

REGULAR PAPER

Flight Characteristics with Different Supercooled Large Droplet Ice Configurations

C. Deiler 

DLR (German Aerospace Center), Institute of Flight Systems, Braunschweig, Germany
E-mail: christoph.deiler@dlr.de

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Abstract

An evaluation of the effects of different ice configurations on the flight characteristics of a fixed-wing aircraft is presented. Within a joint research project of German Aerospace Center (DLR) and Brazilian aircraft manufacturer Embraer simulation models of three supercooled large droplet (SLD) ice configurations were developed for one Phenom 300 prototype. A specific flight test campaign with artificial SLD ice shapes on the aircraft was conducted to gather the relevant flight data. The simulation models for the different ice configuration were obtained by system identification, and specific results for the SLD-ice simulation models are provided. The analysis of aircraft characteristics was based on the results of these high-quality simulation models: the icing-induced changes of the flight performance characteristics evaluated by the interpretation of several parameters like thrust-to-weight ratio and specific excess power. The typical flight performance degradation was found for all ice configurations with different magnitude. The change of aircraft eigenmodes was investigated in detail by analysing the system matrix of the linearised models at a specific trim points. In addition, the diverse effects found for different ice configurations (App. C and SLD) are discussed and the change of root locus is analysed. Furthermore, ice-induced changes of the handling qualities are evaluated using numerical criteria of flying qualities standard “MIL-STD-1797 A”: no significant deterioration was found for the investigated ice configurations.

Nomenclature

base	base model part (clear aircraft, no ice)
$C_{()}$	aerodynamic coefficient
C_D	drag coefficient
C_{D0}	zero-lift drag coefficient
C_L	lift coefficient
C_l	rolling moment coefficient
C_{L0}	lift coefficient at $\alpha = 0^\circ$
C_m	pitching moment coefficient
$C_{m0,WB}$	wing/body pitching moment coefficient at $\alpha = 0^\circ$
c_1, α^*	separation point function parameters
D	drag force, N
DR	Dutch roll
g	gravitational acceleration, m/s^2
IAS	indicated airspeed
ice	Δ -model part (icing)
k_p, d_p	icing model parameters
L	lift force, N
L/D	lift-to-drag ratio
L, M, N	body-fixed aerodynamic moments, Nm

m_{AC}	aircraft mass, kg
max	maximum value
P	model parameter
PH	phugoid
p, q, r	rotational velocities, rad/s
req	required
RO	rolling motion
SEP	specific excess power, m/s
SLD	Supercooled Large Droplets
SP	short period
T	engine thrust force, N
TAS	true airspeed
TWR	thrust-to-weight ratio
V	velocity, m/s
WB	wing/body
\hat{X}	non-dimensional location of the wing separation point
$y_{Wing}^{1,2}$	wing force application point

Greek Symbol

α	angle of attack, rad
β	angle of sideslip, rad
η	elevator deflection, rad
ζ	damping
ξ	aileron deflection, rad
ω_0	natural frequency, rad/s

1.0 Introduction

Icing can have hazardous effects on aircraft performance characteristics and can be a limiting factor for the safe flight envelope. The change of the dynamic behaviour and potential premature stall raise the need for pilot situational awareness and an adaption of control strategy. Various accidents worldwide have shown the severity of icing related degradations, e.g., Refs. [1–4], especially when caused by supercooled large water droplets (SLD) against which current aircraft are not protected. The certification of (modern) transport aircraft for flight into (known) icing conditions was mainly based on the certification requirements given in the so-called App. C to e.g., CS-25. But with the identified hazard to fixed-wing aircraft resulting from SLD the aviation agencies issued the new App. O to the certification requirements. From now on, manufacturers must prove that a newly developed aircraft is also safe for flight into these even more hazardous atmospheric icing conditions.

The new certification requirements led to a demand for acceptable means of compliance and consequently the question about a way to safely demonstrate the remaining aircraft capabilities in flight for the case of SLD icing. These icing conditions can pose a high risk to the aircraft, crew and passengers, which requires a large effort to assure aircraft safety during flight test. Hence, it is mandatory to analyse the possible aircraft performance and control degradation introduced by SLD icing and also monitor the aircraft's remaining capabilities during the complete test flight. The distinct change of aircraft characteristics caused by SLD ice formation is not easy to predict and still topic of current aviation research. As the overall need for a better understanding of the SLD-icing effects on aircraft was identified as a research gap, a German nationally funded research project named SuLaDI (Supercooled Large Droplet Icing) was established between DLR and TU Braunschweig (2011–2016). In parallel, a joint research activity between DLR and Embraer was conducted between 2012 and 2016 to further investigate the icing degradation of aircraft in general but with a distinct view to SLD conditions. The major advantage of this research cooperation was the focus on flight test and flight data analysis with respect to different icing cases (App. C and App. O), which was not part of SuLaDI but is highly important to answer some questions about the distinct effects of icing on aircraft characteristics.

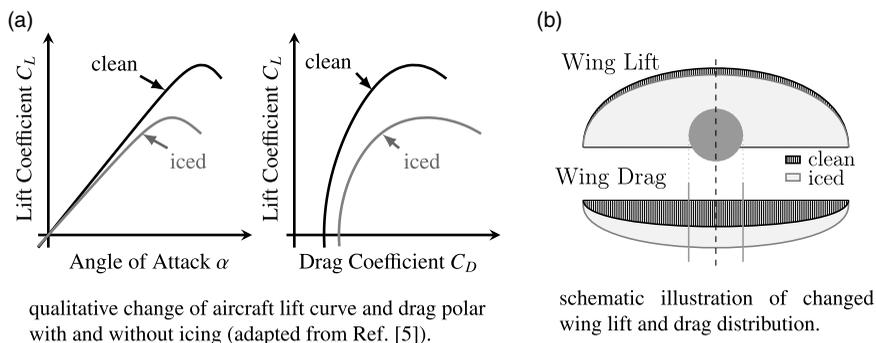


Figure 1. General expected aerodynamic degradation due to icing.



Figure 2. Embraer Phenom 300 test aircraft.

In general, during the flight through icing conditions, ice can accumulate on airframe parts facing the inflow e.g., wing or stabilizer leading edges, aircraft nose, engine intakes or sensors if these are not protected by any countermeasures. The main aerodynamic degradation is expected to be caused by wing ice accretions and manifests itself in a reduced stall angle-of-attack, reduced maximum lift and increased drag. These accumulations can form different shapes depending on e.g., atmospheric conditions and aircraft geometry. The general aerodynamic influence is outlined for example in the AGARD Report 344 [5] and given in Fig. 1a. Expectable changes of the lift and drag distributions are illustrated in Fig. 1b. In the past, these icing-effects had been investigated in various studies for different aerofoils and icing cases [5–7] as well as for the complete aircraft [8–11]. Furthermore, in case of asymmetric wing ice accretion, the reduced stall angle-of-attack can cause the aircraft to roll suddenly, and if stall occurs locally on one wing, a loss of control event might be the result. To obtain a better understanding of these icing effects on aircraft performance and dynamics, new aerodynamic models for nonlinear aircraft simulations have been developed [12, 13], which are based on a different approach than already existing models [14–17].

This paper shows the supplementary results of the joint DLR-Embraer research on aircraft icing which make a contribution to some of the key scientific aspects related to aircraft icing, e.g., aircraft operational limitations and behaviour with accumulated ice on various surfaces. It presents the approach used to analyse the degrading effects of icing with regard to certain SLD-ice configurations on a specific aircraft — a Phenom 300 prototype (see Fig. 2):

1. flight tests data analysis of Phenom 300 flights with artificial SLD-ice shapes, the related dynamic simulation model identification and the model comparison with App. C configuration results in Section 3;

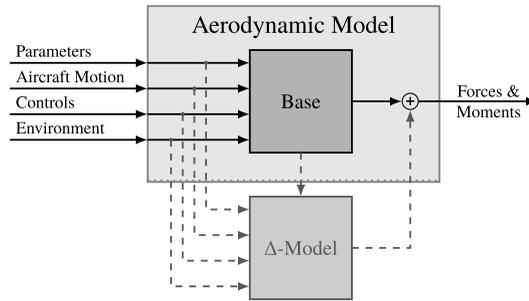


Figure 3. Aerodynamic model with Δ -model extension (from Ref. [13]).

