set by the shear,  $N_c^*$  is a typical value of the buoyancy frequency so that  $N^2 = O(1)$  and, since we are assuming that  $\epsilon^*$  is large enough to sustain an inertial subrange and that the inertial scaling holds,  $\epsilon = O(1)$  (we will assume in the following that  $\epsilon^*$  is constant and, therefore, consider  $\epsilon = 1$  precisely; in fact, we will show in § 3.3 that the precise value of  $\epsilon$  does not affect our results). In practice,  $N_c^{*2}$  and  $U^*/L^*$  are the background stratification and shear of the disturbed profiles considered in the linear stability analysis (§ 3). System (2.6) then becomes

$$\left. \begin{aligned} \partial_t N^2 &= \frac{1}{Pr Re} \partial_{zz} N^2 + \frac{1}{Ri_b} \partial_{zz} [\Gamma(Ri_b Ri) \epsilon], \\ \partial_t S &= \frac{1}{Re} \partial_{zz} S + Pr T \partial_{zz} \left[ \frac{\Gamma(Ri_b Ri) \epsilon}{SRi_b Ri} \right], \\ Pr &:= \frac{\nu^*}{\kappa^*}, \quad Re := \frac{U^* L^*}{\nu^*}, \quad Ri_b := \frac{N_c^{*2} L^{*2}}{U^{*2}}, \end{aligned} \right\} \quad (2.8)$$

where the dependence on three dimensionless parameters (the molecular Prandtl number  $Pr$ , the Reynolds number  $Re$  and the bulk Richardson number  $Ri_b$ ) is made explicit. These two equations are coupled through the scaled gradient Richardson number  $Ri := N^2/S^2$  (always multiplied by  $Ri_b$ ). We expect staircase formation to be favoured at larger  $Pr$  (Taylor & Zhou 2017). For  $Pr = O(1)$ , we can expect density staircases to be smoothed by diffusion, at least for sufficiently small  $Re$  (i.e. sufficiently small Péclet numbers  $Pe := Pr Re$ ). Note that the different dimensionless parameters are considered as free parameters independent of each other and of the dynamical quantities. Indeed, the goal

of our study is to explore the full parameter space in order to determine regions that are prone to staircase formation but not to assess whether the entire parameter space is actually physically accessible. Indeed, constraining relationships between the different dimensionless parameters would restrict the range of accessible parameters but would not change the stability results presented here. As mentioned previously, we also assume  $\epsilon$  to be constant. Hence, we are focusing our attention on turbulent patches that are relatively homogeneous (in space) and sustained (in time). In practice, we consider  $\epsilon = 1$  but show in § 3.3 that the precise value of  $\epsilon$  does not affect our results. Hence, the ‘strength’ of the turbulence does not play a major role in our analysis, as soon as this turbulence follows one of the described scalings.

### 2.2.2. Intermediate scaling for moderately stratified flows

Instead of considering the inertial scaling introduced in the previous section, we can alternatively assume that the dissipation rate of turbulent kinetic energy  $\epsilon^*$  scales as  $U^{*2}N_c^*$  (with the notation of § 2.2.1). This scaling is relevant, for instance, to moderately or strongly stratified flows in the sense that  $Fr_T \lesssim 1$  and, therefore, the turbulent kinetic energy largely dissipates within a buoyancy time scale and, hence,  $\epsilon^* \sim U^{*2}N_c^*$  (Garaik & Venayagamoorthy 2019). Considering that the flow is moderately stratified in an intermediate flow regime, in the sense that the dominant time scale is still set by the shear (assuming, for instance, that we are still in a shear-dominated regime and so the shear time scale  $T_S^*$  is sufficiently small compared with the turbulent time scale  $T_T^*$  and the buoyancy time scale  $T_b^*$  (Mater & Venayagamoorthy 2014)), the system (2.6) becomes

$$\left. \begin{aligned} \partial_t N^2 &= \frac{1}{Pr Re} \partial_{zz} N^2 + \frac{1}{\sqrt{Ri_b}} \partial_{zz} [\Gamma(Ri_b Ri) \epsilon], \\ \partial_t S &= \frac{1}{Re} \partial_{zz} S + Pr_T \sqrt{Ri_b} \partial_{zz} \left[ \frac{\Gamma(Ri_b Ri) \epsilon}{SRi_b Ri} \right]. \end{aligned} \right\} \quad (2.9)$$

This system is equivalent to the one derived using the inertial scaling (system (2.8)) with the mapping  $\sqrt{Ri_b} \Gamma(Ri_b Ri) \rightarrow \Gamma(Ri_b Ri)$ . We will discuss the implications of this intermediate scaling below.

### 2.2.3. Strongly stratified scaling

For sufficiently strongly stratified flows, consistently with the strong stratification scaling derived by Garaik & Venayagamoorthy (2019) and the buoyancy-dominated regime analysed by Mater & Venayagamoorthy (2014) for  $Fr_T \lesssim 1$  (leading to  $\epsilon^* \sim U^{*2}N_c^*$ ), we can also assume that the time scale is set by the buoyancy (i.e.  $t^* = (1/N_c^*)t$ , assuming, for instance,  $T_b^* \ll T_S^*$ ) and obtain

$$\left. \begin{aligned} \sqrt{Ri_b} \partial_t N^2 &= \frac{1}{Pr Re} \partial_{zz} N^2 + \frac{1}{\sqrt{Ri_b}} \partial_{zz} [\Gamma(Ri_b Ri) \epsilon], \\ \sqrt{Ri_b} \partial_t S &= \frac{1}{Re} \partial_{zz} S + Pr_T \sqrt{Ri_b} \partial_{zz} \left[ \frac{\Gamma(Ri_b Ri) \epsilon}{SRi_b Ri} \right]. \end{aligned} \right\} \quad (2.10)$$

Once again this system is equivalent to system (2.8) with the mappings  $\sqrt{Ri_b} \Gamma(Ri_b Ri) \rightarrow \Gamma(Ri_b Ri)$  and  $\sqrt{Ri_b} t \rightarrow t$ , and we will also discuss the implications of this strongly stratified scaling below.

## Turbulent disruption of density staircases

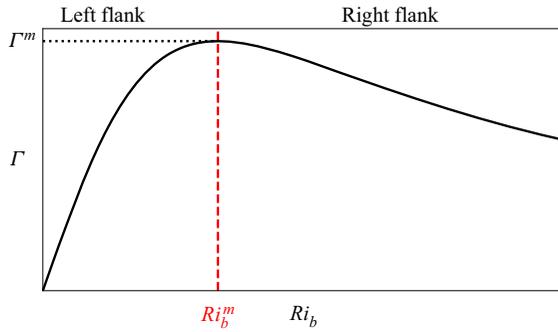


Figure 3. Schematic representation of the parameterisation of the turbulent flux coefficient  $\Gamma$  used throughout this paper. The vertical red dashed line corresponds to the bulk Richardson number that maximizes  $\Gamma$ . It separates the increasing ‘left flank’ of the  $\Gamma$  curve, where  $\Gamma$  is an increasing function of  $Ri_b$  and the decreasing ‘right flank’ where  $\Gamma$  is a decreasing function of  $Ri_b$ . The horizontal dotted line corresponds to the maximum value of  $\Gamma$  (denoted  $\Gamma^m$ ).

### 2.3. Choice of parameterisation for the flux coefficient

We must now choose a specific functional form for the parameterisation of the flux coefficient  $\Gamma$  in terms of the bulk Richardson number  $Ri_b$ . Experimental and numerical data (Turner 1968; Linden 1979; Wells *et al.* 2010) suggest that  $\Gamma$  is a non-monotonic function of  $Ri_b$  with  $\Gamma(Ri_b) \propto Ri_b$  on the increasing flank of  $\Gamma$  and  $\Gamma(Ri_b) \propto 1/Ri_b^p$  (with  $p \geq 0$ ) on the decreasing flank. These scaling regimes may be respected with the functional form

$$\Gamma(Ri_b) = A \frac{Ri_b}{1 + B Ri_b^{p+1}}, \quad (2.11)$$

where  $A$  and  $B$  are chosen so that the maximum value of  $\Gamma$ , attained when  $Ri_b = Ri_b^m \simeq 1$ , is  $\Gamma^m \simeq 0.2\text{--}0.3$  (Ivey & Imberger 1991). (As we discuss further below, the specific chosen values of  $\Gamma^m$  and  $Ri_b^m$  do not affect the qualitative results presented in this work.) Common values for  $p$  are  $p = 1/2$  and  $p = 1$  (Turner 1968; Linden 1980). A schematic representation of the parameterisation used is given in figure 3. It should be noted that in what follows we will try to present results that are as general as possible and do not depend strongly on the precise formulation (2.11) of  $\Gamma$  but only on the sign of its derivative and asymptotic rate of decrease as  $Ri_b \rightarrow \infty$ .

## 3. Marginal linear stability

### 3.1. Formulation

To investigate the conditions that can support the formation of staircases starting from linear velocity and buoyancy profiles, we linearise the system (2.8) around linear profiles of buoyancy and velocity with constant shear  $U^*/L^*$  and buoyancy frequency  $N_c^*$ . We therefore assume that the (dimensionless) shear and stratification fields can be decomposed as

$$S = 1 + \tilde{S}, \quad N^2 = 1 + \tilde{N}^2, \quad (3.1a,b)$$

where the perturbations  $\tilde{S} \ll 1$  and  $\tilde{N}^2 \ll 1$ . Then, at first order in  $\tilde{N}^2$  and  $\tilde{S}$ ,

$$Ri = \frac{1 + \tilde{N}^2}{(1 + \tilde{S})^2} = [1 + \tilde{N}^2][1 - 2\tilde{S}] = 1 + \tilde{Ri}, \quad (3.2)$$

where  $\tilde{Ri} = -2\tilde{S} + \tilde{N}^2$ . Considering the dimensionless system (2.8) and considering a constant dissipation rate of turbulent kinetic energy (set to 1, consistently with  $\epsilon = O(1)$  as mentioned above), we obtain, at first order

$$\left. \begin{aligned} \partial_t \tilde{N}^2 &= \frac{1}{Pr Re} \partial_{zz} \tilde{N}^2 + \frac{1}{Ri_b} \partial_{zz} [\tilde{Ri} Ri_b \Gamma'(Ri_b)], \\ \partial_t \tilde{S} &= \frac{1}{Re} \partial_{zz} \tilde{S} + \frac{Pr_T}{Ri_b} \partial_{zz} [\tilde{Ri} Ri_b \Gamma'(Ri_b) - \tilde{S} \Gamma(Ri_b) - \tilde{Ri} \Gamma(Ri_b)], \end{aligned} \right\} \quad (3.3)$$

where we used the first-order expansion  $\Gamma(Ri_b Ri) = \Gamma(Ri_b) + \tilde{Ri} Ri_b \Gamma'(Ri_b)$  with  $\Gamma' := d\Gamma/dRi_b$ . We now seek normal mode solutions of the form  $[\tilde{S}, \tilde{N}^2] = [\mathcal{A}_S, \mathcal{A}_N] e^{ikz - i\omega t}$  and obtain a system of linear equations for the eigenvector  $[\mathcal{A}_S, \mathcal{A}_N]$ . Since we are interested in non-trivial solutions, we require the determinant of this system to be zero. This condition is equivalent to the dispersion relation

$$\alpha(k)\omega^2 - i\beta(k)\omega + \gamma(k) = 0, \quad (3.4)$$

where

$$\left. \begin{aligned} \alpha(k) &= 1, \\ \beta(k) &= f(Ri_b, Pr_T, Pr, Re)k^2, \\ \gamma(k) &= C(Ri_b, Pr_T, Pr, Re)k^4, \end{aligned} \right\} \quad (3.5)$$

with

$$\left. \begin{aligned} f(Ri_b, Pr_T, Pr, Re) &= (2Pr_T - 1)\Gamma'(Ri_b) - Pr_T \frac{\Gamma(Ri_b)}{Ri_b} - \frac{1}{Re} \left(1 + \frac{1}{Pr}\right), \\ C(Ri_b, Pr_T, Pr, Re) &= Pr_T \frac{\Gamma(Ri_b)\Gamma'(Ri_b)}{Ri_b} + \frac{Pr_T}{Pr Re} \left[-\frac{\Gamma(Ri_b)}{Ri_b} + 2\Gamma'(Ri_b)\right] \\ &\quad - \frac{\Gamma'(Ri_b)}{Re} - \frac{1}{Pr Re^2}. \end{aligned} \right\} \quad (3.6)$$

A wavenumber  $k$  is thus unstable if the dispersion relation (3.4) admits a solution for frequency  $\omega$  with a strictly positive imaginary part. This is equivalent to  $\gamma(k) > 0$  or  $\gamma(k) \leq 0$  and  $\beta(k) > 0$ . These conditions are equivalent to  $f > 0$  or  $C > 0$  and the set of parameters prone to linear instability is therefore

$$\{(Ri_b, Pr_T, Pr, Re), f > 0\} \cup \{(Ri_b, Pr_T, Pr, Re), C > 0\}. \quad (3.7)$$

The boundary of this set separates linearly unstable and stable parameter regions and is plotted in figure 4 for various molecular Prandtl numbers.

