

The ECLIPSE drill: a field-portable intermediate-depth ice-coring drill

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ABSTRACT. A derivative of the Danish tipping-tower intermediate-depth ice-coring drill system has been developed for use in remote areas. The system as described is capable of drilling to depths of 250 m, although the drill has been proven to 350 m. The drill system is designed to be transported by hand and consumes 700 W maximum power from a 24 V d.c. battery bank charged by solar panels or a small generator. A field test in the St Elias Mountains, Yukon, produced good-quality core to 161.6 m depth; drilling at 6500 m a.s.l. on Far East Rongbuk Glacier, Mount Everest, produced good core to 42 m depth.

INTRODUCTION

The University of Copenhagen tipping-tower intermediate-depth electromechanical ice-coring drill system and its predecessors were developed in the 1970s (Rand, 1976; Ruffi and others, 1976; Johnsen and others, 1980; Gundestrup and others, 1989). In 1992, the Geological Survey of Canada (GSC) tested their version of this drill system (called "HILDA") on Agassiz Ice Cap, Ellesmere Island, Northwest Territories. In subsequent years, drilling on Agassiz Ice Cap (1993, 1994) and Penny Ice Cap, Baffin Island (1995, 1996), proved that HILDA can drill dry holes to 350 m, while producing good-quality ice core. HILDA produces 82 mm diameter core in roughly 90 cm lengths with virtually complete core recovery (personal communication from D. Fisher, GSC).

In 1995, the authors began work on a lightweight, hand-portable version of HILDA designed for high-altitude work in the Himalaya. The requirements for the new drill system were that: (1) the complete system should mass no greater than 200 kg; (2) no component should mass greater than 32 kg; (3) the system should produce good core in a dry hole to 200 m depth; and (4) it should be able to operate from a 1000 W solar-panel array.

The resulting design, named "ECLIPSE" after the test site at Eclipse Dome, St Elias Range, Yukon, was field-tested in late-July 1996 and field-proven on Mount Everest in May 1997.

WINCH DESIGN

In meeting the design requirements, using HILDA as a design reference, it was decided that the major mass savings should ensue from redesigning the winch and tower rather than the drill; this was because the HILDA drill is now a proven technology.

As sketched in Figure 1, the frame consists of an open triangular base supporting a square face-frame. The face-

frame, in turn, supports two upright L brackets that hold the winch tower. The face-frame is held upright by two diagonal braces that also support the winch drum, hand winch and winch motor. A final upright near the apex of the base members forms a support for the tipping tower when in the horizontal position. All frame members are 2 in (5.08 cm) square extruded 6061-T6 aluminium tubing. This frame design results in a lightweight, easily assembled yet rigid winch. The winch masses 120 kg with 250 m of cable.

The winch motor is a custom-built 3000 rpm, 24 V d.c. motor drawing 40 A at full load; it is equipped with an electric brake and tachometer. The output from the motor is reduced through an 80:1 Harmonic Drive transmission. The winch drum is chain-driven at a 1:1 ratio from the transmission output and is equipped with a disc brake. A hand crank drives the drum at a 4:1 ratio.

Figure 2 shows the hinge action of the ECLIPSE drill

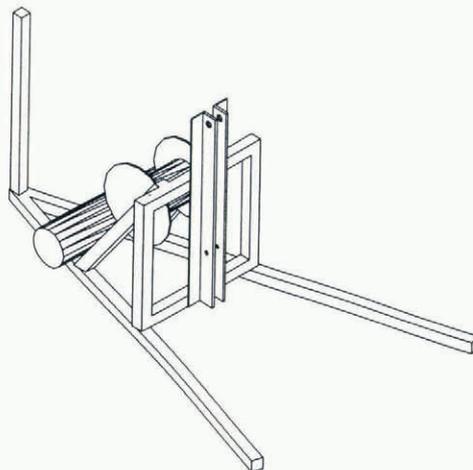


Fig. 1. A perspective view of the lightweight cross-braced winch. The hand crank (not shown), winch drum and winch motor are mounted on the two diagonal braces. The hinged tower (not shown) is mounted at the top of the two L sections.

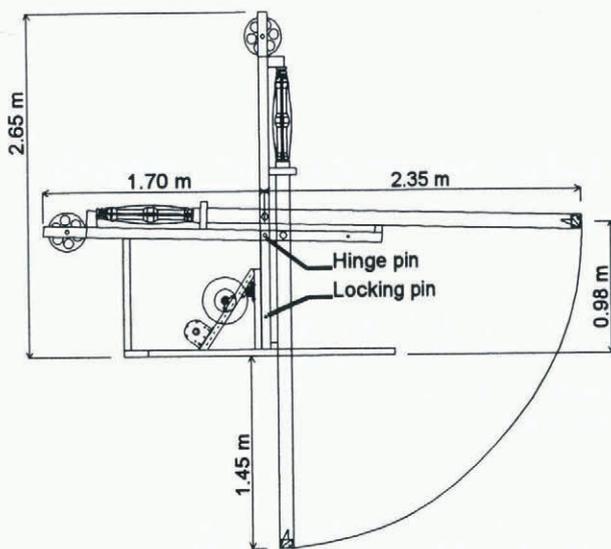


Fig. 2. A side view of the drill, showing the tower and drill in both horizontal and vertical (drilling) positions. The anti-torque section of the drill is visible at the top. In the horizontal position, a slight downward angle is maintained to facilitate removal of the inner barrel.