2. comparison of icing effects, i.e. by an exemplary evaluation of change in aircraft performance (see Section 4), flight dynamics and handling qualities (see Section 5).

A summary and conclusions on the overall results are given in Section 6.

2.0 Modeling of icing effects in aircraft flight simulation

The aerodynamic Δ -model formulation which accounts for additional icing effects on aerodynamics is formulated as an extension of previously developed and validated simulation models for a specific aircraft. It enables to simulate the aerodynamic performance changes due to additional forces and moments related to icing, which are calculated by the Δ -model in parallel to the basic aircraft’s aerodynamics and summed up afterwards (see Fig. 3). During this process the Δ -model is directly connected to the basic aircraft’s aerodynamics to use information about the basic aerodynamics where necessary.

The basic idea of the model extension is to use linearly altered parameters for icing-induced aerodynamic changes in aircraft simulation. The application of such a parameter extension for the modelling of icing effects was first introduced by Bragg [14] around the turn of the millennium. An arbitrary model parameter P including a basic model part P_{base} and an additional Δ -model part ΔP_{ice} can be expressed as

$$P = (1 + k_p) \cdot P_{\text{base}} + d_p = P_{\text{base}} + \Delta P_{\text{ice}}, \tag{1}$$

with the additional factor k_p and the offset d_p to model the degraded aircraft aerodynamics. For an arbitrary aerodynamic model coefficient $C_{(\cdot)}$ depending on an extended parameter P this separation yields in general:

$$C_{(\cdot)}(P) = C_{(\cdot)}(P_{\text{base}} + \Delta P_{\text{ice}}) = \left(C_{(\cdot)}(P_{\text{base}}) \right)_{\text{base}} + \Delta \left(C_{(\cdot)}(P_{\text{base}} + \Delta P_{\text{ice}}) \right)_{\text{ice}}. \tag{2}$$

This coefficient separation can lead to various formulations of the Δ -model depending on the structure of the base aerodynamic model and therefore the considered aircraft. Moreover, the Δ -model structure may vary with the objectives of the later usage. The models presented in Refs. [13, 18] were used for the evaluations presented in this paper. For the the formulation of the aircraft’s equations of motion as well as the base aircraft aerodynamics, the reader is referred to Refs. [13, 18–20] and the publications referenced therein. A further description of the base aircraft model description, the specific flight test campaign for system identification data generation and the system identification results is given in Ref. [21].

3.0 Iced-aircraft simulation models

The main focus of today’s icing research lies on supercooled large droplets (SLD) icing. During the DLR-Embraer cooperation several models for different ice configurations on the Phenom 300 were



Figure 4. Schematic illustration of the App. C wing ice shape configurations: run-back ice (left) and leading-edge ice (right).



Figure 5. Schematic illustration of the artificial wing SLD-ice shapes (not to scale) used for all three SLD configurations.

developed. Initially, data of former test flights with two different artificial App. C ice configurations (see Fig. 4) were analysed [13]. The projects main focus was the the analysis of three different SLD-ice configurations on the Phenom 300. The definition of the SLD-ice shape was based on several assumptions [21]. These resulted in residual ice formations/shapes behind the protected areas as well as ice formations/shapes on unprotected airframe parts. Specific CFD calculations led to the determination of the specific SLD-ice shapes, which were further tested on a Phenom 300 model at TsAGI's T-128 dry air wind tunnel. The results of the Δ -model identification for the different investigated SLD-ice configurations are given in this paper.

3.1 Appendix O data analysis and model development

The definition process for the artificial SLD-ice shapes and together with the results of the dry-air wind tunnel tests are presented in Ref. [21]. The major results of the wind tunnel test campaign can be summarized as follows: the chordwise position of the SLD ice shape has a great impact on the icing-related aerodynamic degradation with reduced influence towards the trailing edge. The most severe degradation found during the wind tunnel test was

- a decrease of about 35% of the maximum lift coefficient;
- a drag increase of about 150%;
- a destabilizing shift of the neutral-point position equivalent to 8% of the reference chord.

Based on the wind tunnel results a position for the ridge ice shape close the to leading-edge was selected for flight-test. Figure 5 provides an illustration of this wing ice shape configuration. The decision was based on the fact that this configuration caused a similar level of maximum lift degradation compared to other tested configurations but guarantees sufficient aileron effectiveness at low angle-of-attack. With the definition of SLD-ice shapes and the flight clearance after the dry-air wind tunnel test with the Phenom 300 model, the flight test campaign was conducted in November 2015. The flight tests took also place at Embraer's flight test site in Gavião Peixoto. For the flight tests, artificial ice shapes were fabricated in full scale and glued to the aircraft skin. Three different aircraft configurations were foreseen for the flight test program:

1. Low-Risk SLD: Artificial ice on the radome, winglets and on the wing upper and lower surface except for the wing area around the ailerons (SLD 1).
2. Incremental SLD: Artificial ice on the radome, winglets and on the wing upper and lower surface including the wing area around the ailerons (SLD 2).
3. Nominal SLD: Artificial ice on the radome, engine pylons, winglets and on the wing upper and lower surface including the wing area around the ailerons (SLD 3).

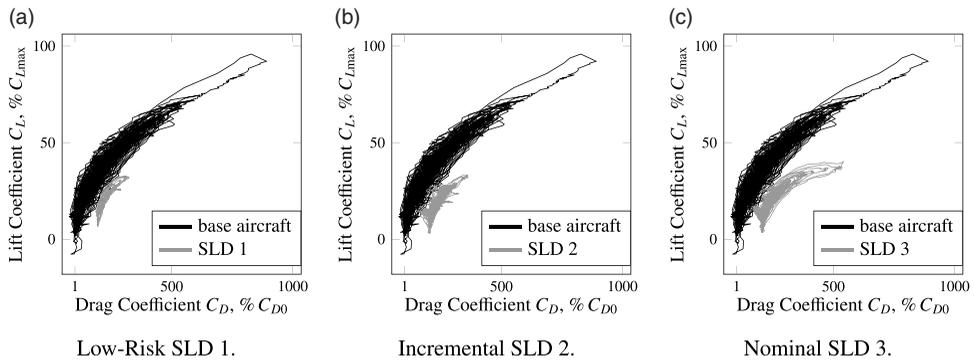


Figure 6. Drag polars computed from measurements as a result of flight test manoeuvres: clean aircraft (black) and specific SLD-ice configuration (gray). Data scaled to base aircraft max. lift coefficient (ordinate) and multiples of zero-lift drag (abscissa).

System identification manoeuvres were performed at three different altitudes (10,000, 15,000 and 20,000ft) and two different velocities (170 and 220kt). The flight test consisted of the same manoeuvres already performed with the clean aircraft for basic model identification [21]. The low speed limit of 170kt indicated airspeed was a result of the wind tunnel test analysis: an increase of the stall speed by a factor of nearly 1.3 for configurations with artificial ice shapes was detected and required the increase in stall margin. During all flights with the SLD-ice shapes a telemetry link was used to send the data to a ground station. Several online system identification tools [22] were operated for monitoring the aircraft characteristics during the whole flight on ground with live data. This way the crew was informed about the current flight characteristics of the aircraft at any time via a direct radio link.

For the first, low-risk SLD-ice flight 30 data segments with approximately 564s of flight time were available after the flight test. These contained necessary manoeuvres to identify parameters of the aerodynamic Δ -model. This first test flight was relatively short and manoeuvres were flown very carefully because the flight crew was concerned about potential degradations of the flight characteristics beyond the expectations, e.g., significantly reduced control surface effectiveness or premature stall. But the initial flight data analysis did not underpin these concerns. For example, the drag curve is calculated from the measured data and plotted together with base aircraft’s drag in Fig. 6a. Note that the data are proprietary and the plot ticks do not contain absolute values which does certainly not affect any results or conclusions.