### 3.2. Link with diffusion

The linearised system (3.3) can be written in the matrix form

$$\begin{bmatrix} \partial_t \tilde{N}^2 \\ \partial_t \tilde{S} \end{bmatrix} = \mathbf{D} \begin{bmatrix} \partial_{zz} \tilde{N}^2 \\ \partial_{zz} \tilde{S} \end{bmatrix}, \quad (3.8)$$

Turbulent disruption of density staircases

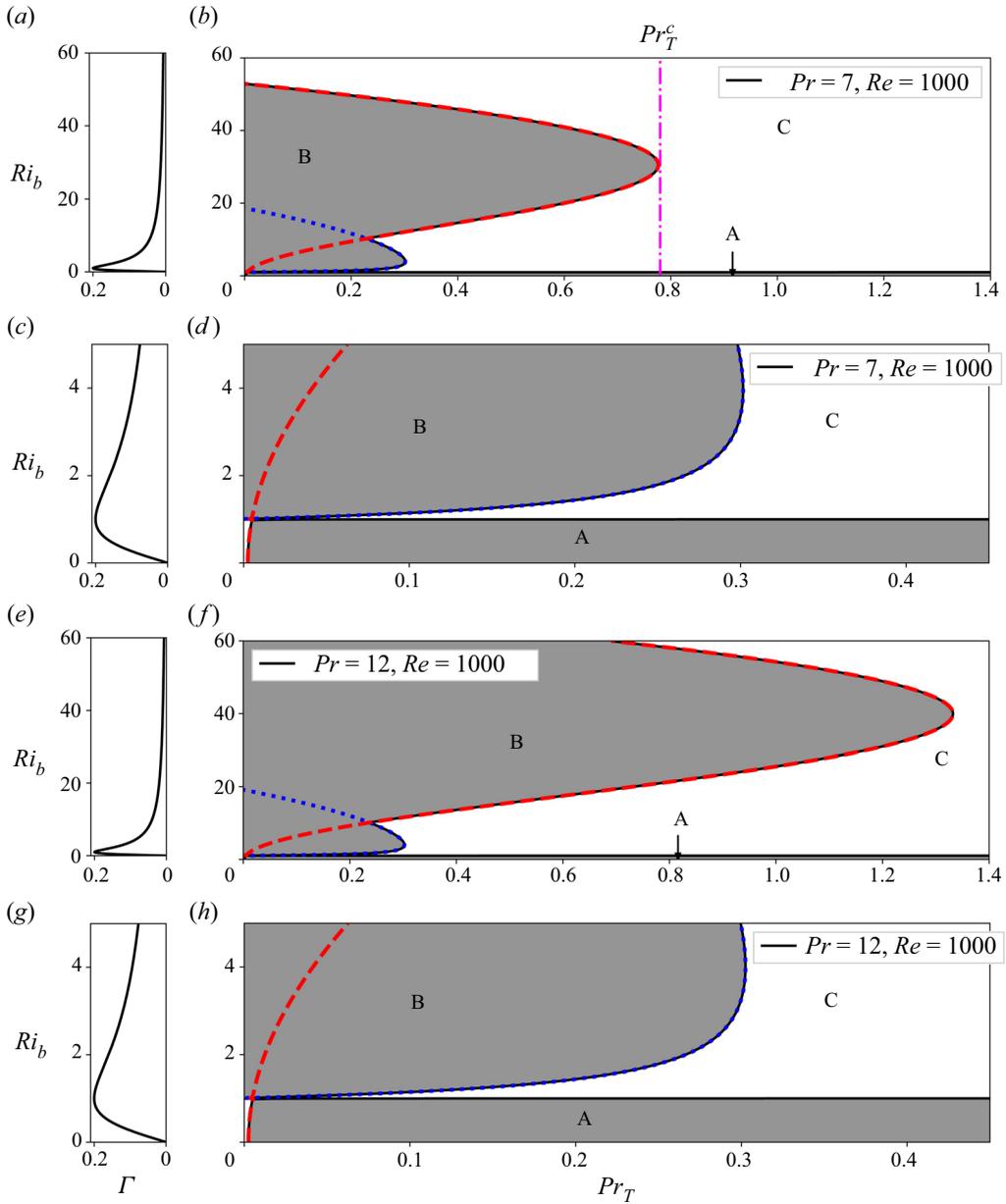


Figure 4. (a–h) Range of bulk Richardson numbers  $Ri_b$  and turbulent Prandtl numbers  $Pr_T$  prone to staircase formation for flows with various molecular Prandtl numbers  $Pr$  and  $Re = 1000$ , using parameterisation (2.11) of  $\Gamma$  with  $p = 1$  (depicted in a,c,e,g). Parameters in regions A and B exhibit staircase formation dynamics (grey shading) whereas parameters in region C do not. The horizontal boundary between A and C corresponds to  $Ri_b = Ri_b^m$  (i.e. the bulk Richardson number at which  $\Gamma$  is maximized). A zoom-in of region A for the considered values of  $Pr$  is shown in (c,d) and (g,h). The dotted blue curves correspond to the marginal condition  $f = 0$  whereas the dashed red curves correspond to the condition  $C = 0$  as defined in (3.6). The magenta dash-dotted vertical line corresponds to the critical value of the turbulent Prandtl number  $Pr_T^c$  above which no instability is possible on the decreasing right flank of the  $\Gamma$  curve.

where

$$\mathbf{D} = \begin{bmatrix} \Gamma'(Ri_b) + \frac{1}{Pr Re} & -2\Gamma'(Ri_b) \\ \frac{Pr_T}{Ri_b} [Ri_b \Gamma'(Ri_b) - \Gamma(Ri_b)] & \frac{Pr_T}{Ri_b} [-2Ri_b \Gamma'(Ri_b) + \Gamma(Ri_b)] + \frac{1}{Re} \end{bmatrix}. \quad (3.9)$$

The matrix  $\mathbf{D}$  may thus be thought of as a diffusion matrix and the real part of its eigenvalues can be interpreted as effective eddy diffusivities of our problem (a discussion on the imaginary parts of these eigenvalues is provided in § 4.2). The trace of this matrix is  $-f$  and its determinant is  $-C$ . Therefore, the instability conditions derived in the previous section are equivalent to the existence of an eigenvalue of this matrix with a negative real part and, hence, an antidiffusive dynamical behaviour that sharpens density gradients. This result can be generalized to the full (nonlinear) system (2.8) (as discussed in more detail in Appendix A) but for the purpose of the stability analysis the above (zeroth-order) eddy diffusivities suffice to understand the mechanism at hand.

### 3.3. Dependence on the parameters

#### 3.3.1. On the increasing left flank of the $\Gamma$ curve

In general, the qualitative stability properties do not depend on the particular functional form of the parameterisation  $\Gamma(Ri_b)$  but rather on the sign of its derivative  $\Gamma'(Ri_b)$ . For sufficiently small  $Ri_b$  such that  $\Gamma'(Ri_b) > 0$  (i.e. on the increasing ‘left flank’ of the flux coefficient curve), the system is linearly unstable for sufficiently large values of  $Pr_T$  (figure 4). As shown in figure 5(c,d), the critical value, denoted  $Pr_T^l$ , can be very small. More precisely, the instability occurs for  $Pr_T > Pr_T^l \simeq 0.001$  for flows where  $Pr = 7, Re = 1000$  and  $\Gamma$  increases as  $\Gamma(Ri_b) \propto Ri_b$ . Moreover,  $Pr_T^l$  appears to be largely insensitive to changes in  $Pr$  and tends towards zero as  $Re \rightarrow \infty$  (see figure 5(c,d)), although it is important to appreciate that the specific case  $Pr_T = 0$  (that yields  $f \leq 0$  and  $C \leq 0$ ) is always linearly stable for flows on the increasing left flank of the flux coefficient curve.

#### 3.3.2. On the decreasing right flank of the $\Gamma$ curve

Conversely, on the decreasing ‘right’ flank where  $\Gamma'(Ri_b) < 0$ , the flow is linearly stable for sufficiently large  $Pr_T$  and, therefore, there exists a critical value of the turbulent Prandtl number  $Pr_T$ , denoted  $Pr_T^c$  in the subsequent, above which no instability is possible on the decreasing left flank of the  $\Gamma$  curve (see figure 4(a,b)).

For finite values of  $Re$  (i.e.  $\nu^* \neq 0$ ; we discuss the strictly inviscid limit  $\nu^* = 0$  in § 3.4) and parameterisations of the form (2.11), the critical value  $Pr_T^c$  depends only on the molecular Prandtl number  $Pr$  as well as on the decreasing power law  $p$  of  $\Gamma$ , but not on  $Re$ . Indeed, if  $\Gamma \propto 1/Ri_b^p$  the mapping

$$Ri_b \rightarrow aRi_b, \quad Re \rightarrow a^{p+1}Re, \quad Pr_T \rightarrow Pr_T, \quad Pr \rightarrow Pr, \quad (3.10a-d)$$

maps  $f \rightarrow 1/a^{p+1}f$  and  $C \rightarrow 1/a^{2p+2}C$ , and so crucially does not affect the sign of these functions (and, hence, the associated stability properties). Hence, changing  $Re$  only stretches the boundary between linearly unstable and stable regions in the  $Ri_b$  direction, as depicted in figure 5, and do not affect  $Pr_T^c$ . Similarly, variations of the parameter  $A$  in

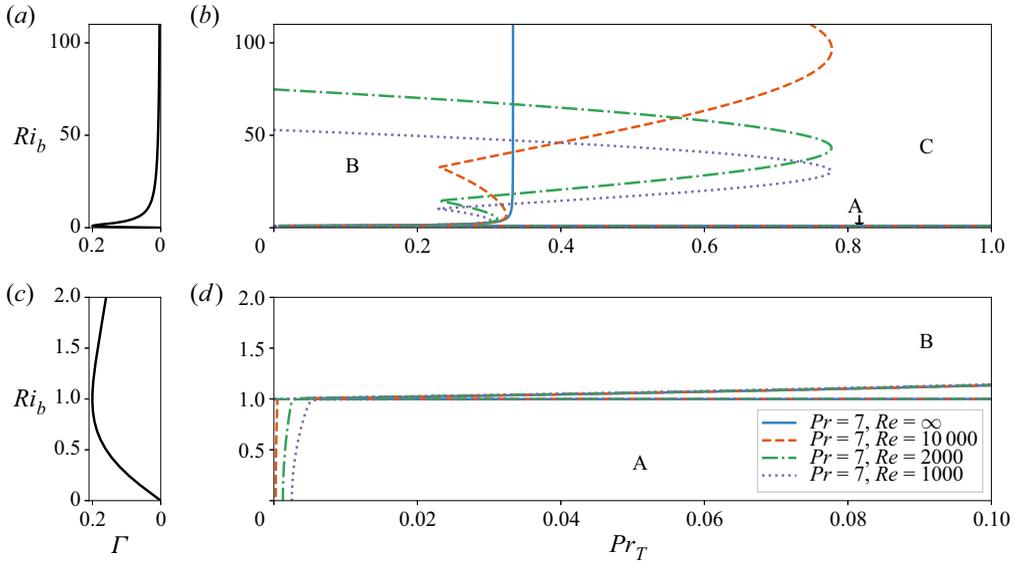


Figure 5. (a–d) Range of bulk Richardson numbers  $Ri_b$  and turbulent Prandtl numbers  $Pr_T$  prone to staircase formation for various Reynolds numbers  $Re$  and  $Pr = 7$ , using parameterisation (2.11) of  $\Gamma$  with  $p = 1$  (depicted in a,c). A zoom-in of region A is shown in (c,d). For  $Re = \infty$  (i.e.  $v^* = 0$ ), the boundary between B and C tends towards the vertical line  $Pr_T = 1/3$  (see solid blue line). As suggested by the scaling (3.10a–d), the critical turbulent Prandtl number  $Pr_T^c$  above which no instability is possible on the decreasing right flank of the  $\Gamma$  curve appears to be independent of  $Re$  for  $v^* \neq 0$ .

(2.11) does not significantly affect  $Pr_T^c$ . This can be established through consideration of the mapping

$$\Gamma \rightarrow a\Gamma, \quad Ri_b \rightarrow Ri_b, \quad Re \rightarrow \frac{1}{a}Re, \quad Pr_T \rightarrow Pr_T, \quad Pr \rightarrow Pr, \quad (3.11a-e)$$

which maps  $f \rightarrow af$  and  $C \rightarrow a^2C$  that once again does not affect the sign of  $f$  and  $C$ , key to the stability properties. Moreover, we have seen previously that scaling  $Re$  is equivalent to stretching the marginal stability curves in the  $Ri_b$  direction only. Therefore, the critical value  $Pr_T^c$  is unaffected by changes of  $A$ . Note that using a similar mapping, we can show that the choice of  $\epsilon$  in (2.8) does not affect  $Pr_T^c$ . Indeed, this constant only comes into play when multiplied by  $\Gamma$ . Likewise, the parameter  $B$  in (2.11) does not affect  $Pr_T^c$ . More precisely, variations in  $B$  translate the marginal stability curves in the  $Ri_b$  direction (since this parameter only affects the value  $Ri_b^m$  of the bulk Richardson number that maximizes  $\Gamma$ ). As a result, the critical value  $Pr_T^c$  depends on the decreasing power law  $p$  (see figure 6) but not on the particular choices for  $A$  and  $B$  in (2.11), suggesting some robustness of our results with respect to the parameterisation of the flux coefficient.

