

# Instabilities in falling films of thixotropic fluids

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Thixotropic fluids with a non-monotonic flow curve display viscosity bifurcations at certain stresses. It has been proposed that these transitions can introduce interfaces (or shear bands) into thin films that can destabilize inertialess flows over inclined planes. This proposition is confirmed in the present paper by formulating a thin-film model, then using this model to construct sheet-like base flows and test their linear stability. It is also found that viscosity bifurcations, and the associated interfaces, are not necessary for instability, but that the time-dependent relaxation of the microstructure responsible for thixotropy within the bulk of the film can promote instability instead. Computations with the thin-film model demonstrate that instabilities saturate supercritically into steadily propagating nonlinear waves that travel faster than the mean flow.

**Key words:** complex fluids, shear-flow instability, thin films

## 1. Introduction

The dynamics of unstable waves developing on a viscous film flowing down an inclined plane is a classical problem in fluid mechanics, often referred to as the Kapitza problem (e.g. Chang 1994). The instability features in a number of everyday settings, including water flow down roads and windscreens on rainy days. Analogous instabilities appear on flowing films of complex fluids, and thereby used to rationalize natural phenomena such as mud surges (e.g. Ng & Mei 1994; Coussot 1997). In this latter context, the instability has been used to illustrate some of the novelties introduced by non-Newtonian behaviour, such as inertialess elastic instability (Shaqfeh, Larson & Fredrickson 1989), stabilization by a yield stress (Balmforth & Liu 2004) and discontinuous shear thickening (Darbois Texier *et al.* 2023; Balmforth 2025). Worded differently, the wavy instabilities on a falling film of complex fluids offer a probe into material behaviour: the spatiotemporal dynamics of the film provides a different setting than simple rheometric flows, and can be compared with relatively straightforward laboratory experiments. A similar vein has been mined for

granular media (Edwards & Gray 2015). A goal of the current paper is to extend these ideas to thixotropic fluids.

Thixotropic fluids have a time-dependent microstructure that builds up when the fluid is at rest, leading to an increase in effective viscosity, but is reversibly broken down by flow, thereby lowering the fluid's resistance (Mewis & Wagner 2009). This behaviour can lead to pronounced hysteresis, or 'thixotropic loops', in rheometers when stresses or strain rates are cycled up and down. A wide range of fluids exhibit thixotropic behaviour, including natural clay suspensions, industrial drilling fluids and cements, printing inks and paints, oils and grease, and food products such as mayonnaise and ketchup (Barnes 1997; Mewis & Wagner 2009).

Thixotropic hysteresis can be particularly pronounced when the material behaviour features so-called 'viscosity bifurcations' (e.g. Coussot *et al.* 2002; Dullaert & Mewis 2006; Møller *et al.* 2006; Alexandrou, Constantinou & Georgiou 2009; Wachs, Vinay & Frigaard 2009; Dimitriou & McKinley 2014). One such transition arises when the fabric of the fluid evolves relatively slowly towards a structured state that is highly viscous or 'jammed' (solid-like), but collapses abruptly under shear. Dramatic failure events can then occur at the initiation of flow. A second type of viscosity bifurcation arises once motion is underway and the microstructure broken down, if that structure is able to swiftly recover and jam again below a critical shear rate. This behaviour has been observed in a number of fluids, and implies that, should stresses decline sufficiently to permit shear rates to descend below the critical shear rate, the viscosity abruptly increases and flow becomes arrested.