There was no further restriction to follow the flight test program by another test flight with the incremental SLD configuration (SLD 2) having also ice shape attached in front of the ailerons. For parameter estimation 45 manoeuvres with a total recording time of approximately 1,365s were extracted from the flight data recordings. The drag curve is also calculated from the flight data recordings and plotted together with base aircraft’s drag in Fig. 6b. The third flight was performed with the nominal SLD-ice configuration, which additionally included ice shapes on the engine pylons. But with the pylons having only a minor effect on the aerodynamic (lift) performance of the aircraft, it could be assumed that the main difference to the second test flight (SLD 2) would be an increase in drag. The data used for the further analysis contain 51 segments with around 1,448s of recorded flight time. The calculated drag polar is shown in Fig. 6c.

With these different available flight data sets the Δ -model structure presented in Ref. [13] was again used to identify parameters which allow suitably representing the change in aircraft aerodynamics for the different SLD-ice configurations. For the SLD 1 and 2 configurations the already existing model structure was well applicable. But to cover the influence from the additional engine pylon ice shapes of the SLD 3 configuration, the Δ -model structure is extended with an additional drag increase $k_{C_{D0,pylon}}$:

$$\Delta C_{D,pylon} = C_{D0} \cdot k_{C_{D0,pylon}} \tag{3}$$

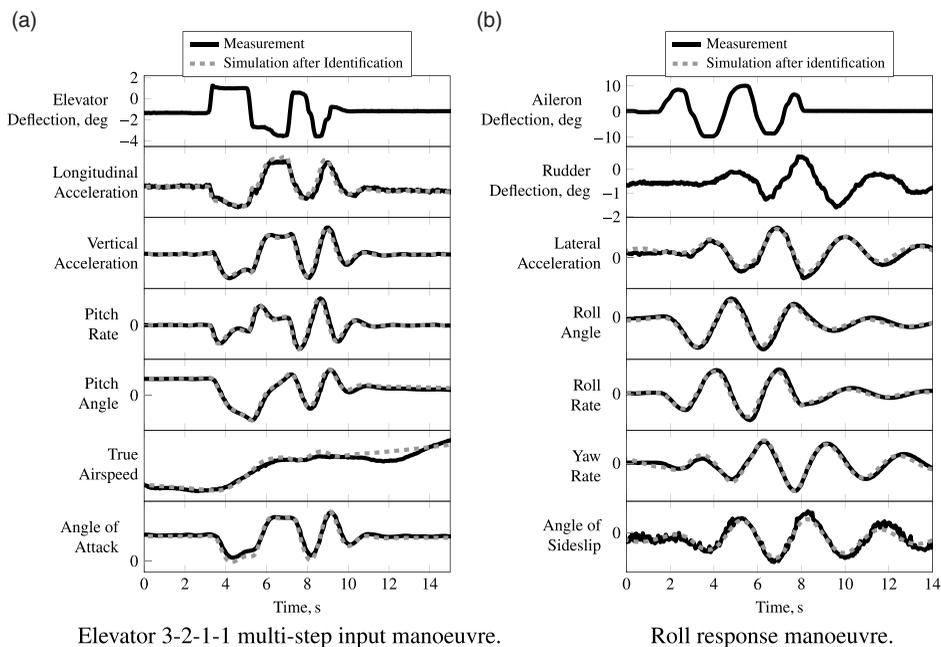


Figure 7. Time history comparison of identified nominal SLD aircraft model (SLD 3) simulation outputs and corresponding measurements for two example manoeuvres.

Before the post flight Δ -model identification was conducted, a sensor calibration check was done, verifying that the previously developed sensor models were still applicable to the flight test data. As an example of the models' quality time histories of two manoeuvres for SLD 3 configuration are given in Fig. 7: one longitudinal and one lateral dynamics manoeuvre. Similar results are obtained for the other two SLD-ice configurations. Time histories of the elevator 3-2-1-1 multistep input manoeuvre (see Fig. 7a) show a very good match of simulation after identification and measurements. Note that the difference in noticeable airspeed offset between measurement and simulation is very small; the whole airspeed variation during the manoeuvre is less than 2kt. After successful parameter estimation, the Δ -model allows to cover the significant changes of the aircraft characteristics. The time histories of an example roll response manoeuvre for SLD 3 configuration are given in Fig. 7b. These manoeuvres were performed during the flight test frequently at different airspeeds to check the available control surface effectiveness. After identification, the simulation matches these lateral manoeuvres also very well.

The estimates for the Δ -model parameters are given in Table 1 together with the values of the Cramér-Rao lower bounds of the final estimation iteration for all three SLD-ice configurations. Note that these parameter values directly reflect the aerodynamic changes for each SLD-ice configuration and are of high importance for further work like the definition of threshold values for indirect ice detection techniques based on changes of the aircraft characteristics [23]. Similar to the parameter estimates for the App. C configurations given in Ref. [13], some parameters had been fixed during the estimation, which is marked in the CRB column in the table. Note that some parameters were initially fixed and others were not estimated until the final estimation iteration. For example, the stall model parameter $k_{c1}^{1,2}$ was initially set to the given values similar to the process for the App. C configurations [13]. The parameter $k_{\alpha^*}^{1,2}$ was fixed during the system identification process. Moreover, as the SLD 3 configuration differs from SLD 2 only in the additional pylon ice shapes, several parameters were kept on the values estimated for SLD 2 during the SLD 3 model identification. It was assumed that these parameters should not vary between both configurations because there should be no effect of the engine pylon shapes on the overall aerodynamic characteristics covered by these coefficients. Furthermore, the system identification

Table 1. Estimated Δ -model parameters of investigated icing cases and the corresponding estimated Cramér-Rao lower bounds (CRB)

Parameter	SLD 1		SLD 2		SLD 3	
	Value	CRB [%]	Value	CRB [%]	Value	CRB [%]
$k_{c_1}^{1,2}$	1.000000	fixed	0.900000	fixed	0.900000	fixed
$k_{\alpha^*}^{1,2}$	-0.497302	fixed	-0.513100	fixed	-0.513100	fixed
$\alpha_{BP}^{1,2}$			0.1121 α^*	fixed	0.1121 α^*	fixed
$k_{C_{L0},low}^{1,2}$	-0.357171	0.12	-0.403737	0.14	-0.400392	0.05
$k_{C_{L\alpha},WB,low}^{1,2}$	-0.024975	0.61	-0.016434	3.25	-0.012650	0.92
$k_{C_{L\alpha},WB,high}^{1,2}$			0.055827	0.82	0.057401	0.31
$k_{C_{D0}}^{1,2}$	0.477353	0.06	0.489419	0.06	0.489419	fixed
$k_{C_{D0},pylon}$					0.039301	0.62
$k_{\frac{\partial C_D}{\partial \alpha}}^{1,2}$	-0.660067	0.24	-0.460703	0.34	-0.528558	0.08
$k_{C_{m0},WB}^{1,2}$	-0.598535	0.18	-0.896946	0.19	-0.896895	0.05
$k_{\frac{\partial C_m}{\partial \alpha}}^{1,2}$	-0.611956	0.12	-0.721821	0.34	-0.724465	0.06
$k_{C_{l\bar{\epsilon}}}$			-0.028111	2.17	-0.028111	fixed
$\frac{\Delta y_{Wing}^{1,2}}{\ y_{Wing,geo}^{1,2}\ }$	0.4490	0.33	0.5778	0.50	0.5778	fixed
$dy_{Wing}/d\beta$	1.001338	0.36	-0.527505	1.64	-0.527505	fixed

results for all three SLD-ice configurations show that the Δ -model is capable to match the changes of lateral aircraft dynamics in its given structure: in contrast to the App. C ice shape evaluation [13] no significant changes of lateral aerodynamics coefficients in the model are revealed. But there is a change of lateral force application point $\Delta y_{Wing}^{1,2}$ detectable between SLD 1 and SLD 2/3 configuration: the additional ice shape in front of the ailerons shift the force application point and therefore slightly changes the lateral behaviour of the aircraft. Similarly, due to the complex aerodynamics along the wing with ice shapes present, the force application point shifts with the angle of sideslip represented by $dy_{Wing}/d\beta$. The change of parameter value from low-risk to nominal SLD-ice configuration reflects the complex aerodynamics, which is also observed for the App. C configurations analysed in Ref. [13]. The relatively small values of the Cramér-Rao lower bounds indicate that the estimation problem was well posed and the choice of model parameters suitable for the model identification. Hence, although the Δ -model structure is relatively complex, it is able to well predict the aircraft aerodynamics for the different SLD-ice configurations with a little number altered model parameters.