Variations of  $Pr_T^c$  with  $Pr$  are depicted in figure 7(a). The critical value  $Pr_T^c$  increases with  $Pr$ , consistently with the fact that staircase formation is favoured at large molecular Prandtl numbers (Taylor & Zhou 2017). More precisely, for  $p = 1$  and  $Pr = 7$  (the typical value of  $Pr$  for thermally stratified water),  $Pr_T^c \simeq 0.8$  whereas for  $Pr = 700$  (i.e. water where density is set by salinity),  $Pr_T^c \simeq 80$ . Variation of the critical value of  $Pr_T^c$  with  $p$  are depicted in figure 7(b). For example, for  $Pr = 7$  (and  $v^* \neq 0$ ), the critical value increases from  $Pr_T^c \simeq 0.5$  when  $p = 1/2$  to  $Pr_T^c \simeq 2$  for  $p = 8$ .

All in all, for  $Pr = 7$  and  $p$  of order unity, the critical value of the turbulent Prandtl number is found to be around  $Pr_T^c \simeq 0.5-0.8$ . Importantly, this key result concerning the

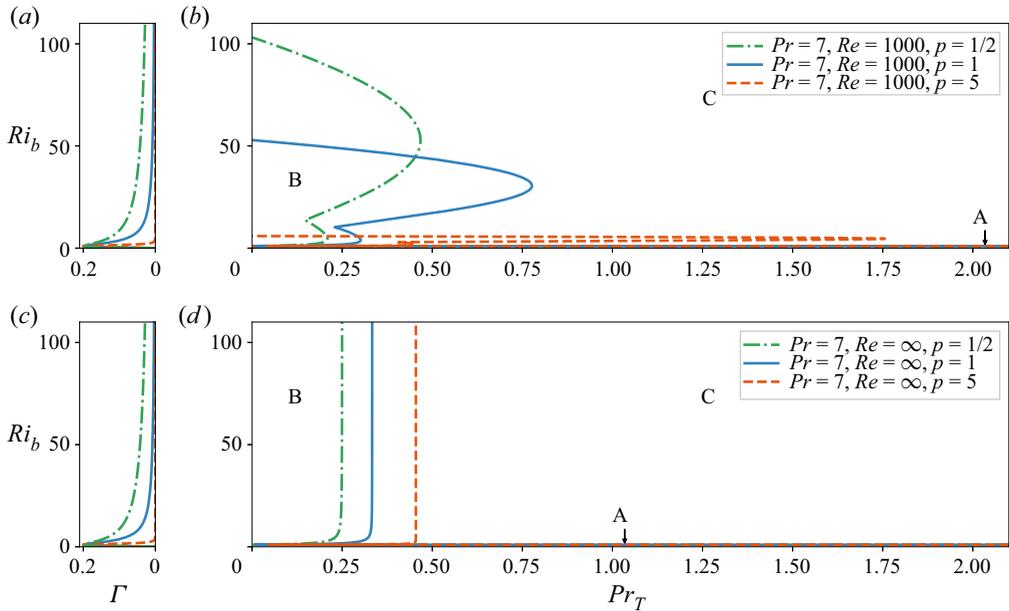


Figure 6. (a,b) Range of bulk Richardson numbers  $Ri_b$  and turbulent Prandtl numbers  $Pr_T$  prone to staircase formation for  $Pr = 7$  and  $Re = 1000$ , using parameterisation (2.11) of  $\Gamma$  with various power laws  $p$  (depicted in a,c). (c,d) Same as (a,b) but with  $Re = \infty$ . Note that the behaviour of  $\Gamma$  at small  $Ri_b$  is independent of  $p$ . Hence, region A is similar to the one depicted in figure 4.

critical turbulent Prandtl number does not depend on the scalings for the dissipation rate of turbulent kinetic energy considered in this paper. Indeed, for the intermediate scaling presented in § 2.2.2 leading to system (2.9), the associated mapping does not change  $Pr_T^c$ , but rather only stretches the marginal stability curves in the  $Ri_b$  direction as shown in figures 7 and 8. Analogously, for the strongly stratified scaling presented in § 2.2.3 leading to system (2.10), the associated mapping again does not change  $Pr_T^c$ , but rather stretches the marginal stability curves in the  $Ri_b$  direction and modifies the magnitude of the (unstable) growth rates.

Note that if  $\Gamma$  saturates at a constant value instead of monotonically decreasing towards zero at large bulk Richardson numbers, then  $\Gamma'(Ri_b) = 0$  for  $Ri_b$  large enough and both  $f$  and  $C$  become negative. Then the system is linearly stable for all  $Pr_T$  and  $Pr_T^c = 0$ .

We can also define a critical bulk Richardson number  $Ri_b^c$  above which no instability is possible. For parameterisations with  $\Gamma \propto 1/Ri_b^p$ ,  $Ri_b^c = O(Pr Re)^{1/(p+1)}$  under the assumption that the dissipation rate exhibits inertial scaling. When the dissipation rate exhibits the intermediate and strongly stratified scalings presented in §§ 2.2.2 and 2.2.3,  $Ri_b^c = O(Pr Re)^{1/(p+1/2)}$ . The fact that this limit increases with  $Re$  seems reasonable (as viscous effects are expected to inhibit perturbation growth), while the fact that  $Ri_b^c$  increases with  $Pr$  is consistent with previous studies establishing that staircase formation seems to be favoured for large molecular Prandtl numbers (Taylor & Zhou 2017).

### 3.4. Limit cases

In this section we analyse four limits of our problem, namely  $\nu^* = 0$ ,  $N_c^{*2} = 0$ ,  $Pr_T = 0$  and the case  $Pr \ll 1$ ,  $Pr Re \ll 1$ .

Turbulent disruption of density staircases

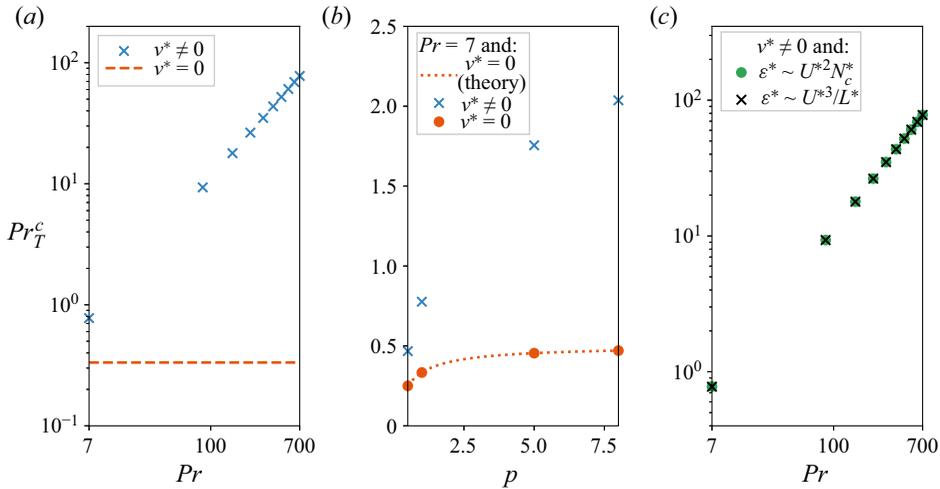


Figure 7. (a) Critical turbulent Prandtl number  $Pr_T^c$  above which no instability is possible on the decreasing right flank of the  $\Gamma$  curve as a function of  $Pr$  for  $v^* \neq 0$  (i.e. finite values of  $Re$ ) and  $v^* = 0$  (i.e.  $Re \rightarrow \infty$ ). From the scaling (3.10a–d), for  $v^* \neq 0$ ,  $Pr_T^c$  does not depend on  $Re$ , while for  $v^* = 0$ ,  $Pr_T^c$  does not depend on  $Pr$  (as shown by the orange dashed line). (b) The critical value  $Pr_T^c$  as a function of  $p$  for  $Pr = 7$  and  $v^* \neq 0$  (in this case,  $Pr_T^c$  depends on  $Pr$  but not on  $Re$ ) and  $v^* = 0$ . When  $v^* = 0$ ,  $Pr_T^c = p/(2p + 1)$  (orange dotted line). (c) The critical value  $Pr_T^c$  as a function of  $Pr$  for the various scalings discussed in § 2.2.

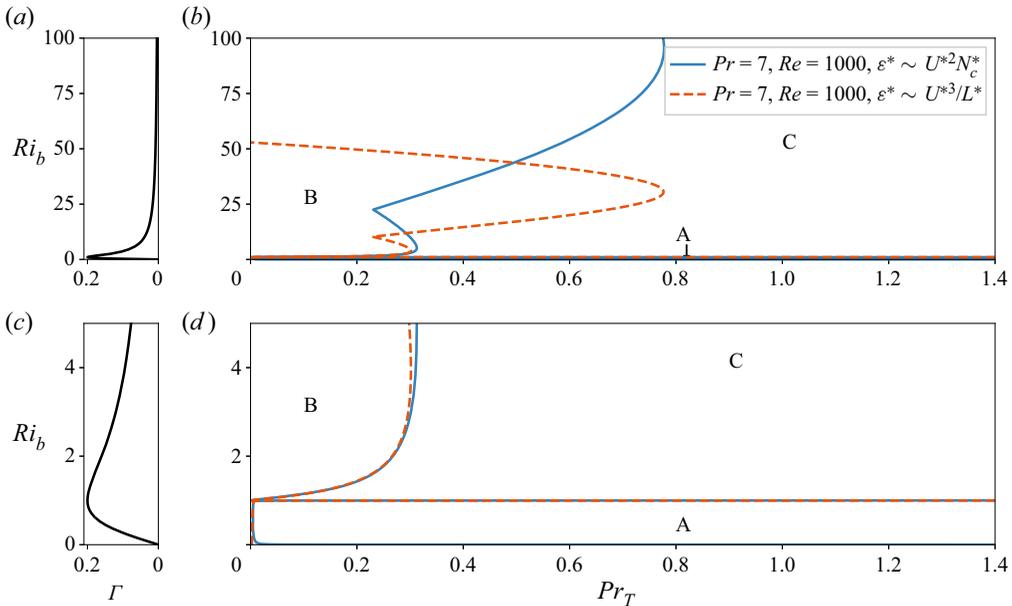


Figure 8. (a–d) Range of bulk Richardson numbers  $Ri_b$  and turbulent Prandtl numbers  $Pr_T$  prone to staircase formation for  $Pr = 7$  and  $Re = 1000$ , using parameterisation (2.11) of  $\Gamma$  with  $p = 1$  (depicted in a,c) for the different scalings for the dissipation rate of turbulent kinetic energy  $\epsilon^*$  discussed in § 2.2. A zoom-in of region A is shown in (c,d).

3.4.1. *Case  $\nu^* = 0$*

We first consider the inviscid limit  $\nu^* = 0$  (i.e.  $Re \rightarrow \infty$ ). On the increasing left flank of the  $\Gamma$  curve, we have  $C > 0$  for all  $Pr_T > 0$  and, therefore, the system is unstable in this case (the case  $Pr_T = 0$  gives  $C = 0$  and  $f < 0$  and is therefore stable). Conversely, on the decreasing right flank of the  $\Gamma$  curve, the condition  $C \geq 0$  is no longer well defined, as is apparent from the definition (3.6). Moreover, the condition  $f \geq 0$  cannot be satisfied on the decreasing right flank of the  $\Gamma$  curve for  $Pr_T \geq 1/2$ . Hence, on the decreasing right flank of the  $\Gamma$  curve and for  $\nu^* = 0$ , if  $Pr_T \geq 1/2$  the system is linearly stable and this result is valid for any decreasing  $\Gamma$  curve, a result first derived by Kranenburg (1980). For  $\Gamma \propto 1/Ri_b^p$ , this bound can be sharpened to  $Pr_T \geq p/(2p + 1)$ , as shown in figures 6 and 7. (This result is not in contradiction with the critical value  $Pr_T^c$  for instability found in § 3.3 using the scaling (3.10a–d) since this scaling is valid for finite values of the Reynolds number  $Re$  only.)

3.4.2. *Case  $N_c^{*2} = 0$*

In the unstratified limit  $N_c^{*2} = 0$  there is (of course) no buoyancy to mix. The above analysis suggests that the case  $N_c^{*2} = 0$  (which is equivalent to  $Ri_b = 0$ ) is linearly unstable (at least for large enough turbulent Prandtl numbers) and we therefore expect instabilities to develop in the velocity field rather than in the buoyancy field. Since the scalings presented in § 2.2 cannot be used when  $N_c^{*2} = 0$ , we consider here the dimensional system (2.6). Let us first linearise the system (2.6) around a state of zero stratification, i.e. we decompose the buoyancy field (in dimensional form) as  $N^{*2} = 0 + \tilde{N}^{*2}$  (where  $\tilde{N}^{*2}$  is a small perturbation), implying the decomposition  $Ri_g = 0 + \tilde{N}^{*2}/S^{*2}$  for the Richardson number (no assumptions are made about the size of  $S^*$ ). We then obtain, at first order, in dimensional form

$$\left. \begin{aligned} \partial_t^* \tilde{N}^{*2} &= \kappa^* \partial_{z^*}^2 \tilde{N}^{*2} + \Gamma'(0) \partial_{z^*}^2 \left[ \epsilon^* \frac{\tilde{N}^{*2}}{S^{*2}} \right], \\ \partial_t^* S^* &= \nu^* \partial_{z^*}^2 S^* + Pr_T \Gamma'(0) \partial_{z^*}^2 \left[ \frac{\epsilon^*}{S^*} \right]. \end{aligned} \right\} \tag{3.12}$$

The  $\tilde{N}^{*2}$  equation is parabolic, and using a maximum principle (assuming, for example, Dirichlet boundary conditions), we can show that the perturbation  $\tilde{N}^{*2}$  will remain at all times bounded by the initial perturbation  $\max_{z^*} |\tilde{N}^{*2}(t^* = 0, z^*)|$ . Therefore, starting from a perturbation of the buoyancy profile small enough such that the above linearisation stands, this perturbation will remain small and any interesting dynamics will develop in the velocity profile alone.