Hewitt & Balmforth (2013) previously explored the dynamics of thixotropic fluids with viscosity bifurcations for inertialess gravity currents (see also Oishi, Martins & Thompson 2017). In this setting, the sudden release and collapse of a reservoir seeds the runout of the current towards a final deposit. During runout, the thixotropic rheology of the material leads to a characteristic two-layer structure to the flow, with lower-lying destructured material conveying along a structured top layer. Under certain conditions, Hewitt & Balmforth (2013) observed that the interface between the layers developed what looked like wavy instabilities. This observation was rationalized by drawing an analogy with the instabilities that appear in multilayer, viscously stratified or non-Newtonian flows (e.g. Loewenherz & Lawrence 1989; Loewenherz, Lawrence & Weaver 1989; Chen 1993, 1995; Charru & Hinch 2000; Balmforth, Craster & Toniolo 2003; Ern, Charru & Luchini 2003). The idea that instability can be triggered by the deformation of rheologically induced interfaces has also featured in the discussion of other shear flows of complex fluids (e.g. Renardy 1995; Fielding 2005, Wilson & Fielding 2006; Fielding 2007; Nghe *et al.* 2010; Cromer, Cook & McKinley 2011; Nicolas & Morozov 2012; Renardy & Renardy 2017; Castillo & Wilson 2020).

Nevertheless, in order to attack the gravity current problem, Hewitt & Balmforth (2013) significantly simplified the rheological model that they employed. In particular, they assumed that the microstructure adapted instantaneously to local shear rates. As a consequence, wherever stresses prompted a viscosity bifurcation, it was assumed that the material instantaneously switched state. Without spatial diffusion, the border between structured and destructured fluid then becomes a jump discontinuity that evolves as a material interface. The limitations inherent in this approximation (which were necessary to simplify the gravity current model), lead one to question whether interfacial instability can arise in low-Reynolds-number thixotropic flows.

The purpose of the present article is to reconsider the linear stability of inertialess, thin films of thixotropic material, with a view to addressing this question. We therefore return to the original rheological model proposed by Hewitt & Balmforth (2013), which aligns with many others used in the literature on complex fluids (Coussot *et al.* 2002;

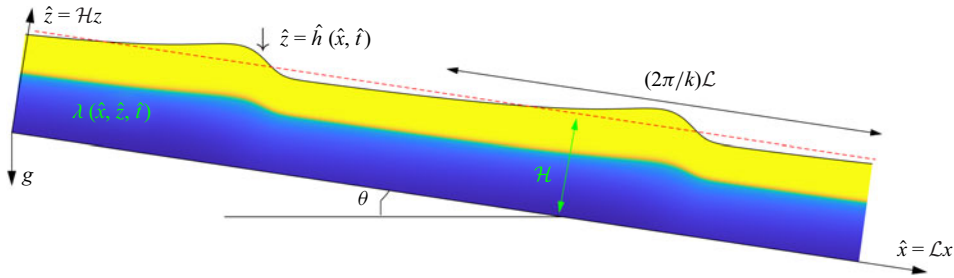


Figure 1. Geometry of the thin-film model: a shallow layer of thixotropic fluid, with viscosity dictated by a structure function  $\lambda(\hat{x}, \hat{z}, \hat{t})$ , flows down an incline of slope  $\tan \theta = \varepsilon = \mathcal{H}/\mathcal{L}$ , where  $\mathcal{H}$  is the mean depth.

Dullaert & Mewis 2006; Møller *et al.* 2006; Alexandrou *et al.* 2009). We thereby accommodate the time-dependent relaxation of the microstructure and also its spatial diffusion, formulating a model suitable for a thin-film setting (§ 2). Armed with this model, we construct steady base states corresponding to sheet-like flow down an inclined plane (§ 3), and then test their linear stability (§ 4). We find that the instability detected by Hewitt & Balmforth (2013) can indeed feature, and interrogate its dynamics more thoroughly, including at the finite amplitudes where instability saturates (§ 5). For completeness, Appendix A presents a summary of the Hewitt–Balmforth reduction and its predictions for the current problem of the wavy instabilities on a falling fluid film.