3.2 Comparison of models

The resulting models were used to simulate the change in aircraft aerodynamics for comparison between the individual SLD configuration and with the App. C ice shapes. The results for each identified lift curve and drag polar are given in Fig. 8. For a more distinct view on the degradation this figure contains two zoom plots of the lift and drag curve on the right hand side. Basically, all noticeable changes of aircraft aerodynamics are similar with regard to aircraft lift and drag degradation. Furthermore, the changes of aerodynamics resulting from the different SLD-ice configurations are quite similar to the leading-edge ice shape degradation (App. C), except for the zero-lift drag increase. Although the ice shapes on the wings are much smaller than in the leading-edge App. C case, the SLD-ice configurations

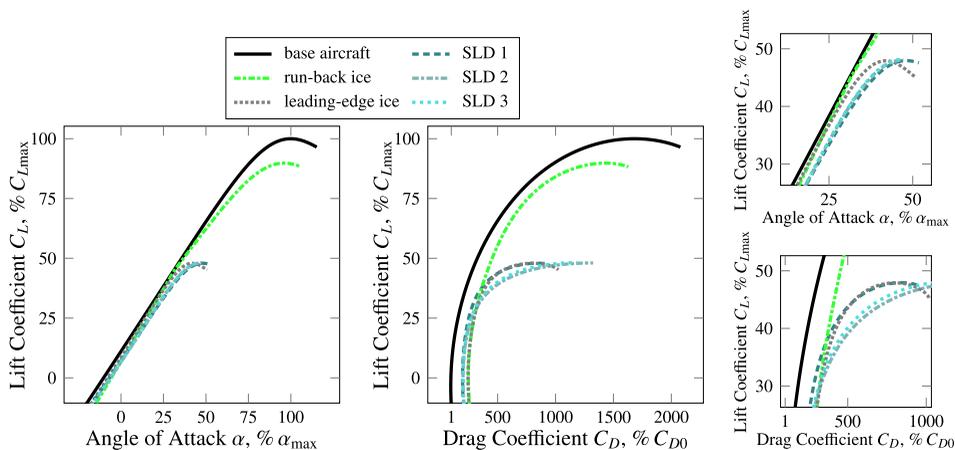


Figure 8. Changes of lift and drag curves for different ice cases; aerodynamic model data (after identification) for the light business jet aircraft. Right hand side: zoom plots for medium lift coefficients. Data scaled to base aircraft max. lift coefficient (ordinate), corresponding max. angle of attack (abscissa), and multiples of zero-lift drag (abscissa).

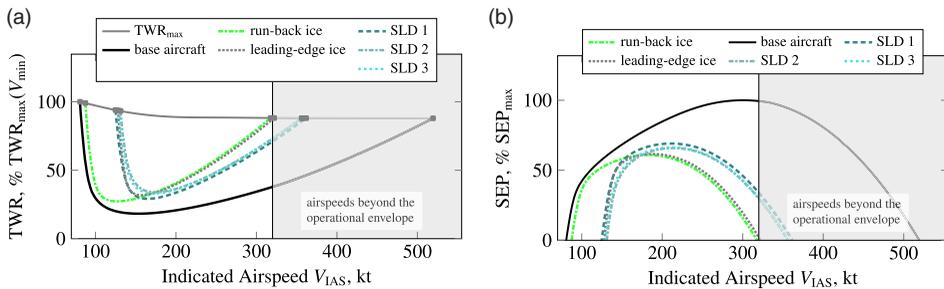
show a significant degradation of aircraft aerodynamics and can be also detrimental for a safe aircraft operation.

The three models for each SLD-ice reflect the slightly different aircraft characteristics for each configuration, which can be also seen in the parameters listed in Table 1. The detectable drag change of the SLD 1 configuration is about 95% of the base aircraft's zero lift drag with a stronger curvature of the drag polar. Further, a only slight lift curve slope reduction of 2% was estimated. The premature flow separation at angles of attack far below the base aircraft's maximum angle-of-attack is similar to the behaviour detected for the leading-edge ice case. For the incremental ice configuration (SLD 2) with additional ice shapes in front of the ailerons the lift curve reveals a slightly nonlinear behaviour with a kink at an angle-of-attack of around 4deg. This might result from the additional ice shapes on the wing tip disturbing the flow over the wing and therefore influencing the whole aircraft's lift characteristics. The predicted stall behaviour of the aircraft with this ice configuration is similar to SLD 1. The estimated drag increase reflects the effect of the additional ice shapes: zero-lift drag increases about 98% and the drag polar shows a stronger curvature. The SLD 3 configuration differs from SLD 2 only by the additional ice shapes on the engine pylons. Therefore, there are no significant changes in the lift characteristics detectable during the model identification compared to SLD 2, neither lift slope nor non-linear behaviour representing the wing flow separation. But the pylons also produce vertical forces and a slight change of the aircraft pitching moment was detected during the identification. The zero-lift drag increases by 4% and is accompanied by a slight reduction of the drag polar curvature.

The analysis of lateral aerodynamics revealed a change in the aircraft roll and yaw behaviour for all configurations, which directly affects the aircraft roll mode and Dutch roll. But only a small reduction of the aileron efficiency (2%) was found in the data analysis for SLD 2 and 3 configurations. These results are backed-up by pilots' reports after the campaign: no significant change in relevant aircraft dynamics and handling qualities to safely operate the aircraft were noticeable during the flight.

4.0 Limitations of aircraft flight performance

The main influence of icing on a fixed-wing aircraft is the limitation of its flight performance. It constrains the possible aircraft operations, i.e. the aircraft range and endurance and/or the available speed



Required thrust-to-weight ratio (TWR_{req}) in comparison to maximum available TWR . Data scaled to maximum available TWR at minimum achievable speed V_{min} .

Specific excess power (SEP). Data scaled to maximum available SEP of base aircraft.

Figure 9. Limited flight performance under icing conditions: required thrust-to-weight ratio and specific excess power; exemplary results for base aircraft and the five different ice cases in 10,000ft altitude.

range. The flight performance degradation is mainly affected by the increasing drag with ice accretion present on the wing. Consequently, the lift-to-drag ratio

$$L/D = \frac{C_L}{C_D}, \tag{4}$$

which is a suitable parameter to describe an aircraft’s aerodynamic performance, decreases with stronger ice influence. Its change emerges directly from the different shapes of the lift and drag coefficient curves, and L/D can quantify the performance loss for a given ice shape at a certain flight point. But for all aircrafts (except sailplanes) the correlation of loss in L/D and the required/available thrust is of greater interest, because then the operational limits of the aircraft are revealed.

Therefore the required thrust-to-weight ratio

$$TWR_{req} = \frac{T_{req}}{m_{AC} \cdot g}, \tag{5}$$

for a steady horizontal flight is analysed and compared to

$$TWR_{max} = \frac{T_{max}}{m_{AC} \cdot g}, \tag{6}$$

which denotes the maximum available thrust-to-weight ratio at the given flight point and limits the (steady) aircraft envelope. The difference between the required and maximum available thrust-to-weight ratio determines to the specific excess power SEP [24]

$$SEP = \frac{(T_{max} - T_{req}) \cdot V_{TAS}}{m_{AC} \cdot g} = (TWR_{max} - TWR_{req}) \cdot V_{TAS}, \tag{7}$$

which is equivalent to the maximum available climb rate at a given speed and altitude.