3.4.3. *Case  $Pr_T = 0$*

In the limit of small turbulent Prandtl numbers, any layering dynamics will occur preferentially in the buoyancy field. More precisely, setting  $Pr_T = 0$  (and  $\epsilon = 1$  for clarity) in the dimensionless system (2.8) yields

$$\left. \begin{aligned} \partial_t N^2 &= \partial_{zz} \left[ \frac{1}{Pr Re} N^2 + \frac{1}{Ri_b} \Gamma(Ri_b Ri) \right], \\ \partial_t S &= \frac{1}{Re} \partial_{zz} S, \end{aligned} \right\} \tag{3.13}$$

and the system is now decoupled. The second equation is a purely diffusive equation that will damp any perturbation in the shear profile exponentially fast on molecular time scales. Hence, the shear  $S$  will tend towards the constant profile  $S_0 = 1$ , remembering that this system is dimensionless. The  $N^2$  equation is prone to the Phillips mechanism, as staircases will form in the buoyancy profile when the right-hand side  $F(N^2) = (1/Pr Re)N^2 + (1/Ri_b)\Gamma(Ri_b(N^2/S_0))$  is a decreasing function of  $N^2$ , whereas any perturbation will be damped on the increasing flank of this function. This observation is consistent with linear stability analysis. Indeed, for  $Pr_T = 0$ , we obtain the equivalent condition for instability,

$$f > 0 \text{ or } C > 0 \Leftrightarrow \Gamma'(Ri_b) < -\frac{1}{Pr Re}. \quad (3.14)$$

Therefore, the case  $Pr_T = 0$  is equivalent to the Phillips mechanism as formulated in Phillips (1972) and in this limit the system is linearly stable for  $Ri_b \leq Ri_b^m$  and staircase formation can only happen for sufficiently stratified flows. As shown in §3.3, this result can be extended to  $Pr_T \ll 1$ . On the contrary, for larger values of  $Pr_T$ , the instability seems to be favoured for small bulk Richardson numbers, i.e. sufficiently weakly stratified flows on the increasing left flank of the  $\Gamma$  curve. Hence, once again the central conclusion is that in the presence of shear- and buoyancy-driven turbulence, the Phillips mechanism for staircase formation in strongly stratified flows seems to survive only in the limit of small turbulent Prandtl numbers.

#### 3.4.4. Case $Pr \ll 1, Pr Re \ll 1$

Let us consider the case of small molecular Prandtl and Péclet numbers, where the Péclet number is defined as  $Pe := Pr Re$  and can be understood as the ratio of the advective and diffusive time scales. This case is relevant to astrophysical stratified turbulent flows where  $Pr$  usually ranges between  $10^{-9}$  and  $10^{-5}$  and can therefore sustain small  $Pe$ , high  $Re$  regimes (Garaud *et al.* 2015). In the limit  $Pr \ll 1$  and  $Pe \ll 1$  (and considering finite Reynolds, bulk Richardson and turbulent Prandtl numbers), consideration of (3.6) shows that  $f \rightarrow -\infty$ , while  $C \rightarrow \infty$  for  $Pr_T[-\Gamma(Ri_b)/Ri_b + 2\Gamma'(Ri_b)] - 1/Re > 0$  and  $C \rightarrow -\infty$  otherwise. Therefore, on the decreasing right flank of the  $\Gamma$  curve (i.e. where  $\Gamma'(Ri_b) \leq 0$ ), both  $f$  and  $C$  are negative and the system is linearly stable. Hence, for sufficiently large  $Ri_b$ , staircase formation is prohibited, consistently with the fact that buoyancy anomalies are rapidly diffused for  $Pe \ll 1$  (Cope *et al.* 2020).

### 4. Instability properties

#### 4.1. Wavenumber dependence

The dispersion relation (3.4) yields

$$\omega(k) = \frac{1}{2}[ik^2f \pm \Delta_0(k)^{1/2}], \quad (4.1)$$

where  $\Delta_0(k) := (-i\beta)^2 - 4\alpha\gamma = (-f^2 - 4C)k^4$ . Therefore,  $\omega \propto k^2$  and any perturbation of linearly unstable velocity and buoyancy profiles will grow with growth rates that are proportional to the square of the vertical wavenumber, as shown in figure 9. Hence, the model exhibits an ‘ultraviolet catastrophe’ of unbounded growth at small scales. This unphysical behaviour is a consequence of the fact that flux-gradient parameterisations of eddy turbulent fluxes inevitably break down at small scales (namely scales below the representative scale of the turbulent microstructures that shape the flow on larger scales). Similar issues have been encountered in the double-diffusion literature. For example,

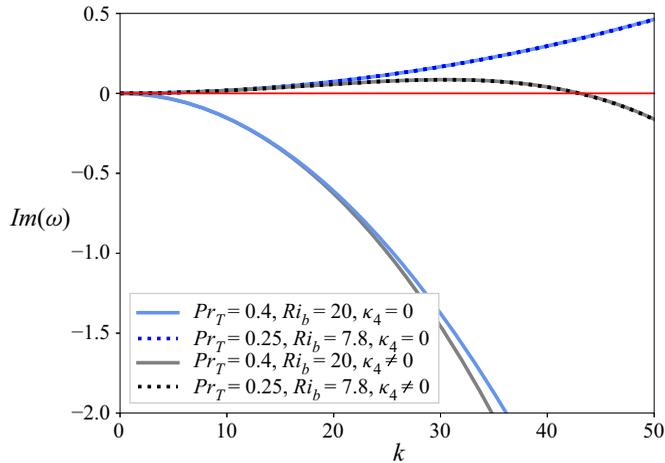


Figure 9. Growth rate as a function of the wavenumber  $k$  for various sets of parameters and with or without hyperdiffusion  $\kappa_4$ . The red horizontal line corresponds to  $Im(\omega) = 0$ . The blue curves (corresponding to  $\kappa_4 = 0$ ) unveil an ‘ultraviolet catastrophe’ of unbounded growth at small scales (i.e. large vertical wavenumbers  $k$ ).

Radko (2014) shows that fingering flux-gradient models tend to fail ‘when the size of the phenomenon of interest is comparable to the scale of microstructure that those laws strive to parameterise’.

Furthermore, Ma & Peltier (2021) encounter an ultraviolet catastrophe when studying salt-fingering-engendered thermohaline staircases using a diffusive parameterisation of heat and salinity turbulent fluxes. Again, the problem originates from the assumption that flux-gradient laws are valid at all scales, even those that are smaller than salt-finger widths. To resolve the problem, hyperdiffusive terms were added to the model to correct the model and dampen perturbations at small scales. This can be justified by a multiscale analysis of the problem (as performed by Radko 2019) that takes into account the interaction between small (microstructure turbulence) and larger scales.

#### 4.2. Regularisation of the model at small scales

Following the ideas of Radko (2019) and Ma & Peltier (2021), we add hyperdiffusion terms to regularise our dimensionless system (2.8) as follows:

$$\left. \begin{aligned} \partial_t N^2 &= \frac{1}{Pr Re} \partial_{zz} N^2 + \frac{1}{Ri_b} \partial_{zz} [\Gamma (Ri_b Ri) \epsilon] - \kappa_4 \partial_z^4 N^2, \\ \partial_t S &= \frac{1}{Re} \partial_{zz} S + \frac{Pr_T}{Ri_b} \partial_{zz} \left[ \frac{\Gamma (Ri_b Ri) \epsilon}{SRi} \right] - \kappa_4 \partial_z^4 S. \end{aligned} \right\} \quad (4.2)$$

The scaling factor  $\kappa_4$  will be chosen later.

Importantly, the addition of hyperdiffusion does not change our stability results. Indeed, following the same approach as in § 3, it can be shown that the dispersion relation becomes

$$\alpha_h(k) \omega^2 - i \beta_h(k) \omega + \gamma_h(k) = 0, \quad (4.3)$$

with

$$\left. \begin{aligned} \alpha_h(k) &= 1, \\ \beta_h(k) &= -2\kappa_4 k^4 + k^2 f(Ri_b, Pr_T, Pr, Re), \\ \gamma_h(k) &= k^4[-\kappa_4^2 k^4 + \kappa_4 f(Ri_b, Pr_T, Pr, Re)k^2 + C(Ri_b, Pr_T, Pr, Re)], \end{aligned} \right\} \quad (4.4)$$

where  $f$  and  $C$  are identical to the previous expressions given in (3.6). A wavenumber  $k$  is unstable if  $\gamma_h(k) > 0$  or  $\gamma_h(k) \leq 0$  and  $\beta_h(k) > 0$ . The condition  $\beta_h(k) > 0$  is equivalent to

$$k^2 < f/2\kappa_4. \quad (4.5)$$

Therefore, the existence of  $k \geq 0$  such that  $\beta_h(k) > 0$  is equivalent to  $f > 0$ . Then, if a set of parameters  $(Ri_b, Pr_T, Pr, Re)$  satisfy  $f > 0$  we can find small wavenumbers  $k < (f/2\kappa_4)^{1/2}$  that are linearly unstable. Regarding the condition on  $\gamma_h$ , we can show using the fact that  $\gamma_h/k^4$  is a polynomial of degree two in  $k^2$  that the existence of a wavenumber  $k \geq 0$  such that  $\gamma_h(k) > 0$  is equivalent to  $C > 0$  or  $C \leq 0$  and  $f > 0$  and  $f^2 > -4C$ . Combining the above conditions, the unstable set of parameters is defined by  $\{f > 0\} \cup \{C > 0\} \cup [\{C \leq 0\} \cap \{f > 0\} \cap \{f^2 > -4C\}] = \{f > 0\} \cup \{C > 0\}$ , exactly as in § 3. Moreover, using again the polynomial structure of  $\gamma_h/k^4$ , we can show that the maximum wavenumber satisfying  $\gamma_h(k) \geq 0$  is  $O(\kappa_4 \max(f, \sqrt{C})/\kappa_4^2)^{1/2} = O(\max(f, \sqrt{C})/\kappa_4)^{1/2}$  when it exists. Therefore, since the magnitude of  $f$  and  $\sqrt{C}$  is set by  $1/Re$  for the range of Reynolds numbers considered here, the largest unstable wavenumber, if it exists, is of order  $O(1/Re\kappa_4)^{1/2}$ .

All in all, the boundaries between stable and unstable regions do not depend on the ‘strength’ of the regularising hyperdiffusion (since  $f$  and  $C$  do not depend on  $\kappa_4$ ). However,  $\kappa_4$  does affect the magnitude of the growth rates. As a result, the system now has the largest unstable wavenumber (denoted  $k_c$  in the subsequent and of order  $O(1/Re\kappa_4)^{1/2}$  as shown previously) and a maximum growth rate  $\sigma_{max}$  attained at a wavenumber that we will denote  $k_{max}$ . We plot these quantities for various values of the parameters in figures 10 and 11. The maximum growth rate  $\sigma_{max}$  may be interpreted as a relevant time scale of staircase formation whereas  $k_{max}$  may be thought of as the length scale of the staircases potentially forming, at least at early times, before subsequent coarsening through layer merger, as we discuss further below.