## 2. Shallow flow model

### 2.1. Dimensional formulation

Consider a complex fluid flowing down a plane inclined at angle  $\theta$ . The geometry is described by a Cartesian coordinate system  $(\hat{x}, \hat{z})$ , orientated such that the  $x$ -axis points down the slope, see figure 1. The fluid velocity is  $\hat{\mathbf{u}} = (\hat{u}, \hat{w})$ . The fluid is shallow, with a mean depth  $\mathcal{H}$  that is much smaller than the characteristic length scale for variations over the plane,  $\mathcal{L}$ . The slope angle is also taken to be relatively small, leading us to set

$$\tan \theta = \varepsilon = \frac{\mathcal{H}}{\mathcal{L}} \ll 1. \quad (2.1)$$

In this setting, we consider waves evolving over spatially periodic domains of length of  $2\pi\mathcal{L}/k$ , where  $k$  is an  $O(1)$  dimensionless wavenumber. The local fluid depth is  $\hat{z} = \hat{h}(\hat{x}, \hat{t})$ .

Assuming that the fluid is incompressible and inertia is negligible, conservation of mass and momentum demand that

$$\frac{\partial \hat{u}}{\partial \hat{x}} + \frac{\partial \hat{w}}{\partial \hat{z}} = 0, \quad (2.2)$$

and

$$\mathbf{0} = \rho \tilde{\mathbf{g}} - \nabla \hat{p} + \nabla \cdot \hat{\boldsymbol{\tau}}. \quad (2.3)$$

Here,  $\tilde{\mathbf{g}} = (g \sin \theta, 0, -g \cos \theta)$ , with constant gravitational acceleration  $g$ , the pressure is  $\hat{p}$  and the deviatoric stress is  $\hat{\boldsymbol{\tau}} = \{\hat{\tau}_{ij}\}$ , which we relate to the rate of strains by the generalized Newtonian fluid model,

$$\hat{\tau}_{ij} = \hat{\mu}(\lambda) \hat{\gamma}_{ij}, \quad (2.4)$$

where

$$\hat{\boldsymbol{\gamma}} = \{\hat{\gamma}_{ij}\} = \nabla \hat{\mathbf{u}} + (\nabla \hat{\mathbf{u}})^T. \quad (2.5)$$

The tensors have second invariants,  $\hat{\gamma} = \sqrt{(1/2) \sum_{i,j} \hat{\gamma}_{ij} \hat{\gamma}_{ij}}$  and  $\hat{\tau} = \sqrt{(1/2) \sum_{i,j} \hat{\tau}_{ij} \hat{\tau}_{ij}}$ . The viscosity  $\hat{\mu}(\lambda)$ , is controlled by the parameter  $\lambda(\hat{x}, \hat{z}, \hat{t})$ , which gauges the degree of microstructural order.

There is no slip at the base of the fluid and we assume that the top surface is stress-free,

$$\begin{aligned} \hat{\mathbf{u}} &= 0 \quad \text{at} \quad \hat{z} = 0, \\ (\hat{\tau}_{ij} - \hat{p} \delta_{ij}) n_j &= 0 \quad \text{at} \quad \hat{z} = \hat{h}(\hat{x}, \hat{t}), \end{aligned} \quad (2.6)$$

where  $\mathbf{n}$  is the normal to the upper surface  $\hat{z} = \hat{h}$ , and the kinematic condition there is

$$\frac{\partial \hat{h}}{\partial \hat{t}} + \hat{\mathbf{u}} \frac{\partial \hat{h}}{\partial \hat{x}} = \hat{w} \quad \text{at} \quad \hat{z} = \hat{h}(\hat{x}, \hat{t}). \quad (2.7)$$

The omission of surface tension is potentially problematic in thin films with relatively small length scales, as in the Kapitza problem (e.g. Chang 1994). We assume here that the film has larger length scale so that capillary effects are small, our purpose being to interrogate instabilities driven by rheological effects rather than how surface tension might stabilize them.