DLR’s Matlab tool “MAPET” (Model-based Aircraft Performance Evaluation Tool) [25] is used with both simulation models and the different available wing ice configurations for flight performance analysis. Based on trimmed flight conditions the tool evaluates several model in- and outputs and calculates the desired flight performance parameters. A complete flight performance analysis was performed for numerous altitudes and aircraft masses and gave well comparable results in all cases. Figure 9 contains analysis results for one example altitude (10,000ft), which represent well the region of the normal flight envelope where icing mainly occurs. Moreover, the results presented herein are exemplary for an aircraft mass of 7,500kg and an aircraft configuration with flaps clean and gear up. Figure 9 illustrates change of thrust-to-weight ratio (left side) and specific excess power (right side) versus indicated airspeed (base

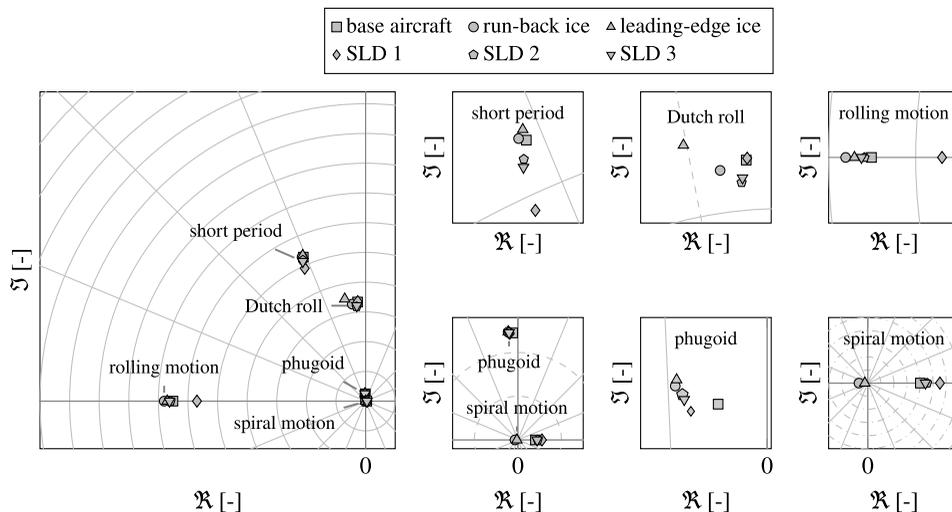


Figure 10. Ice-induced change of aircraft dynamics: exemplary locations of roots in complex plane for the aircraft model with and without icing; at 175kt in 10,000ft.

aircraft and five ice configurations). The required thrust-to-weight ratio significantly increases for indicated airspeeds above 200kt in all ice cases. Because of the well comparable identified increase in zero-lift drag for the three SLD-ice configurations the maximum achievable airspeed is very similar for these cases and far below the base aircraft's limitation but above the maximum achievable airspeed for the App. C ice case. This result reflects the identified aerodynamics (see Fig. 8) and hence the expected degradations for the SLD configurations. The icing-induced premature stall behaviour, particularly in case of the SLD-ice configurations and the leading-edge ice, the corresponding drag increase cause also a restriction of the minimum airspeed which could be theoretically achieved in steady flight with the available engine thrust. But nevertheless, the aircraft can still be operated within its safe envelope. In the medium speed range, the TWR_{req} -increase leads to a noticeable reduction of SEP in Fig. 9b, which is in accordance with the expectations from literature [5, 17, 26, 27] and reported occurrences in the past [3, 28–30].

All in all, these results regarding the aircraft flight performance under icing influence meet the general expectations concerning the aircraft degradation. A final comparison of the icing-related parameter changes for all ice configurations reveal a homogeneous degrading effect. These results are not surprising and well known, since pilots and engineers have been familiar with the phenomenon of icing for decades.

5.0 Changes in flight dynamics

The aerodynamic degradation caused by icing has an influence on the aircraft's dynamic behaviour. But, the specific effects on longitudinal and especially lateral motion are dependent on the magnitude of degradation and the location of the corresponding ice shape. To compare icing-induced changes of a certain ice configuration to another and to the basic aircraft it is suitable to analyse the characteristics of the dynamic modes. Therefore, the aircraft is trimmed in open loop and linearized at a certain flight condition, and the eigenvalues of the state matrix are calculated. The analysis of the corresponding eigenvectors allows mapping the roots to each dynamic mode. The location of roots in the complex plane further allows to reveal the icing-induced changes of the specific dynamic mode's frequency and damping.

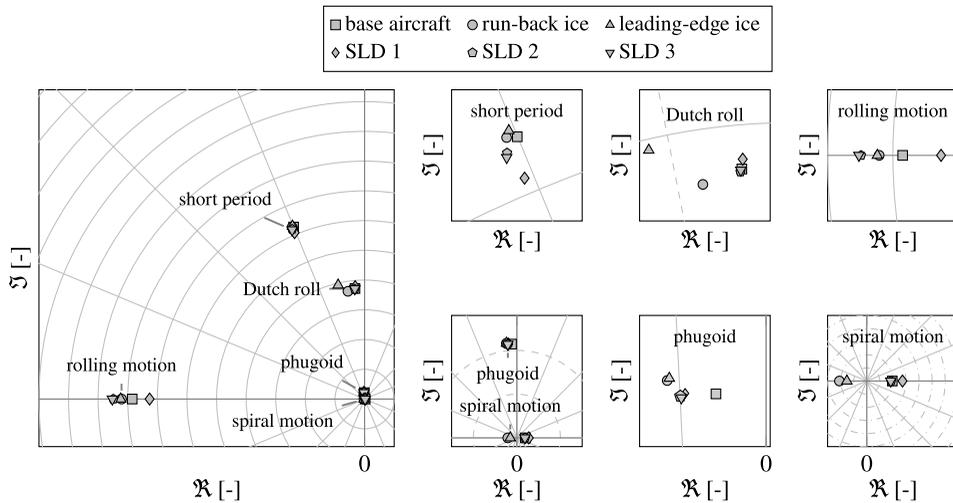


Figure 11. Ice-induced change of aircraft dynamics: exemplary locations of roots in complex plane for the aircraft model with and without icing; at 200kt in 10,000ft.

5.1 Evaluation of dynamic modes

As an example, the different aircraft configurations (without and with icing influence, flaps clean and gear up) are trimmed at 10,000ft with identical airspeed. To obtain results which are comparable to the previous flight performance analysis in Section 4 similar aircraft weight-and-balance configurations are used. Figure 10 illustrates the changes of roots in the complex plane for the Phenom 300 for all five investigated ice configurations and an indicated airspeed of 175kt. Similar plots of the changes of roots due to icing are given in Fig. 11 for an indicated airspeed of 200kt.

For the investigated ice configurations only a slight influence on the short period characteristics is noticeable. The App. C configurations (run-back and leading-edge ice) do not show a significant deterioration of the short period dynamics [13, 31, 32] whereas the SLD-ice configurations reveal a slightly different behaviour. The SLD-ice configurations show a change of pitching characteristics compared to the classical App. C cases and the clean aircraft in terms of an increase of damping and decrease of natural frequency (see zoom plots in Figs. 10 and 11). The ridge-ice shapes representing the SLD-ice configurations change the pitching moment of the aircraft which is well represented by the models. It is further interesting that the low-risk SLD 1 configuration (with no ice shapes attached on the outer wing sections) show a more significant change of short period dynamics than the other two SLD-ice configurations tested. Note that the models are identified from the actually measured flight data with manoeuvres flown at flight conditions very close the ones presented for this evaluation herein. Therefore, there is a high confidence that the identified models will correctly represent the flight dynamics (see also results in Section 3). Nevertheless, the distinct cause of this finding cannot be revealed with the information about the complex flow on the iced wing available for this work.

The phugoid mode is significantly affected by all ice configurations. The zoom plots in Figs. 10 and 11 show that the corresponding roots of all ice configurations move away from the base aircraft’s eigenvalue similar for both airspeeds: the significant drag increase due to the ice shapes changes the aircraft’s lift-to-drag ratio and therefore the phugoid characteristics. The phugoid damping can be approximated by

$$\zeta_{PH} \approx \frac{1}{\sqrt{2} \cdot (L/D)}, \tag{8}$$

whereas the natural frequency is mainly airspeed dependent [33].