It is apparent from figures 10 and 11 that the unstable region on the decreasing right flank of the  $\Gamma$  curve (region B) divides into two distinct regions of relatively large  $\sigma_{max}$  and  $k_c$  separated by a gap of relatively small  $\sigma_{max}$  and  $k_c$ , suggesting the existence of different types of unstable dynamics for  $Ri_b \geq Ri_b^m$ . A more precise description of these two dynamics can be given by considering in more detail the dispersion relation of the corrected system. More precisely, it can be written as

$$\omega(k) = \frac{1}{2}[-2i\kappa_4 k^4 + ik^2 f \pm \Delta_h(k)^{1/2}], \quad (4.6)$$

where  $\Delta_h(k) := (-i\beta_h)^2 - 4\alpha_h\gamma_h = (-f^2 - 4C)k^4 = \Delta_0(k)$  ( $\Delta_0$  has been defined in (4.1)). Therefore, if  $\Delta_0(k) > 0$ ,  $\omega(k)$  has both an imaginary and a real part and the component of vertical wavenumber  $k$  of the solution of the linearised problem will hence be exponentially increasing or decreasing (depending on the sign of the imaginary part of  $\omega(k)$ ) while oscillating with a frequency  $\frac{1}{2}\Delta_0(k)^{1/2}$ . On the contrary, if  $\Delta_0(k) \leq 0$ , then  $\omega(k)$  is purely imaginary and the dynamic of the linearised solution associated with the wavenumber  $k$  will be purely exponentially increasing or decreasing. Note that  $\Delta_0$  is of the

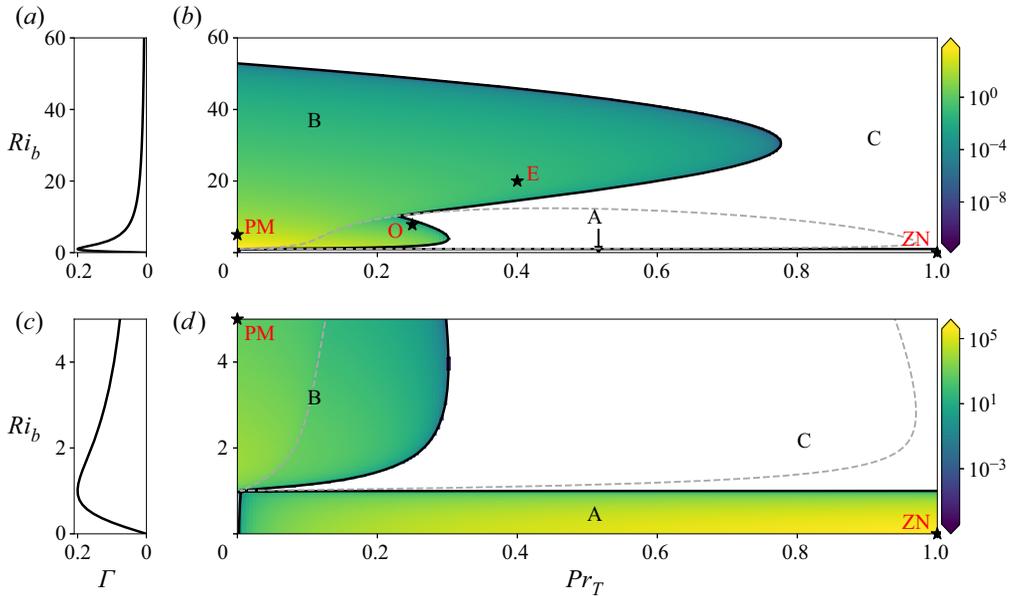


Figure 10. (a–d) Variation of maximum growth rate  $\sigma_{max}$  (on a logarithmic scale) with bulk Richardson number  $Ri_b$  and turbulent Prandtl number  $Pr_T$  for  $Pr = 7$ ,  $Re = 1000$ ,  $\kappa_4 = 10^{-7}$  and using parameterisation (2.11) of  $\Gamma$  with  $p = 1$  (depicted in a,c). The white regions correspond to  $\sigma_{max} \leq 0$  and, hence, are linearly stable regions. The black line separates linearly stable and unstable regions (and do not depend on the hyperdiffusion  $\kappa_4$ ). The dotted grey line corresponds to the contour line  $\Delta = 0$ . The stars mark the parameter values of the cases studied in § 5. Note from the vertical axes that (c,d) correspond to the small  $Ri_b$  region of (a,b). Note also the difference between the scales of (b,d). The labels PM, E, O and ZN denote the Phillips mechanism, exponential, oscillatory and zero  $N$  cases, respectively.

sign of  $\Delta := -f^2 - 4C$ , which depends only on the parameters  $Ri_b$ ,  $Pr_T$ ,  $Pr$  and  $Re$ , but crucially not on  $k$  nor on  $\kappa_4$ . We therefore expect different dynamics depending on the sign of  $\Delta$ : an ‘oscillatory’ behaviour for parameters satisfying  $\Delta > 0$  and a purely damped or exponentially growing one for  $\Delta \leq 0$ . (Note that these conditions on  $\Delta$  correspond to the condition for the diffusion matrix of our linearised system (see § 3.2) to have or not have eigenvalues with non-vanishing imaginary parts.) Importantly, this result is independent of the addition of a hyperdiffusion correction. The contour line corresponding to  $\Delta = 0$  is plotted in figure 10. Interestingly, it aligns with the gap of small  $\sigma_{max}$  and  $k_c$  mentioned above and shown in figures 10 and 11. This supports again the fact that at least two different types of unstable dynamics coexist in the unstable region B.

Using the above results, we can determine a relevant value for  $\kappa_4$ . More precisely, it is chosen so that the largest unstable wavenumber  $k_c$  is of order or smaller than, in dimensionless form,  $L^*/L_K^*$ , where  $L_K^* := (\nu^{*3}/\epsilon^*)^{1/4}$  is the Kolmogorov length scale. We choose this scale as it is the scale below which viscosity finally dissipates kinetic energy. Since the flows we are interested in typically have  $Pr \gtrsim 1$ ,  $L_K^* > L_B^* := L_K^*/\sqrt{Pr}$ , where  $L_B^*$  is the Batchelor scale at which fine structure in the scalar field is smoothed out by diffusivity. Therefore,  $L_K^*$  is a natural conservative scale to choose to regularise the build-up of perturbations at small scales. We have shown that the largest unstable wavenumber is of order  $O(1/Re\kappa_4)^{1/2}$  and, using the inertial scaling,  $L^*/L_K^*$  is of order  $O(Re^{3/4})$ . Therefore, for  $Re = O(1000)$ , we want  $\kappa_4 \gtrsim 10^{-8}$ . For the purpose of our numerical experiment (§ 5) and in order to form staircases that are not too small nor too

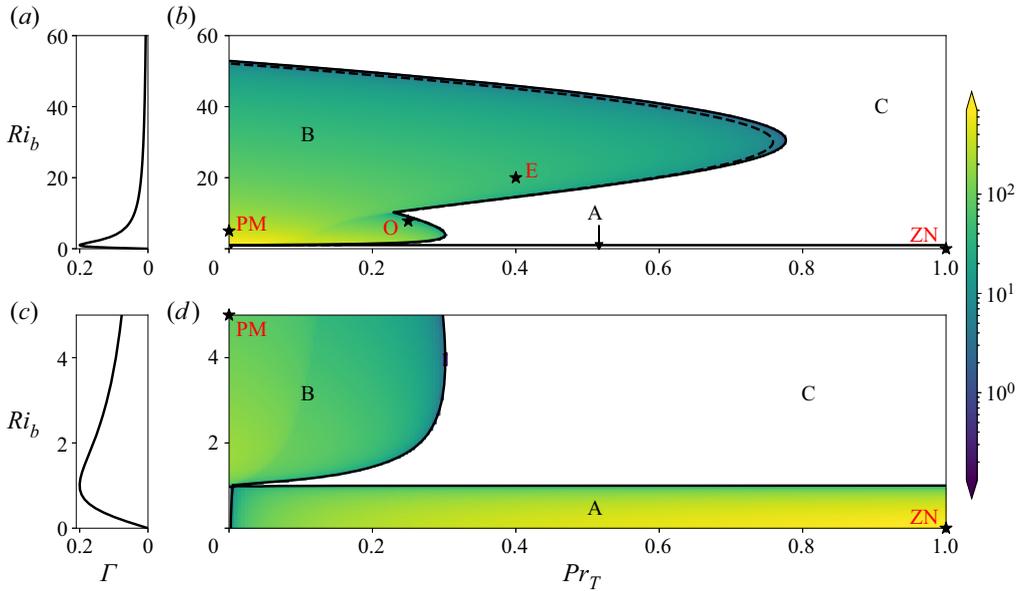


Figure 11. (a–d) Variation of the largest unstable wavenumber  $k_c$  (on a logarithmic scale) with bulk Richardson number  $Ri_b$  and turbulent Prandtl number  $Pr_T$  for  $Pr = 7$ ,  $Re = 1000$ ,  $\kappa_4 = 10^{-7}$  and using parameterisation (2.11) of  $\Gamma$  with  $p = 1$  (depicted in a,c). The white regions correspond to  $k_c = 0$  and, hence, are linearly stable regions. The black line separates linearly stable and unstable regions. The dashed line corresponds to the  $k_c = 2\pi$  contour line. Whereas parameters in the coloured regions (regions A and B) are prone to staircase formation, only parameters in the region inside the dotted line will exhibit staircase formation dynamics numerically. The stars correspond to the cases studied in § 5. Note from the vertical axes that (c,d) correspond to the small  $Ri_b$  region of (a,b).

large, we henceforth choose the conservative values  $\kappa_4 = 10^{-5}$  or  $10^{-7}$ , depending on the particular choice of the parameters, as discussed further below.

### 5. Nonlinear dynamics

In this section we numerically solve the regularised dimensionless system (4.2) and compare the nonlinear dynamics to the linear stability analysis presented above.

In order to solve (4.2), boundary conditions need to be specified. In the following, we consider periodic boundary conditions for the shear  $S$  and stratification  $N^2$ ,

$$\forall t \geq 0, \quad S(t, z = 0) = S(t, z = 1), \quad N^2(t, z = 0) = N^2(t, z = 1). \quad (5.1a,b)$$

These conditions quantize the range of admissible vertical wavenumbers  $k$ , which are now of the form  $k = 2\pi n$ , where  $n = 0, 1, \dots$  (in practice,  $n$  will in fact be bounded above by  $1/dz$ , where  $dz$  is the spatial grid size of our numerical calculations). Since the case  $n = 0$  has zero growth rate, if the largest unstable wavenumber  $k_c$  (which exists thanks to the addition of hyperdiffusion) is smaller than  $2\pi$ , the system will be ‘numerically’ linearly stable, although it could of course have been linearly unstable provided other boundary conditions were chosen. We plot the largest unstable wavenumber for various values of the parameters in figures 11 as well as the contour line  $k_c = 2\pi$ .

Inspired by the linear stability analysis (§ 3) we consider the following dimensionless initial conditions for three different choices with non-zero  $Ri_b$  marked on figure 11 (i.e. the

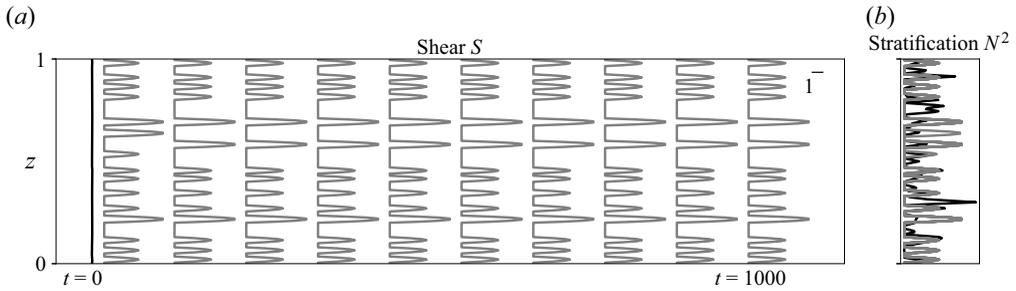


Figure 12. Evolution of the shear and stratification for case ZN with  $N_c^{*2} = 0$ ,  $Pr_T = 1$ ,  $Pr = 7$  and  $Re = 1000$ . (a) The horizontal axis is time and each profile is separated by 100 dimensionless time units. Peaks in these profiles correspond to interfaces of enhanced vertical gradients separating well-mixed layers. The initial shear profile is depicted in black. The horizontal scale on the top right corner corresponds to a representative scale of variations of the shear  $S$ . (b) The initial condition (black line) as well as the profile at a later time (grey lines) can be plotted on the same axis, demonstrating that the magnitude of the perturbations on the buoyancy profile do not grow significantly above the initial perturbation. (Note that in order to form staircases that are big enough to be visible, we use the higher value of  $\kappa_4 = 10^{-5}$ .)

Phillips mechanism (PM), oscillatory (O) and exponential (E) cases):

$$\forall z \in [0, 1], \quad S(t = 0, z) = 1 + \tilde{n}(z), \quad N^2(t = 0, z) = 1 + \tilde{n}(z). \quad (5.2a,b)$$

Here  $\tilde{n}$  is a small random noise, normally distributed with 0 mean and 0.01 standard deviation. For the zero  $Ri_b$  case (case ZN, i.e. ‘zero  $N$ ’),  $N_c^{*2} = 0$  and we then set  $N^2(t = 0, z) = \max(0, \tilde{n}(z)) \geq 0$  so that the profile is always statically stably stratified.

Using the above boundary and initial conditions, system (4.2) can be solved using the method presented in Appendix B. In order to obtain the velocity and the buoyancy fields from the computed shear and the stratification profiles,  $S$  and  $N^2$  are integrated over space. The integration constants are chosen so that the conservation of mass and momentum is respected, i.e.

$$\forall t \geq 0, \quad \int_0^1 b(t, z) dz = \int_0^1 b(0, z) dz, \quad \int_0^1 u(t, z) dz = \int_0^1 u(0, z) dz. \quad (5.3a,b)$$

We focus our attention on the following four sets of linearly unstable parameters, each with  $Re = 1000$  and  $Pr = 7$ , as marked with stars on figures 10 and 11.