winch/tower with the drill held in its cradles. Clearances around the drill are noted on the drawing. A 1.5 m deep trench is required to accommodate the drill when in the vertical position. We also install a trapdoor at the bottom of the trench; the door prevents foreign objects from falling into the hole whenever the drill is at the surface. In its horizontal position, the drill has a slight (1.5°) downward angle to assist in removing the inner barrel. An optical encoder attached to the tower sheave measures cable travel.

DRILL CABLE

The authors decided to use steel cable rather than Kevlar cable, as the former is more compact and rugged. Steel cable can also accept a smaller bending radius, thereby permitting a smaller, lighter drum and sheave. The cable used for the drill is Vector Schlumberger 4-18P armoured steel well-logging cable, having a diameter of 4.8 mm, a breaking strength of 14 kN and a mass of 91 kg km^{-1} .

The cable has four 24 AWG copper conductors, each with an electrical resistance of $85 \Omega \text{ km}^{-1}$. The sheath has a resistance of $22 \Omega \text{ km}^{-1}$. Two of the conductors are paired to supply power to the motor (with ground return through the cable sheath); the remaining conductors are used for the tachometer. An anti-torque failure alarm was not included in this ECLIPSE design but could be implemented with a slight modification of the tachometer circuit. The drill advances reliably once drilling has begun; cessation of advance normally occurs only when the drill motor stalls due to overfilling, a condition that can be distinguished from anti-torque failure by examining the tachometer reading.

DRILL

The ECLIPSE drill has an overall length of 3.6 m and a mass of 50 kg. The drill has three major components: a motor/anti-torque section, a rotating inner barrel and a non-rotating outer barrel.

The inner barrel is a 231 cm long, 3.50 in (89 mm) out-

side-diameter thin-wall stainless-steel tube fitted with three nylon spirals. Each spiral has a pitch of 7.0 in (178 mm). An aluminium cutter head equipped with three hardened tool-steel cutters is attached to the inner barrel. The cutter head follows closely the design of Gundestrup and others (1989). The cutters are equipped with a selection of trailing shoes that set the maximum cut depth (shoes 3–6 have a nominal 3, 4, 5 or 6 mm of cut per revolution, respectively). The cutters have a cutting angle of 45° , a relief (or free) angle of 15° and a rake angle of 7° (leading edge on the inside). There is no relief angle on the sides of the cutter. The cutter head also has three core dogs which serve to break and hold the core. The inner barrel is attached to the drive capstan of the motor section with three bayonet-type locking pins inserted through an access port in the outer barrel.

The fixed (non-rotating) outer barrel has an outside diameter of 4.25 in (108 mm) and has 30 straight grooves cut into its inner surface. These grooves extend from the bottom end of the barrel to the access port and serve to assist chip transport. The radial clearance between the inner and outer barrels is approximately 0.6 mm.

The motor section contains a custom 3750 rpm, 200 V d.c. motor, a tachometer and a 50:1 Harmonic Drive gear reducer in a sealed housing. The anti-torque section uses three leaf springs to provide pressure against the bore-hole walls (Reeh, 1984). The wall pressure is adjustable using two locking nuts. The anti-torque section also contains a hammer mass and a slip-ring assembly (Litton Poly-Scientific AC4898 series).

The inner barrel and cutter head are driven at 75 rpm by the drill motor. Chips are carried up the flights and dumped into the inner barrel through chip ports located at the top of the spiral flights. The chips fall on to a nylon core-separator plug that rests on top of the ice core. Core is removed at the surface by tipping the winch tower to a horizontal position, removing the three locking pins and extracting the inner barrel from the drill. The separator plug serves two purposes: (1) it helps keep the chips clear of the core, and (2) it allows the chips to be carried out of the hole should no core be recovered.

CONTROL MODULE

The control module takes a nominal 24 V d.c. input from a lead-acid battery bank; the input to the module is polarity-protected. A MOSFET pulse-width modulator (PWM) circuit provides power for the winch motor (current limit is 50 A). A 40–250 V d.c. switcher-type circuit provides power for the drill motor (current limit is 2 A). Control functions provided include: (1) drill-motor start, stop, direction and speed; (2) winch-motor start, stop, direction and speed; (3) winch emergency-stop switches on the winch frame; (4) tower stop switch to stop winch motor when the drill has been raised; and (5) lockout functions for preventing motor starts when motors are turning. Display functions provided include: (1) drill-motor current and speed; (2) winch-motor current and speed; (3) battery voltage and current draw; and (4) drill depth.