The analysis further reveals interesting changes of lateral aircraft mode characteristics for the evaluated ice configurations. The mode characteristics changes are inhomogeneous for different SLD-ice

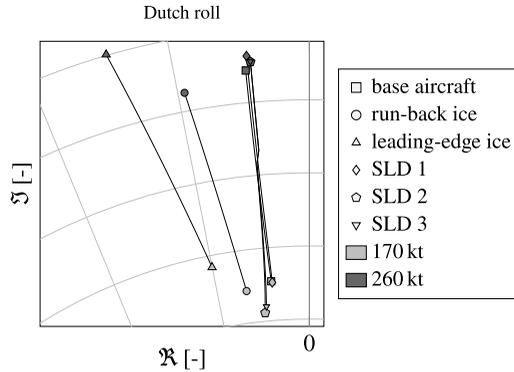


Figure 12. Ice-induced change of aircraft dynamics, Dutch roll root locus: exemplary change of location of roots in complex plane for the clean aircraft and five different ice configurations between 170 and 260kt indicated airspeed in 10,000ft.

configurations and also not similar to the results for the App. C cases (see also Refs. [31, 32]). The rolling mode root moves away from the origin due to a higher aerodynamic damping for the App. C cases, which can be attributed to changes in lift characteristics: increase of lift curve slope at distinct angles of attack compared to the base aircraft (see Fig. 8). For the SLD-ice configurations the change of roll damping is less and different to the App. C cases: lift characteristics change in a different manner with a slight decrease of lift slope at lower angles of attack and a slight increase above the break point for SLD 2 and 3 as given in Section 3. Hence, the change of roll damping is dependent on airspeed for the incremental and nominal SLD-ice configuration: roll damping increase for lower angles of attack, roll damping decrease for higher angles of attack compared to the base aircraft. The SLD 1 configuration shows a decrease of roll damping for the investigated airspeeds.

The Dutch roll becomes better damped for the App. C configurations, which can be attributed to the local drag increase on the wing and the consequent increase of yaw damping N_r :

$$\zeta_{DR} \approx -\frac{1}{2} \frac{N_r}{N_\beta} \tag{9}$$

For the SLD-ice configurations the dynamic analysis results show a different picture: the Dutch roll root locus changes although the roots for the SLD-ice configurations lie much closer to clean aircraft root than for the classical App. C cases. Figure 12 shows the Dutch roll root locus for indicated airspeeds between 170 and 260kt in 10,000ft. Although the drag increases also for all three SLD-ice configurations, the increase is not as strong as for the investigated App. C cases and consequently the ratio between the yaw damping N_r and directional stability N_β in Equation (9) is affected differently. During the identification, there was no additional increase of yaw damping $k_{C_{n\beta}}$ found as it was identified for the App. C cases [13]. Moreover, as the Dutch roll motion is a coupling of yawing and rolling motion the changes in roll characteristics for the SLD-ice configuration further contribute to the visible change of the Dutch roll root locus.

Furthermore, the change of aircraft’s spiral mode shows a similar picture: it is stabilized for the App. C cases and the root locus is again changed differently for the SLD-ice configurations. The spiral mode is stable (see Ref. [33] for further explanation) if

$$N_r L_\beta - N_\beta L_r > 0. \tag{10}$$

For the App. C cases the yaw damping N_r is increased and L_β is enhanced due to the reduced sensitivity of the aircraft’s local lift to a local angle of attack change which consequently results in a reduced rolling moment/motion. Similar to the change of the Dutch roll mode the spiral mode change shows also an inhomogeneous result: the SLD 1 configuration reveals a destabilized spiral mode for all investigated

Table 2. Comparison of relative aircraft dynamic mode change: Phenom 300 for different ice configurations (\Uparrow strong increase, \Downarrow strong decrease, \Uparrow increase, \Downarrow decrease, $\not\rightarrow$ change of root locus).

Dynamic mode		App. C		App. O		
		run-back	leading-edge	SLD 1	SLD 2	SLD 3
Phugoid	ζ_{PH}	\Uparrow	\Uparrow	\Uparrow	\Uparrow	\Uparrow
Short period	ζ_{SP}	\Uparrow	\Uparrow	\Uparrow	\Uparrow	\Uparrow
	$\omega_{0,SP}$	\Downarrow	\Uparrow	\Downarrow	\Downarrow	\Downarrow
Dutch roll	ζ_{DR}	\Uparrow	\Uparrow	\Downarrow	$\not\rightarrow$	$\not\rightarrow$
	$\omega_{0,DR}$	\Downarrow	\Uparrow	\Uparrow	$\not\rightarrow$	$\not\rightarrow$
Rolling motion	T_{RO}	\Downarrow	\Downarrow	\Uparrow	$\not\rightarrow$	$\not\rightarrow$
Spiral motion	T_{SR}	Stabilized		\Downarrow	$\not\rightarrow$	$\not\rightarrow$

airspeeds compared to the base aircraft whereas the change is airspeed dependent for the other two configurations. The spiral mode is dependent on the yawing and rolling characteristics similar to the Dutch roll for which reason the change of aerodynamic characteristics is the cause of the visible effects. There is no strong change of yaw damping as for the App. C cases and the roll characteristics are not affected sufficiently – and in a right manner – to e.g., stabilize the spiral mode. Nevertheless, the spiral mode change is not critical and does not affect safe aircraft operations although getting more unstable for the low-risk SLD-ice configuration.

The combination of aircraft models and ice configurations show different results concerning the icing influence on the aircraft flight dynamics. Table 2 contains a comparison of the change of the aircraft characteristics. The phugoid shows a well comparable behaviour for the different ice configurations due to the strong effect on its damping by the drag increase respectively reduced lift-to-drag ratio. Although the effect on the short period damping ζ_{SP} seems to be homogeneous, the change itself is very small and might be different for other aircraft as given in Refs. [31, 32]. Moreover, the change of lateral motion characteristics is different for the five investigated ice configurations.

Changing the flight condition to different altitudes gives similar results: the roots generally change according to the expected behaviour with the corresponding change of flight condition. All in all, the evaluation results reveal a direct correlation of icing-induced changes of aircraft dynamics on the specific aerodynamic degradation. Therefore, no general statement about the change of aircraft dynamics under icing influence can be made based on the presented results. Hence, it is further not possible to make a verification of existing methods to detect icing based on a changed aircraft dynamic behaviour [34–37].

5.2 Handling qualities assessment

The change of aircraft dynamics under icing influence could lead to an alteration of handling qualities. Several numerical criteria given in “MIL-STD-1797A” (38) are directly based on the aircraft’s mode characteristics (damping, natural frequency, time constant). Therefore, the evaluation of these criteria delivers a first but limited¹ impression of the icing influence on handling qualities. The Phenom 300 can be categorized as class II (light or medium transport) and the handling qualities are evaluated for category B and C operations. The evaluation reveals that the analysed icing-induced changes of aerodynamics have no significant – especially no significant negative – effect on the aircraft’s handling qualities. Table 3 gives an overview of the resulting handling qualities assessment based on the analysed numerical criteria for the eigenvalues of the linearised dynamic system.

¹ Only focused on open-loop aircraft control, which plays only a secondary role in normal operation of modern aircraft

Table 3. Comparison of handling qualities based on numerical criteria (class II, categories B & C): Phenom 300 for different ice configurations at 10,000ft and airspeeds between 170 and 260kt; all criteria for base aircraft are level 1

Numerical criterion	App. C		App. O		
	run-back	leading-edge	SLD 1	SLD 2	SLD 3
Phugoid damping	Level 1	Level 1	Level 1	Level 1	Level 1
Short period damping	Level 1	Level 1	Level 1	Level 1	Level 1
Dutch roll damping natural frequency	Level 1	Level 1	Level 1*	Level 1	Level 1
Rolling motion time constant	Level 1	Level 1	Level 1	Level 1	Level 1
Spiral motion time to double	(Level 1)	(Level 1)	Level 1	Level 1	Level 1

*Change to level 2 for low airspeeds.