- (i) Case ZN:  $N_c^{*2} = 0$  and  $Pr_T = 1$ . This choice of parameters illustrates the limiting unstratified case  $N_c^{*2} = 0$  presented in § 3.4.2. We show the numerical results in figure 12. Here the perturbations in the buoyancy profile do not grow above their initial magnitude and layering occurs in the velocity profile.
- (ii) Case PM:  $Ri_b = 5$  (on the decreasing right flank of the  $\Gamma$  curve) and  $Pr_T = 0$ . This set of parameters illustrates the theoretical results presented in § 3.4.3 for  $Pr_T = 0$ . We show the numerical solution in figure 13. Perturbations in the velocity profile are damped and the linear velocity profile (constant shear profile) is retrieved whereas perturbations in the buoyancy profile grow and form layers that eventually merge.
- (iii) Case O:  $Ri_b = 7.8$  (decreasing right flank of the  $\Gamma$  curve) and  $Pr_T = 0.25$ . This set of parameters has been chosen in the unstable region B as shown in figure 11, so that  $\Delta > 0$ . The maximum growth rate is  $\sigma_{max} \simeq 0.09$  and attained for a

Turbulent disruption of density staircases

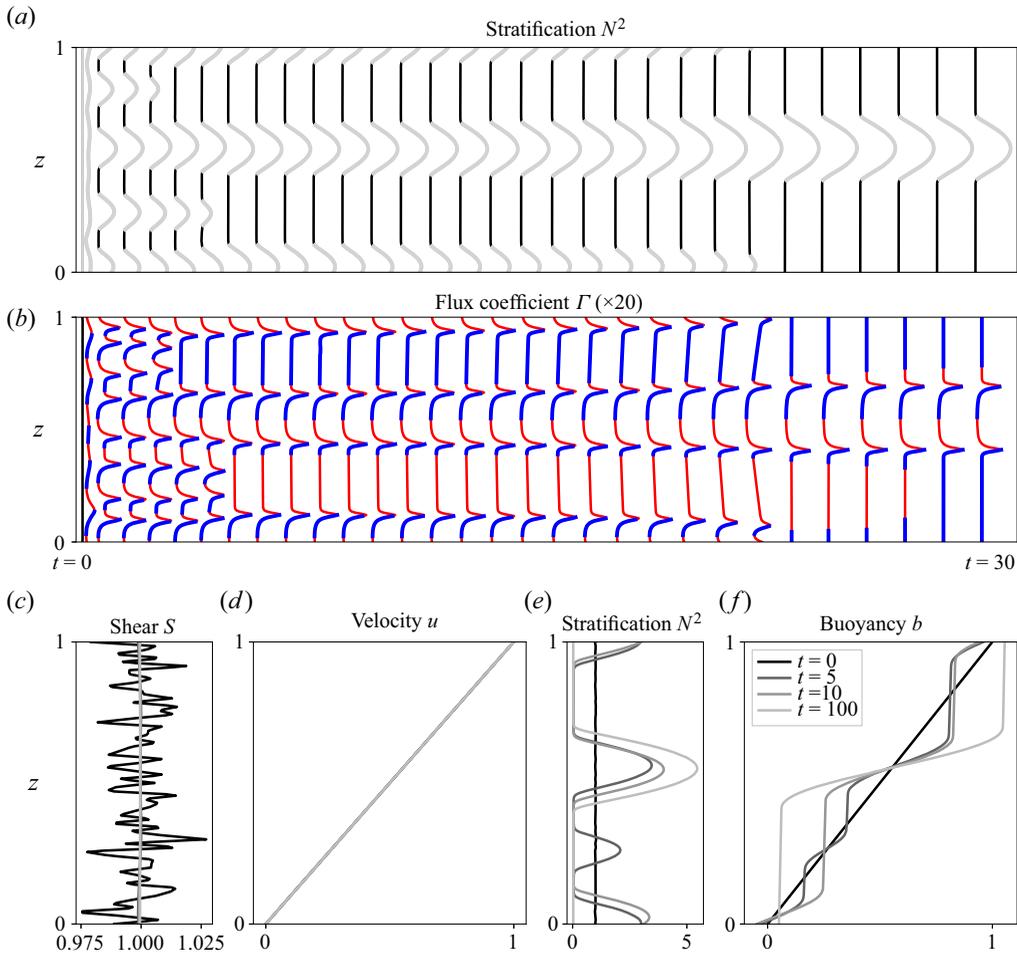


Figure 13. (a–f) Evolution of the buoyancy, velocity and flux coefficient profiles for case PM with  $Ri_b = 5$ ,  $Pr_T = 0$ ,  $Pr = 7$  and  $Re = 1000$ . (c–f) The black lines correspond to the initially disturbed profiles (the same perturbation is used for both the velocity and buoyancy). (a,b) The horizontal axis is time and each profile is separated by one dimensionless time unit. On the  $N^2$  profiles (a), the grey regions correspond to regions where the effective eddy diffusivity defined in Appendix A is negative. For the flux coefficient profiles (b), red corresponds to upwelling while blue corresponds to downwelling, unveiling the convergence/divergence of buoyancy flux patterns underlying the Phillips mechanism (note that in order to form staircases that are big enough to be visible, we use the higher value of  $\kappa_4 = 10^{-5}$ ).

wavenumber  $k_{max} \simeq 30.4$ . Therefore, we expect the development of structures of length scale  $\sim 0.2$  dimensionless space units in around 10 dimensionless time units. Since  $\Delta > 0$ , we also expect some kind of oscillatory behaviour in the time evolution of the buoyancy and velocity profiles. We show the time evolution of the amplitude of the fastest growing mode (corresponding to  $k_{max}$ ) as well as numerical profiles in figures 14–17. After a transient phase, yet before the saturation of the instability, the perturbation appears to grow at the predicted rate simultaneously and concomitantly in both the shear and stratification profiles. Interestingly, staircases seem to ‘pulse’ with a period of approximately 3 dimensionless time units, corresponding to the theoretical period  $2\pi/(0.5\Delta_0(k_{max})^{1/2}) \simeq 3$  (see § 4). Furthermore, the development of buoyancy and velocity staircases appears to be

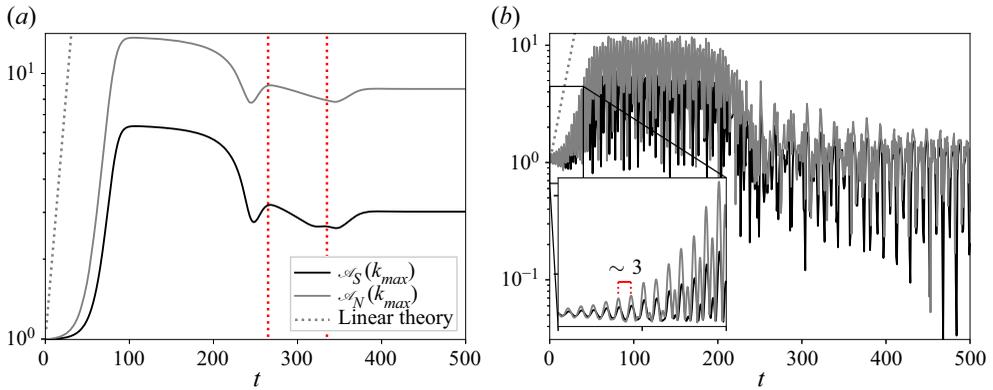


Figure 14. Time evolution of the amplitude of the fastest growing mode (normalized by the initial amplitude) for case E with  $Ri_b = 20$ ,  $Pr_T = 0.4$ ,  $Pr = 7$ ,  $Re = 1000$  and  $\kappa_4 = 10^{-7}$  (a); and case O with  $Ri_b = 7.8$ ,  $Pr_T = 0.25$ ,  $Pr = 7$ ,  $Re = 1000$  and  $\kappa_4 = 10^{-7}$  (b) for the shear (black line) and stratification (grey line). The dotted grey line corresponds to the evolution predicted by the linear theory. The red dotted lines correspond to the end of merging events.

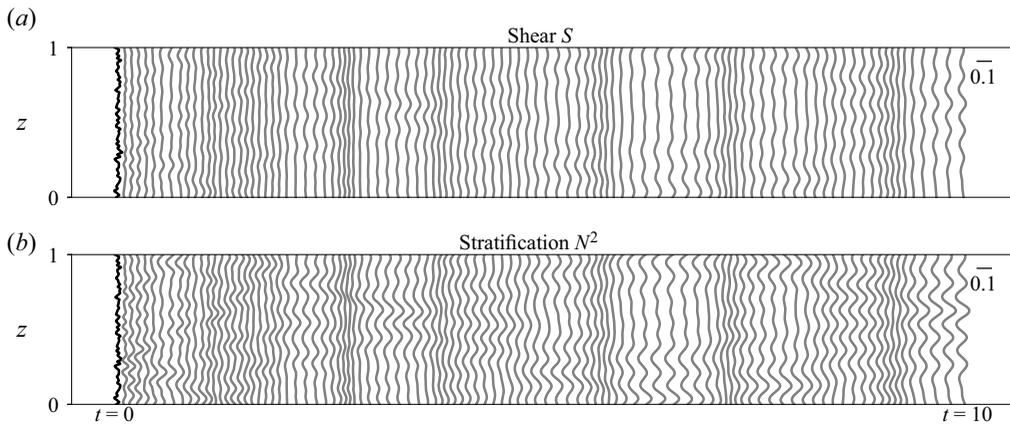


Figure 15. Evolution of shear and stratification profiles for case O with  $Ri_b = 7.8$ ,  $Pr_T = 0.25$ ,  $Pr = 7$  and  $Re = 1000$ . The black lines correspond to the initially disturbed profiles. The horizontal axis is time and each profile is separated by a 0.1 dimensionless time unit. We use the lower value of  $\kappa_4 = 10^{-7}$ .

locked and in phase. The initial layers (before they start merging), have a length scale of  $\sim 0.2$  dimensionless space units, demonstrating the relevance of the linear stability analysis. Similar dynamics is observed for other sets of linearly unstable parameters on the decreasing right flank of the  $\Gamma$  curve satisfying  $\Delta > 0$ .

- (iv) Case E:  $Ri_b = 20$  (also on the decreasing right flank of the  $\Gamma$  curve) and  $Pr_T = 0.4$ . This set of parameters lies on the linearly unstable region B and satisfies  $\Delta \leq 0$ . It has been chosen so that the unstable branch of the growth rate spectrum associated with this case is similar to the one associated with the previous case (see figure 9). Therefore, the relevant time and length scales associated with the development of potential instabilities will be similar in both cases and we expect a structure of length scale  $\sim 0.2$  dimensionless space units to appear. We show the time evolution of the amplitude of the fastest growing mode as well as numerical profiles in figures 14

*Turbulent disruption of density staircases*

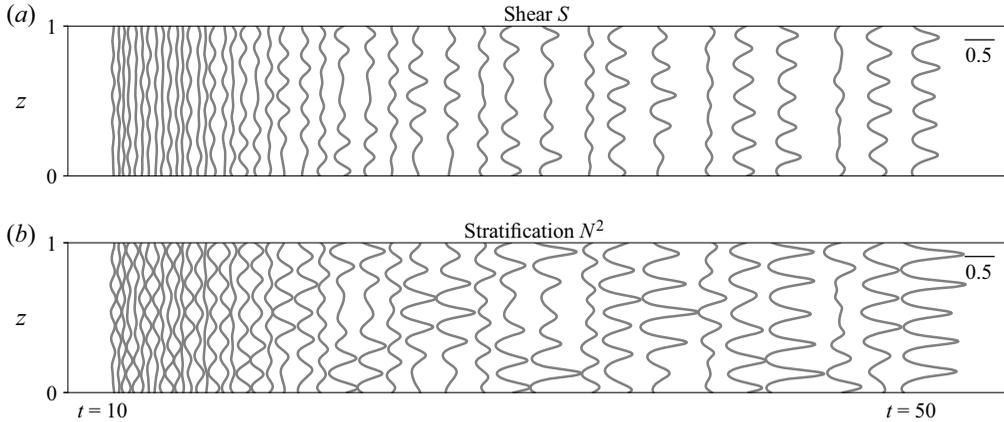


Figure 16. Later time evolution in the same format as figure 15 (case O). The horizontal axis is again time and each profile is separated by 1 dimensionless time unit.

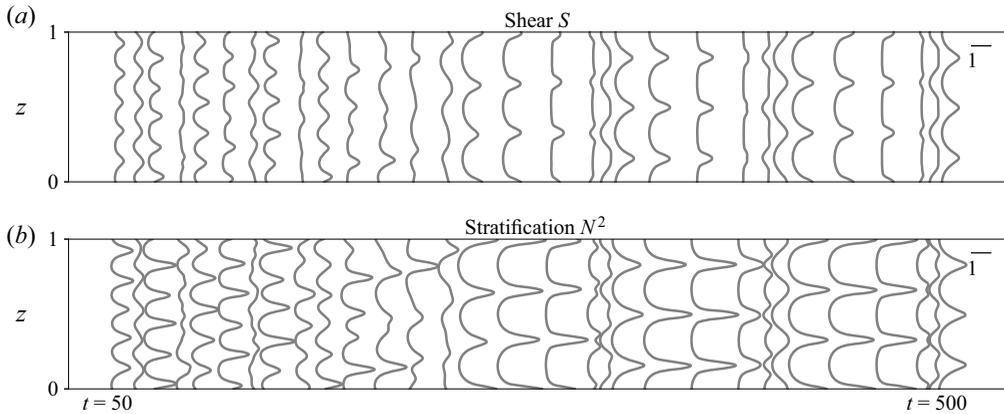


Figure 17. Further later time evolution in the same format as figure 15 (case O). The horizontal axis is again time and each profile is separated by 15 dimensionless time units.

and 18. After a short transient (and before saturation of the instability), the fastest growing mode grows at the expected theoretical rate. The initial layers (before they start merging) have a length scale of  $\sim 0.2$  dimensionless space units, once again as predicted by the linear theory. As the instability saturates, layers start to merge. No oscillations in time are observed, in line with  $\Delta \leq 0$ . Interestingly, and unlike the previous case where the perturbations in the stratification and the shear seemed to evolve concomitantly and staircases form almost simultaneously and in phase in the buoyancy and velocity profiles, buoyancy staircases seem to form slightly before velocity ones. Similar dynamics is observed for other sets of parameters on the decreasing right flank of the  $\Gamma$  curve satisfying  $\Delta \leq 0$ . This behaviour is also reminiscent of the case  $Pr_T = 0$  exhibiting the Phillips mechanism and associated with the condition  $C \geq 0$  (that implies  $\Delta \leq 0$ ) where staircases form exclusively in the buoyancy field.