The control function, display functions and PWM circuitry are implemented on a single 75 mm by 250 mm circuit board; the commercial switcher-type supply for the drill motor is in a separate 15 cm by 15 cm by 35 cm enclosure. Relays are used to implement on/off and polarity rever-

sal functions for the two motors. Size 4 AWG welding cable is used for all high-current wiring outside the control module; size 6 AWG wire is used inside the module.

FIELD TEST

In late-July 1996, the drill was transported by Helio Courier aircraft from the Arctic Institute of North America Kluane Lake Research Station to Eclipse Dome, a small ice rise at 60°51'N, 139°47' W. The drill site is at 2950 m a.s.l. and has a mean annual accumulation rate of approximately 1.5 m w.e. year⁻¹ (Holdsworth, 1985).

Though the drill can be operated comfortably by two people, the field party consisted of three people. It took one person 5 hours to assemble the drill and dig the drill trench. Drilling was accomplished in the open with no shelter. Because solar heating caused melting on the drill, most drilling was done at night, with the drill stored at depth during the day to keep it cold. A 2.2 kW Honda generator charging a 24 V, 32 A h battery bank was used for the field test.

Core recovery

Total depth drilled was 161.6 m below surface over 5.5 days. Figure 3 shows the cumulative drill advance and core recovery. Aside from approximately 60 cm of core lost in the upper 2 m due to soft snowpack, core recovery is believed to be virtually complete (calculated value is 99.7%). Core quality from 2 m to approximately 136 m was very good to excellent; below this depth, core quality varied from fair to good. The entire 161 m core was cut in half lengthwise in the field and one half of the core has been returned to the University of New Hampshire for analysis; the remainder of the core is archived on site but will be retrieved in 1997 or 1998.

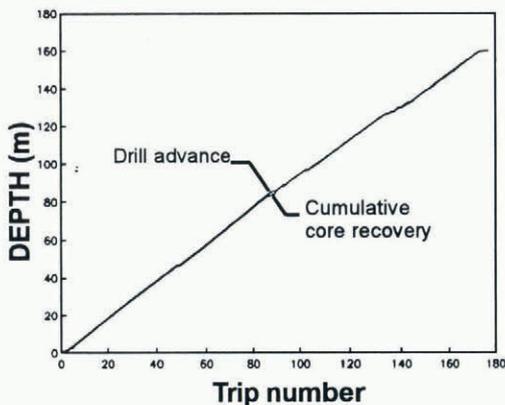


Fig. 3. Drill advance and cumulative core recovery vs trip number for the July 1996 field test.

Figure 4 shows the core length retrieved vs drill depth. A total of ten trips retrieved no core (recorded as 0 cm). The average advance per trip, including trips when there was no advance or core recovery, was 92 cm; typical advance per trip was 100 cm.

Power consumption and performance

When idling, the drill motor consumes 120 W; when drilling at 1.1 cm s⁻¹, the motor draws 180 W and the switching power supply draws 250 W. Approximately 20 W are lost as heat in

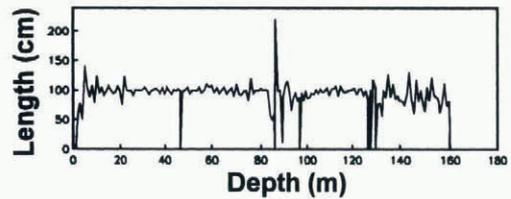


Fig. 4. Core length vs drill depth for the July 1996 field test.

the cable. The winch motor consumes 690 W at a top speed of 42 cm s⁻¹ during ascent; the power consumption drops to 160 W at 60 cm s⁻¹ during descent.

Trip time

The total time required for a complete trip (lowering drill, drilling, raising core, core removal/handling and resetting the drill) varies, of course, with depth. At a depth of 140 m, trip time was 16 min; at a depth of 160 m, trip time was 18 min.

MOUNT EVEREST DRILL SEASON

In May 1997, a drill camp on the north side of Mount Everest was established by Wake and others (personal communication from C. P. Wake). After vehicular transport to Everest base camp, Tibet, at 5200 m a.s.l. the drill system was carried 10 km by yaks and a further 5 km by porters to the drill site on Far East Rongbuk Glacier (6500 m a.s.l.; 28°06' N, 86°58' E). Unforeseen delays resulted in a shortage of time, so drilling was limited to 42 m of core. The drill performed flawlessly.

CONCLUSIONS

The ECLIPSE drill system meets our requirements for high-altitude fieldwork. The drill can be dismantled and carried by hand. When dismantled, the mass of the heaviest component (winch drum with 250 m of cable) is 33 kg and the length of the longest component (outer barrel) is 2.82 m. The entire drill (including spare parts and toolkit) breaks down into eight or nine porter loads. The total mass of the drill is 195 kg.

A 101 mm version of the ECLIPSE drill has been designed but not yet built.

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