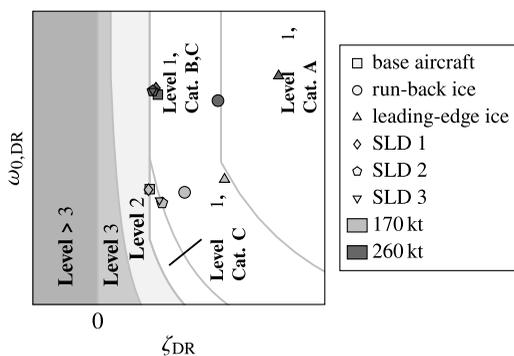


Figure 13. Ice-induced change of aircraft dynamics, Dutch roll handling qualities assessment: exemplary change of natural frequency and damping on the numerical criteria map for the clean aircraft and five different ice configurations in 10,000ft and indicated airspeeds of 170 and 260kt; without yaw damper.

In detail: the phugoid damping increases for all investigated ice configurations due to the higher drag. Therefore, level 1 handling qualities are not affected. Furthermore, the short period damping is not significantly changed for the different ice configurations and consequently the level 1 rating persists. The aircraft showed some interesting changes of the lateral motion characteristics for the different ice configurations (see Table 2). The effects on the rolling motion are different in terms of change of the time constant T_{RO} , but the numerical criterion evaluation does still result in a level 1 assessment for all analysed airspeeds. Figure 12 shows the change of Dutch roll root locus for SLD-ice which is different from the effects caused by the App. C ice shapes. To evaluate the corresponding influence on the aircraft's handling qualities the Dutch roll damping and natural frequency are plotted on the numerical criteria map in Fig. 13 for 170 and 260kt indicated airspeed. In contrast to the App. C ice configurations, where the distance to the level 2 boundary is enlarged, the SLD-ice configurations are close to the base aircraft values and therefore the level 2 boundary. For low airspeeds this boundary is even crossed in case of the low-risk SLD-ice configuration. The spiral mode is also affected differently by the five ice configurations: it is stabilized by the App. C ice configurations, destabilized by the low-risk SLD-ice and shows a change of root locus for SLD 2 and 3. Hence the corresponding handling qualities criterion based on the time to double is not applied for the App. C configurations and the assessment results in level 1. Although the SLD-ice configurations change respectively destabilize the spiral mode characteristics a level 1 rating is still obtained. All in all, the handling qualities of the Phenom 300 do not show a significant or not-manageable degradation with all investigated ice cases.

6.0 Conclusion

The influence of icing on aircraft characteristics of a Phenom 300 was analysed and is presented in this paper. Different ice configurations – two classical App. C as well as three specific SLD-ice (App. O) configurations – were evaluated as a result of a joint DLR-Embraer research activity. Furthermore, the results of the model identification for these three different SLD-ice configurations are given herein. The individual model evaluation revealed that the effects of the SLD-ice configurations followed the expectations but of course differ from App. C influence. Nevertheless, the significant drag increase at even lower angles of attack showed the risk for aircraft operation resulting from such ice formations. A homogeneous icing-induced degradation of flight performance parameters was found, which is mainly related to the uniform change of lift-to-drag ratio with ice present on the aircraft: for all five investigated ice configurations a significant drag increase was found and the flight performance was consequently degraded as expected. In contrast, the analysis for the Phenom 300 revealed that the changes of flight dynamics are case-dependent. Especially for the SLD-ice configurations a change of root locus for the lateral motion eigenmodes was detected.

However, within this work no general conclusions on the effects on aircraft dynamics can be drawn for the following reasons: only one specific aircraft with a limited number of distinct ice configurations was evaluated in this study and the results are inconclusive; the changes of the aircraft's dynamic modes are a consequence of the change of local aircraft aerodynamics which is different for different ice configurations. Therefore, no general conclusion on the icing-induced change of aircraft dynamics could be drawn. These new results complement existing work, which showed different results for other ice configurations on different aircraft (simulation models).

Nevertheless, the icing-related strong increase of drag and its further consequences could be found in aircraft performance and dynamic characteristics for the investigated App. C and SLD-ice configurations. Moreover, the exemplary evaluation of numerical handling qualities changes for the investigated flight conditions did not show any significant deterioration. The high-quality simulation models – especially for the investigated SLD-ice configurations – are contributing to the general understanding of the icing influence on aircraft characteristics. However, further information about the effects of additional ice configurations on different aircraft would be beneficial for future work.

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References

- Green, S.D. A study of U. S. inflight icing accidents and incidents, 1978 to 2002. Number AIAA 2006-82, Reno, Nevada, USA, January 9th – 12th, 2006, 44th AIAA Aerospace Sciences Meeting and Exhibit, American Institute of Aeronautics and Astronautics, Inc. (AIAA). doi: [10.2514/6.2006-82](https://doi.org/10.2514/6.2006-82).
- Green, S.D. The icemaster database and an analysis of aircraft aerodynamic icing accidents and incidents, Technical Report DOT/FAA/TC-14/44, R1, Federal Aviation Administration, Atlantic City, NJ, USA, October 2015.
- Anon. *Final Report (BFU 5X011-0/98)*. German Federal Bureau of Aircraft Accident Investigation, Braunschweig, Germany, April 2001.
- Anon. *Aircraft Accident Report (NTSB/AAR-96/01, DCA95MA001)*, Safety Board Report. National Transportation Safety Board (NTSB), Washington, DC, USA, July 9th 1996.
- Anon. Ice accretion simulation. AGARD Advisory Report 344, Advisory Group for Aerospace Research & Development (AGARD) – Fluid Dynamics Panel Working Group 20, North Atlantic Treaty Organization (NATO), Neuilly-Sur-Seine, France, December 1997.
- Gray, V.H. Prediction of aerodynamic penalties caused by ice formations on various airfoils, Technical Note D-2166, National Aeronautics and Space Administration (NASA), Washington, D.C., USA, February 1964.
- Broeren, A.P., Whalen, E.A., Busch, G.T. and Bragg, M.B. Aerodynamic simulation of runback ice accretion, *J. Aircr.*, 2010, **47**, (3), pp 924–939. doi: [10.2514/1.46475](https://doi.org/10.2514/1.46475).
- Ranuado, R.J., Batterson, J.G., Reehorst, A.L., Bond, T.H. and O'Mara, T.M. Determination of longitudinal aerodynamic derivatives using flight data from an icing research aircraft, Number AIAA 89-0754, Reno, Nevada, USA, January 9th - 12th, 1989, 27th AIAA Aerospace Sciences Meeting, American Institute of Aeronautics and Astronautics, Inc. (AIAA), 1989. doi: [10.2514/6.1989-754](https://doi.org/10.2514/6.1989-754).