All in all, the unstable parameters region should be thought of as being divided into three subregions: a low  $Ri_b$  region (corresponding to  $Ri_b \ll 1$ ) where the dynamics is mostly shear-driven and where staircase formation happens in the velocity profile since there are

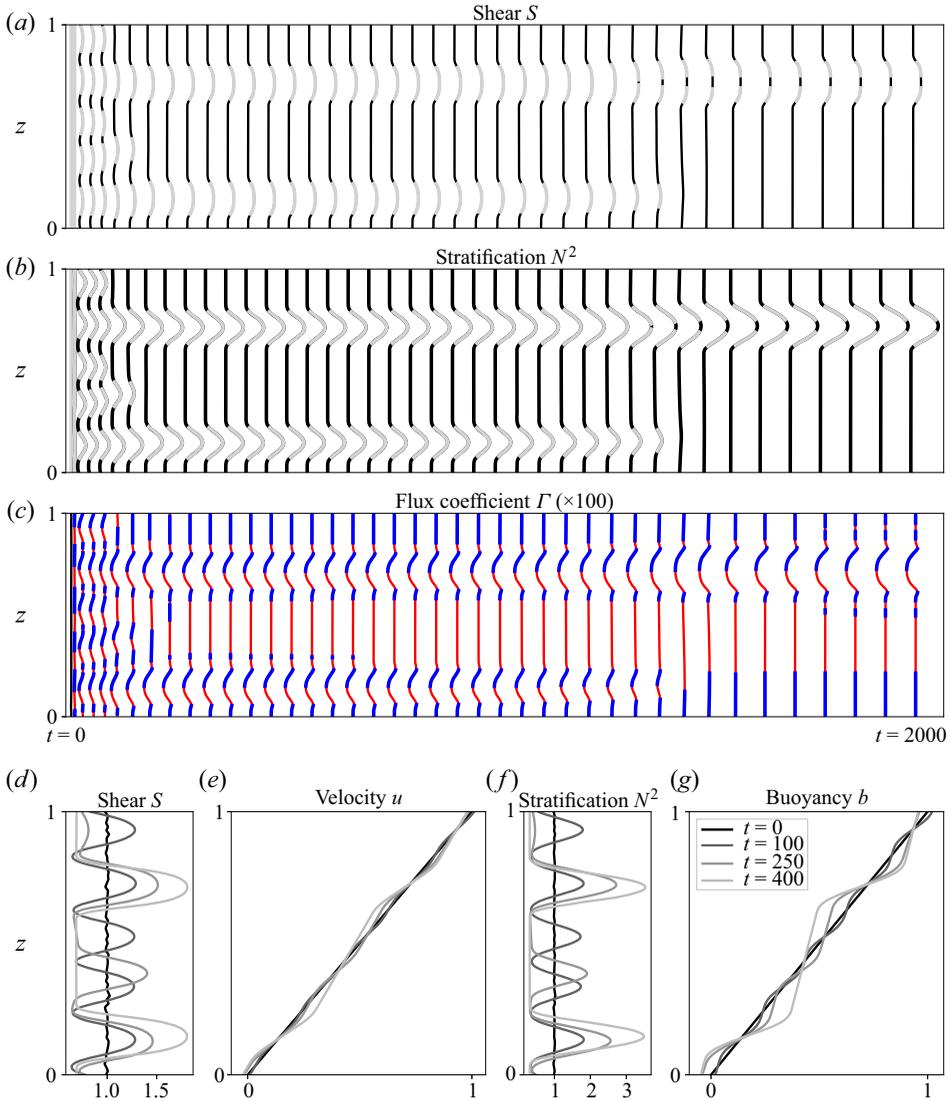


Figure 18. (a–g) Evolution of the buoyancy, velocity and flux coefficient profiles for case E with  $Ri_b = 20$ ,  $Pr_T = 0.4$ ,  $Pr = 7$  and  $Re = 1000$ . (a–c) The horizontal axis is time and each profile is separated by 50 dimensionless time units. On the shear and stratification profiles (a,b), the grey regions correspond to regions where the effective eddy diffusivity defined in Appendix A is negative. On the flux coefficient profiles (c), red corresponds to upwelling while blue corresponds to downwelling.

no buoyancy gradients to mix; an intermediate  $Ri_b$  and small  $Pr_T$  region (corresponding to  $Ri_b \geq Ri_b^m$ ,  $\Delta > 0$ ) where the dynamics is buoyancy- and shear-driven and where staircases form almost simultaneously in both the buoyancy and velocity fields with staircase ‘pulsation’; and an intermediate to large  $Ri_b$  and small  $Pr_T$  region (corresponding to  $Ri_b \geq Ri_b^m$  and  $\Delta \leq 0$ ) where the dynamics is again shear- and buoyancy-driven and staircases develop without ‘pulsation’ before merging as the instability saturates.

The nonlinear dynamics also pinpoint the qualitatively different mixing happening in the well-mixed layers and in the strongly stratified interfaces separating layers. Inside the layers, the density anomalies are smoothed and mixing can therefore be described by an

appropriately defined positive eddy diffusivity (see [Appendix A](#)). In the interfaces, such an eddy diffusivity becomes formally negative (see [figures 13](#) and [18](#) for instance) and the mixing is therefore in some sense ‘antidiffusive’, in the specific sense that it appears to sharpen the buoyancy gradients by scouring the interface, as suggested by the presence of local maxima of  $\Gamma$  at the borders of density interfaces (although further analysis and direct numerical simulations are undoubtedly needed to confirm this point). Similarly, the observation that inside the interfaces the flux coefficient is minimal supports the hypothesis that density staircases are barriers to mixing.

## 6. Discussion

In this paper we have derived a reduced-order model aiming at describing the formation and evolution of density staircases in sheared and (stably) stratified turbulent flows. Following the ideas of Phillips (1972) and Posmentier (1977), we have parameterised the turbulence using flux-gradient models. Using this framework, we have determined regions in the parameter space ( $Ri_b, Pr_T, Pr, Re$ ) prone to staircase formation. Crucially, these regions depend on the monotonicity of variation of the flux coefficient  $\Gamma$  with the bulk Richardson number  $Ri_b$ . Since experimental, observational and numerical evidence seem to indicate that  $\Gamma$  increases with  $Ri_b$  up to some critical value  $Ri_b^m$  and plausibly decreases for  $Ri_b \geq Ri_b^m$  (Linden 1979, 1980; Wells *et al.* 2010), the staircase ‘instability’ depends on the size of  $Ri_b$  compared with  $Ri_b^m$ . Most importantly, we have also presented theoretical evidence that this instability depends on the turbulent Prandtl number  $Pr_T$ .

On the increasing left flank of the  $\Gamma$  curve, the instability occurs for  $Pr_T$  above a (very small) given threshold, found to be around 0.001 for the case with  $\Gamma(Ri_b) \propto Ri_b$ ,  $Pr = 7$  and  $Re = O(1000)$ . Therefore, for sufficiently small  $Pr_T \ll 1$ ,  $Ri_b < Ri_b^m$  is stable to staircase formation, retrieving the result from Phillips (1972) that stratification needs to be sufficiently large (i.e. on the decreasing right flank of the  $\Gamma$  curve) to be prone to staircase formation. However, for larger (though still small) values of  $Pr_T$ , staircase instabilities can actually be triggered in weakly stratified flows (in the sense  $Ri_b < Ri_b^m$ , i.e. on the increasing left flank of the  $\Gamma$  curve) in the presence of buoyancy- and shear-driven turbulence.

Conversely, on the decreasing right flank of the  $\Gamma$  curve, the instability occurs for sufficiently small turbulent Prandtl numbers and moderate to large bulk Richardson numbers. More precisely, for relevant oceanic parameters, staircase formation via the Phillips mechanism is only possible within this model for  $Pr_T \lesssim 0.5\text{--}0.8$ . The existence of this upper bound on the turbulent Prandtl number, that importantly has been shown to depend strongly on  $Pr$  and weakly on the precise parameterisation of the turbulent fluxes (in the sense that it depends only on the rate of the decrease of  $\Gamma$  with  $Ri_b$ ) but not on  $Re$  (for non-zero values of the molecular diffusivity  $\nu^*$ ) nor on the scalings for the dissipation rate of turbulent kinetic energy discussed in this work, confirms that the Phillips mechanism for staircase formation in strongly stratified flows is only valid for small values of  $Pr_T$  in the presence of both buoyancy- and shear-driven turbulence. It also suggests that staircase formation is not favoured in ocean interiors, as empirically observed. Indeed, the turbulent Prandtl number in stably stratified turbulence is usually found to be  $Pr_T \gtrsim 0.7$  (Venayagamoorthy & Stretch 2010) and observational data (see [figure 1](#)) supports the fact that ocean interiors are sufficiently strongly stratified, suggesting that these regions are not in a favourable parameter regime for staircase formation via the Phillips mechanism.

Considering further the decreasing right flank of the  $\Gamma$  curve, as the molecular Prandtl number increases, the upper bound on  $Pr_T$  increases, favouring staircase formation as discussed in Taylor & Zhou (2017). The upper bound on  $Pr_T$  reaches values of order  $O(100)$  for  $Pr = 700$  (salty water), consistently with the fact that staircase formation has often been observed in laboratory experiments using salinity gradients rather than temperature gradients. This also suggests that staircase formation could be favoured in regions of the ocean where stratification is salt dominated, such as estuaries (Holleman, Geyer & Ralston 2016). Finally, in the limit  $\nu^* = 0$  (i.e.  $Re \rightarrow \infty$ ), the upper bound on  $Pr_T$  for instability is smaller than  $1/2$ , regardless of the form of  $\Gamma$ . This result, independent of the explicit form of  $\Gamma$ , supports again the fact that the Phillips mechanism for staircase formation in strongly stratified flows seems to survive only in the limit of small turbulent Prandtl numbers and that density staircase formation via this mechanism is not favoured in the presence of buoyancy- and shear-driven turbulence in relatively strongly stratified flows.

The nonlinear dynamics following the initial linear instability growth exhibit various interesting properties. For flows with unstable parameters on the decreasing right flank of the  $\Gamma$  curve, the nonlinear behaviour seems to be divided into two categories. For flows with parameters such that  $\Delta > 0$  (see § 4), a staircase instability appears to develop simultaneously in both the buoyancy and velocity fields which forms layers that pulse and merge as time evolves. Conversely, for flows with parameters such that  $\Delta \leq 0$ , staircases develop without pulsing and merge as the instability saturates, reminiscent of the purely buoyancy-driven mechanism that occurs for  $Pr_T = 0$ , a case that is equivalent to the Phillips mechanism as formulated in Phillips (1972) (§ 3.4.3) and for which the instability is also associated with the condition  $\Delta \leq 0$ .

More generally, the nonlinear evolution of the layers underlines the qualitative differences between the mixing expected in the presence or absence of density staircases. In the absence of density staircases, the mixing is purely diffusive in the sense that it smooths density gradients and can be modelled by an appropriately defined positive eddy diffusivity (see Appendix A). On the contrary, the interfaces between layers are characterised by a negative effective eddy diffusivity and the mixing process at hand scours density interfaces, sharpens density gradients and, hence, is in some sense ‘antidiffusive’. Since antidiffusive problems are both mathematically and numerically challenging, this raises intricate parameterisation issues for flux-gradient based models.

There are of course several limitations of our model. Firstly, our model is relevant to regions of the ocean where double-diffusive effects (due to the presence of gradients of both temperature and salinity for instance) are negligible but breaks down in regions of the world’s oceans where double diffusion becomes prominent such as in polar regions or the Mediterranean Sea. Similarly, our model breaks down near boundaries where boundary effects might become significant. Secondly, it is important to remember that  $\Gamma$  cannot be parameterised in terms of the Richardson number only. It depends on other parameters, such as the buoyancy Reynolds number  $Re_b = \epsilon^*/(\nu^*N^*2)$  (Shih *et al.* 2005; Salehipour *et al.* 2016; Mashayek *et al.* 2017). Thirdly, we considered the different dimensionless control parameters of our system as free parameters that crucially were independent of each other and of the dynamical quantities. Several studies suggest however dependence of the turbulent Prandtl number  $Pr_T$  with, for instance, the gradient or bulk Richardson number (see Venayagamoorthy & Stretch (2010) or Katul *et al.* (2014) for more detailed discussions). Since our goal was to explore the full parameter space but not to assess whether it was indeed entirely accessible, we did not take these relationships into account.

However, we expect that enforcing such constraints would restrict the range of accessible parameters but not change our linear stability results and, hence, would not alter the main conclusions of our work. Similarly, our analysis has considered ranges of parameters prone to staircase formation provided they can sustain turbulence (so that the considered scalings for  $\epsilon^*$  hold). We however did not assess whether the full parameter space considered here could actually maintain turbulence, a study that is beyond the scope of this work. Similarly, our model assumes constant  $\epsilon^*$  and focuses therefore on patches of relatively homogeneous in space and sustained in time turbulence. However, the robustness of our results with regard to various scalings for  $\epsilon^*$  (§ 2.2.2) as well as to the size of  $\epsilon^*$  itself suggests that the model presented here is relevant to both shear-dominated and buoyancy-dominated turbulent regimes (Mater & Venayagamoorthy 2014) as well as to weakly and strongly stratified regimes (Garanaik & Venayagamoorthy 2019).

**Acknowledgements.** We would like to kindly thank L. Baker for giving us access to the data used to generate the first figure of this work as well as P. Sellers and J. Clouseau for inspiration. Thanks are also due to three anonymous reviewers whose comments greatly improved this manuscript. For the purpose of open access, the authors have applied a Creative Commons Attribution (CC BY) licence to any author accepted manuscript version arising from this submission.

**Funding.** This project has received funding from the European Union’s Horizon 2020 research and innovation program under the Marie Skłodowska-Curie grant agreement no. 956457. A.M. acknowledges funding from the NERC IRF fellowship grant NE/P018319/1 and from the ONR grant 13328635.

**Declaration of interests.** The authors report no conflict of interest.

**Author ORCIDs.**

- Ⓜ Nicolaos Petropoulos <https://orcid.org/0000-0002-8585-7139>;
- Ⓜ Ali Mashayek <https://orcid.org/0000-0002-8202-3294>;
- Ⓜ Colm-cille P. Caulfield <https://orcid.org/0000-0002-3170-9480>.

**Appendix A**

Similarly to what we have done in § 3.2, we recast the full (nonlinear) problem (2.8) as a diffusion problem. To do so, note that it can be put into the following matrix form:

$$\begin{bmatrix} \partial_t b \\ \partial_t u \end{bmatrix} = \mathbf{D}_{nl} \begin{bmatrix} \partial_{zz} b \\ \partial_{zz} u \end{bmatrix}. \tag{A1}$$

Here

$$\mathbf{D}_{nl} = \begin{bmatrix} \frac{\Gamma'(Ri_b Ri)}{(\partial_z u)^2} + \frac{1}{Pr Re} & -2 \frac{\Gamma'(Ri_b Ri) Ri}{\partial_z u} \\ \frac{Pr_T}{Ri_b Ri^2 (\partial_z u)^3} [Ri_b Ri \Gamma'(Ri_b Ri) & \frac{Pr_T}{Ri_b Ri \partial_z u} [-2 Ri_b Ri \Gamma'(Ri_b Ri) \\ - \Gamma(Ri_b Ri)] & + \Gamma(Ri_b Ri)] + \frac{1}{Re} \end{bmatrix}. \tag{A2}$$

The matrix  $\mathbf{D}_{nl}$  is the nonlinear diffusion matrix associated to our problem. The real part of the eigenvalues of this matrix can be interpreted as effective eddy diffusivities of the system. Since the sign of these real parts is related to the sign of the trace  $\text{Tr}(\mathbf{D}_{nl})$  and determinant  $\det(\mathbf{D}_{nl})$  of  $\mathbf{D}_{nl}$ , regions where  $\text{Tr}(\mathbf{D}_{nl}) < 0$  or  $\det(\mathbf{D}_{nl}) < 0$  will be prone to antidiffusive dynamics that will sharpen density interfaces. (Note that these quantities are defined locally in space.) Note that  $-f$  and  $-C$  are the zeroth-order approximation of these quantities, linking the linear dynamics to the nonlinear dynamics.

## Appendix B

Let us formally write the system of (4.2) in the following form:

$$\partial_t y = \partial_{zz}[f(y)] - \kappa_4 \partial_z^4 y. \quad (\text{B1})$$

We first discretize the above in space using second order in space schemes and obtain

$$\partial_t y_i = \frac{1}{dz^2} [f(y_{i+1}) - 2f(y_i) + f(y_{i-1}))] + \frac{1}{dz^4} [y_{i+2} - 4y_{i+1} + 6y_i - 4y_{i-1} + y_{i-2}], \quad (\text{B2})$$

where  $i \in \{2, \dots, N-2\}$  are the indices of the grid points,  $dz$  is the spacing between grid points and  $\mathbf{y}(t) = (y_0(t), \dots, y_N(t))^T$  are the approximate values of  $y(t)$  at the grid points. The formulae for  $i \in \{0, 1, N-1, N\}$  depend on the boundary conditions used in  $z = 0$  and  $z = 1$ . We have considered periodic boundary conditions in our analysis. The above can be put into a matrix form

$$\partial_t \mathbf{y} = \mathbf{A}_{dz}(\mathbf{y}), \quad (\text{B3})$$

with  $\mathbf{A}_{dz} : \mathbb{R}^{N+1} \rightarrow \mathcal{M}^{N+1, N+1}(\mathbb{R})$ . This is a system of  $N+1$  ordinary differential equations. We can now use an appropriate time-stepping scheme to solve the problem numerically. We have used the backward differentiation formula method with an adaptive step size from the python library `scipy` in order to resolve accurately the stiff dynamics that appear as staircases form.

As staircases form, the shear  $S$  might become close to zero. This can introduce inappropriate divisions by zero in the definition of the Richardson number and lead to numerical difficulties. To avoid this issue, we consider  $Ri = N^2 / (S^2 + \eta)$ , where  $\eta$  is a small parameter. We use  $\eta = 10^{-9}$  in our simulations.

## REFERENCES

- BALMFORTH, N.J., LLEWELLYN SMITH, S.G. & YOUNG, W.R. 1998 Dynamics of interfaces and layers in a stratified turbulent fluid. *J. Fluid Mech.* **355**, 329–358.
- BARENBLATT, G.I., BERTSCH, M., DAL PASSO, R., PROSTOKISHIN, V.M. & UGHI, M. 1993 A mathematical model of turbulent heat and mass transfer in stably stratified shear flow. *J. Fluid Mech.* **253**, 341–358.
- BILLANT, P. & CHOMAZ, J.-M. 2001 Self-similarity of strongly stratified inviscid flows. *Phys. Fluids* **13** (6), 1645–1651.
- BOUFFARD, D. & BOEGMAN, L. 2013 A diapycnal diffusivity model for stratified environmental flows. *Dyn. Atmos. Oceans* **61**, 14–34.
- CAULFIELD, C.P. 2021 Layering, instabilities, and mixing in turbulent stratified flows. *Annu. Rev. Fluid Mech.* **53** (1), 113–145.
- COPE, L., GARAUD, P. & CAULFIELD, C.P. 2020 The dynamics of stratified horizontal shear flows at low Péclet number. *J. Fluid Mech.* **903**, A1.
- GARANAİK, A. & VENAYAGAMOORTHY, S.K. 2019 On the inference of the state of turbulence and mixing efficiency in stably stratified flows. *J. Fluid Mech.* **867**, 323–333.
- GARAUD, P., MEDRANO, M., BROWN, J.M., MANKOVICH, C. & MOORE, K. 2015 Excitation of gravity waves by fingering convection, and the formation of compositional staircases in stellar interiors. *Astrophys. J.* **808** (1), 89.
- HOLLEMAN, R.C., GEYER, W.R. & RALSTON, D.K. 2016 Stratified turbulence and mixing efficiency in a salt wedge estuary. *J. Phys. Oceanogr.* **46** (6), 1769–1783.
- IVEY, G.N. & IMBERGER, J. 1991 On the nature of turbulence in a stratified fluid. Part I: the energetics of mixing. *J. Phys. Oceanogr.* **21** (5), 650–658.
- IVEY, G., IMBERGER, J. & KOSEFF, J.R. 1998 *Buoyancy Fluxes in a Stratified Fluid*, Coastal and Estuarine Studies, vol. 54, pp. 377–388. American Geophysical Union.

## Turbulent disruption of density staircases

- KATUL, G.G., PORPORATO, A., SHAH, S. & BOU-ZEID, E. 2014 Two phenomenological constants explain similarity laws in stably stratified turbulence. *Phys. Rev. E* **89** (2), 023007.
- KAY, D.J. & JAY, D.A. 2003 Interfacial mixing in a highly stratified estuary 1. Characteristics of mixing. *J. Geophys. Res. (Oceans)* **108** (C3), 3072.
- KRANENBURG, C. 1980 On the stability of turbulent density-stratified shear flow. *J. Phys. Oceanogr.* **10** (7), 1131–1133.
- LINDEN, P.F. 1979 Mixing in stratified fluids. *Geophys. Astrophys. Fluid Dyn.* **13** (1), 3–23.
- LINDEN, P.F. 1980 Mixing across a density interface produced by grid turbulence. *J. Fluid Mech.* **100** (4), 691–703.
- MA, Y. & PELTIER, W.R. 2021 Gamma instability in an inhomogeneous environment and salt-fingering staircase trapping: determining the step size. *Phys. Rev. Fluids* **6**, 033903.
- MASHAYEK, A., BAKER, L.E., CAEL, B.B. & CAULFIELD, C.P. 2022 A marginal stability paradigm for shear-induced diapycnal turbulent mixing in the ocean. *Geophys. Res. Lett.* **49** (2), e2021GL095715.
- MASHAYEK, A., SALEHIPOUR, H., BOUFFARD, D., CAULFIELD, C.P., FERRARI, R., NIKURASHIN, M., PELTIER, W.R. & SMYTH, W.D. 2017 Efficiency of turbulent mixing in the abyssal ocean circulation. *Geophys. Res. Lett.* **44** (12), 6296–6306.
- MATER, B.D. & VENAYAGAMOORTHY, S.K. 2014 A unifying framework for parameterizing stably stratified shear-flow turbulence. *Phys. Fluids* **26** (3), 036601.
- OGLETHORPE, R.L.F., CAULFIELD, C.P. & WOODS, A.W. 2013 Spontaneous layering in stratified turbulent Taylor–Couette flow. *J. Fluid Mech.* **721**, R3.
- OSBORN, T.R. 1980 Estimates of the local rate of vertical diffusion from dissipation measurements. *J. Phys. Oceanogr.* **10** (1), 83–89.
- PARK, Y.-G., WHITEHEAD, J.A. & GNANADESKIAN, A. 1994 Turbulent mixing in stratified fluids: layer formation and energetics. *J. Fluid Mech.* **279**, 279–311.
- PHILLIPS, O.M. 1972 Turbulence in a strongly stratified fluid—is it unstable? In *Deep Sea Research and Oceanographic Abstracts*, vol. 19, pp. 79–81. Elsevier.
- POSMENTIER, E.S. 1977 The generation of salinity finestructure by vertical diffusion. *J. Phys. Oceanogr.* **7** (2), 298–300.
- RADKO, T. 2014 Applicability and failure of the flux-gradient laws in double-diffusive convection. *J. Fluid Mech.* **750**, 33–72.
- RADKO, T. 2016 Thermohaline layering in dynamically and diffusively stable shear flows. *J. Fluid Mech.* **805**, 147–170.
- RADKO, T. 2019 Thermohaline layering on the microscale. *J. Fluid Mech.* **862**, 672–695.
- RIPPETH, T. & FINE, E. 2022 Turbulent mixing in a changing Arctic Ocean. *Oceanography* **35** (3/4), 66–75.
- RUDDICK, B.R., MCDOUGALL, T.J. & TURNER, J.S. 1989 The formation of layers in a uniformly stirred density gradient. *Deep Sea Res. A. Oceanogr. Res. Papers* **36** (4), 597–609.
- SALEHIPOUR, H., PELTIER, W.R., WHALEN, C.B. & MACKINNON, J.A. 2016 A new characterization of the turbulent diapycnal diffusivities of mass and momentum in the ocean. *Geophys. Res. Lett.* **43** (7), 3370–3379.
- SHIH, L.H., KOSEFF, J.R., IVEY, G.N. & FERZIGER, J.H. 2005 Parameterization of turbulent fluxes and scales using homogeneous sheared stably stratified turbulence simulations. *J. Fluid Mech.* **525**, 193–214.
- TAYLOR, J.R. & ZHOU, Q. 2017 A multi-parameter criterion for layer formation in a stratified shear flow using sorted buoyancy coordinates. *J. Fluid Mech.* **823**, R5.
- THORPE, S.A. 1982 On the layers produced by rapidly oscillating a vertical grid in a uniformly stratified fluid. *J. Fluid Mech.* **124**, 391–409.
- TIMMERMANS, M.-L., TOOLE, J., KRISHFIELD, R. & WINSOR, P. 2008 Ice-tethered profiler observations of the double-diffusive staircase in the Canada Basin thermocline. *J. Geophys. Res.: Oceans* **113** (C1).
- TURNER, J.S. 1968 The influence of molecular diffusivity on turbulent entrainment across a density interface. *J. Fluid Mech.* **33** (4), 639–656.
- VENAYAGAMOORTHY, S.K. & STRETCH, D.D. 2010 On the turbulent Prandtl number in homogeneous stably stratified turbulence. *J. Fluid Mech.* **644**, 359–369.
- WELLS, M., CENEDESE, C. & CAULFIELD, C.P. 2010 The relationship between flux coefficient and entrainment ratio in density currents. *J. Phys. Oceanogr.* **40** (12), 2713–2727.
- WOODS, A.W., CAULFIELD, C.P., LANDEL, J.R. & KUESTERS, A. 2010 Non-invasive turbulent mixing across a density interface in a turbulent Taylor–Couette flow. *J. Fluid Mech.* **663**, 347–357.