9. Ratvasky, T.P. and Ranuado, R.J. Icing effects on aircraft stability and control determined from flight data. preliminary results, Number AIAA 93-0398, Reno, Nevada, USA, January 11th - 14th, 1993. 31st AIAA Aerospace Sciences Meeting and Exhibit, American Institute of Aeronautics and Astronautics, Inc. (AIAA), 1993. doi: [10.2514/6.1993-398](https://doi.org/10.2514/6.1993-398).
10. Lee, S., Barnhart, B.P. and Ratvasky, T.P. Dynamic wind-tunnel testing of a sub-scale iced S-3B viking, Number AIAA 2010-7986, Toronto, Ontario, Canada, August 2nd - 5th, AIAA Atmospheric and Space Environments Conference, American Institute of Aeronautics and Astronautics, Inc. (AIAA), 2010. doi: [10.2514/6.2010-7986](https://doi.org/10.2514/6.2010-7986).
11. Gingras, D.R. Requirements and modeling of in-flight icing effects for flight training, Number AIAA 2013-5075, Boston, Massachusetts, USA, August 19th - 22th. AIAA Modeling and Simulation Technologies (MST) Conference, American Institute of Aeronautics and Astronautics, Inc. (AIAA), 2013. doi: [10.2514/6.2013-5075](https://doi.org/10.2514/6.2013-5075).
12. Deiler, C. Time domain output error system identification of iced aircraft aerodynamics, *CEAS Aeronaut. J.*, 2017, **8**, (2), pp 231–244. doi: [10.1007/s13272-016-0231-2](https://doi.org/10.1007/s13272-016-0231-2).
13. Deiler, C. Aerodynamic modeling, system identification, and analysis of iced aircraft configurations, *J. Aircr.*, 2018, **55**, (1), pp 145–161. doi: [10.2514/1.C034390](https://doi.org/10.2514/1.C034390).
14. Bragg, M.B., Hutchison, T., Merret, J., Oltman, R. and Pokhariyal, D. Effect of ice accretion on aircraft flight dynamics, Number AIAA 2000-0360, Reno, Nevada, USA, January 10th - 13th, 2000. 38th AIAA Aerospace Sciences Meeting and Exhibit, American Institute of Aeronautics and Astronautics, Inc. (AIAA), 2000. doi: [10.2514/6.2000-360](https://doi.org/10.2514/6.2000-360).
15. Brown, A.P. Negative speed stability, a factor in transport airplane icing upsets, Number AIAA 2002-3051, St. Louis, Missouri, USA, June 24th - 26th 2002, 20th AIAA Applied Aerodynamics Conference, American Institute of Aeronautics and Astronautics, Inc. (AIAA), 2002. doi: [10.2514/6.2002-3051](https://doi.org/10.2514/6.2002-3051).
16. Deters, R.W., Dimock, G.A. and Selig, M.S. Icing encounter flight simulator, *J. Aircr.*, 2006, **43**, (5), pp 1528–1537. doi: [10.2514/1.20364](https://doi.org/10.2514/1.20364).
17. Lampton, A. and Valasek, J. Prediction of icing effects on the dynamic response of light airplanes, *J. Guid. Cont. Dyn.*, 2007, **30**, (3), pp 722–732. doi: [10.2514/1.25687](https://doi.org/10.2514/1.25687).
18. Deiler, C. and Kilian, T. Dynamic aircraft simulation model covering local icing effects, *CEAS Aeronaut. J.*, 2018, **9**, (3), pp 429–444. doi: [10.1007/s13272-018-0291-6](https://doi.org/10.1007/s13272-018-0291-6).
19. Fischenberg, D. A method to validate wake vortex encounter models from flight test data, Nice, France, September 19th - 24th 2010. 27th International Congress of the Aeronautical Sciences, International Council of the Aeronautical Sciences (ICAS). http://www.icas.org/ICAS_ARCHIVE/ICAS2010/PAPERS/041.PDF.
20. Jategaonkar, R. *Identification of the Aerodynamic Model of the DLR Research Aircraft ATTAS from Flight Test Data*. DLR-FB 90-40. Deutsche Forschungsanstalt für Luft- und Raumfahrt e. V. (DLR), Cologne, Germany, September 1990.
21. Deiler, C., Ohme, P., Raab, C., Mendonca, C. and Silva, D. Facing the challenges of supercooled large droplet icing: Results of a flight test based joint DLR-embraer research project, *SAE Int. J. Adv. Curr. Pract. Mob.*, 2020, **2**, (1), pp 192–204. ISSN 2641-9637. doi: [10.4271/2019-01-1988](https://doi.org/10.4271/2019-01-1988).
22. Raab, C., Ohme, P. and Deiler, C. Support of icing flight tests by near real-time data analysis, *CEAS Aeronaut. J.*, 2017, **8**, (4), pp 561–577. doi: [10.1007/s13272-017-0260-5](https://doi.org/10.1007/s13272-017-0260-5).
23. Deiler, C. and Fezans, N. Performance-based ice detection methodology. *J. Aircr.*, 2020, **57**, (2), pp 209–223. doi: [10.2514/1.C034828](https://doi.org/10.2514/1.C034828).
24. Phillips, W.F. *Mechanics of Flight*. John Wiley & Sons, Inc., Hoboken, New Jersey, USA, 2004. ISBN 9780471334583.
25. Ohme, P. and Raab, C. A model-based approach to aircraft performance assessment. Honolulu, Hawaii, USA, August 18th - 21st, 2008. AIAA Atmospheric Flight Mechanics Conference and Exhibit, American Institute of Aeronautics and Astronautics, Inc. (AIAA), 2008. doi: [10.2514/6.2008-6873](https://doi.org/10.2514/6.2008-6873).
26. Ranuado, R.J., Mikkelsen, K.L., McKnight, R.C. and Perkins Jr., P.J. Performance degradation of a typical twin engine commuter type aircraft in measured natural icing conditions, Reno, Nevada, USA, January 9th - 12th, 1984. 22nd AIAA Aerospace Sciences Meeting, American Institute of Aeronautics and Astronautics, Inc. (AIAA), 1984. doi: [10.2514/6.1984-179](https://doi.org/10.2514/6.1984-179).
27. Whalen, E.A., Lee, S., Bragg, M.B. and Ratvasky, T.P. Characterizing the effect of ice on aircraft performance and control from flight data, Reno, Nevada, USA, January 14th-17th, 2002, 40th AIAA Aerospace Sciences Meetings and Exhibit, American Institute of Aeronautics and Astronautics, Inc. (AIAA), 2002.
28. Anon. *Report On Serious Incident (AIBN/Rep. 2009/02)*. Accident Investigation Board Norway (AIBN), Lillestrøm, Norway, January 2009.
29. Anon. *Accident Report (BFU EX001-0/00) [in German]*. German Federal Bureau of Aircraft Accident Investigation, Braunschweig, Germany, October 2002.
30. Anon. *Aircraft Incident Report (EW/G2014/10/04)*, *AAIB Bulletin: 9/2015. Air Accidents Investigation Branch (AAIB)*, Department of Transport, Farnborough, UK, September 2015.
31. Deiler, C. Flight characteristics of iced aircraft, AIAA Scitech Forum, San Diego, California, USA, January 7th - 11th, 2019. American Institute of Aeronautics and Astronautics, Inc. (AIAA), 2019. doi: [10.2514/6.2019-0560](https://doi.org/10.2514/6.2019-0560).
32. Deiler, C. Comparison of flight characteristics of two different airplanes and ice configurations, *J. Aircr.*, 2020, **57**, (5), pp 995–1000. doi: [10.2514/1.C035801](https://doi.org/10.2514/1.C035801).
33. Yechout, T.R. *Introduction to Aircraft Flight Mechanics*, American Institute of Aeronautics and Astronautics, Inc., Reston, Virginia, USA, 2 Ed., 2014.
34. Myers, T.T., Klyde, D.H. and Magdaleno, R.E. The dynamic icing detection system (dids), Reno, Nevada, USA, January 10th - 13th, 1999. 38th AIAA Aerospace Sciences Meeting and Exhibit, American Institute of Aeronautics and Astronautics, Inc. (AIAA), 1999. doi: [10.2514/6.2000-364](https://doi.org/10.2514/6.2000-364).

35. Melody, J.W., Hillbrand, T., Başar, T. and Perkins, W.R. H_{∞} parameter identification for inflight detection of aircraft icing: The time-varying case, *Cont. Eng. Pract.*, 2001, 9, (12), pp 1327–1335. doi: [10.1016/S0967-0661\(01\)00081-8](https://doi.org/10.1016/S0967-0661(01)00081-8).
36. Bragg, M.B., Başar, T., Perkins, W.R., Selig, M.S., Voulgaris, P.G., Melody, J.W. and Sater, N.B. Smart icing systems for aircraft icing safety, Reno, Nevada, USA, January 14th - 17th 2002. 40th AIAA Aerospace Sciences Meeting and Exhibit, American Institute of Aeronautics and Astronautics, Inc. (AIAA), 2002. doi: [10.2514/6.2002-813](https://doi.org/10.2514/6.2002-813).
37. Gingras, D.R., Barnhart, B.P., Ranuado, R.J., Martos, B., Ratvasky, T.P. and Morelli, E.A. Development and implementation of a model-driven envelope protection system for in-flight ice contamination, Toronto, Ontario, Canada, August 2nd - 5th, 2010. AIAA Guidance, Navigation and Control Conference, American Institute of Aeronautics and Astronautics, Inc. (AIAA), 2010. doi: [10.2514/6.2010-8141](https://doi.org/10.2514/6.2010-8141).
38. Anon. Flying qualities of piloted aircraft. Military Standard MIL-STD-1797 A, U. S. Department of Defense, Arlington, Virginia, USA, January 1990.