## 2.2. Dimensionless leading-order formulation

To remove the dimensions (and hats) from the equations, we introduce the rescalings

$$\hat{t} = \frac{\mathcal{L}}{\mathcal{U}} t, \quad \hat{x} = \mathcal{L} x, \quad (\hat{z}, \hat{h}) = \mathcal{H}(z, h), \quad (2.8)$$

$$\hat{\mathbf{u}} = \mathcal{U} \mathbf{u}, \quad \hat{w} = \varepsilon \mathcal{U} w, \quad \hat{p} = \rho g \mathcal{H} p \cos \theta, \quad \hat{\tau}_{ij} = \frac{\mu_0 \mathcal{U}}{\mathcal{H}} \tau_{ij}, \quad \hat{\mu} = \mu_0 \mu, \quad (2.9)$$

where  $\mu_0$  is a characteristic viscosity and the speed scale

$$\mathcal{U} = \frac{\mathcal{H}^3 \rho g}{\mathcal{L} \mu_0} \cos \theta. \quad (2.10)$$

With these scalings, and omitting terms of  $O(\varepsilon^2)$ , (2.3) reduces to the lubrication equations

$$0 = 1 - \frac{\partial p}{\partial x} + \frac{\partial \tau_{xz}}{\partial z}, \quad 0 = -1 - \frac{\partial p}{\partial z}. \quad (2.11)$$

The dominant component of the rate of strain tensor is the vertical shear  $\dot{\gamma}_{xz} = \partial u / \partial z + O(\varepsilon^2)$ , and to leading order, the stress conditions in (2.6b) become

$$p = \tau_{xz} = 0 \quad \text{at} \quad z = h(x, t). \quad (2.12)$$

The kinematic condition (2.7) is unchanged after scaling (but for the removal of the hats). Equations (2.11) and (2.12) imply that the pressure is hydrostatic,

$$p = h - z, \quad (2.13)$$

and the shear stress is given by

$$\begin{aligned}\tau_{xz} &= (h - z) \left(1 - \frac{\partial h}{\partial x}\right) = (1 - \zeta)\tau_b, \quad \tau_b = h \left(1 - \frac{\partial h}{\partial x}\right), \quad \zeta = \frac{z}{h}, \\ &= \mu(\lambda) \frac{\partial u}{\partial z},\end{aligned}\tag{2.14}$$

where  $\tau_b$  is the basal shear stress.

Finally, mass conservation integrated over the fluid layer implies

$$\frac{\partial h}{\partial t} = -\frac{\partial}{\partial x} \int_0^h u \, dz = -\frac{\partial}{\partial x} \int_0^h (h - z) \frac{\partial u}{\partial z} \, dz.\tag{2.15}$$

Since

$$\frac{\partial u}{\partial z} = \frac{\tau_{xz}}{\mu(\lambda)} = \frac{(1 - \zeta)\tau_b}{\mu(\lambda)},\tag{2.16}$$

the constitutive law can now be plugged into (2.15) to arrive an evolution equation for the fluid thickness. The exercise is complicated by the structure parameter  $\lambda$ , however, which retains an unknown vertical profile, as discussed next.

### 2.3. Constitutive law

Thixotropic rheology has been described using simple constitutive models (Barnes 1997; Mewis & Wagner 2009; Larson & Wei 2019) in which the structure parameter  $\lambda(x, z, t)$  satisfies the (dimensional) evolution equation,

$$\frac{\partial \lambda}{\partial t} + \hat{u} \frac{\partial \lambda}{\partial \hat{x}} + \hat{w} \frac{\partial \lambda}{\partial \hat{z}} = \frac{1 - \lambda}{T} - \alpha \lambda \tilde{\gamma} + K \nabla^2 \lambda,\tag{2.17}$$

and controls the fluid rheology through the viscosity law (2.4). The order parameter lies in a range  $[0, 1]$ ; for  $\lambda = 0$ , the fluid has no effective microstructure, while it is fully structured when  $\lambda = 1$ . The evolution equation in (2.17) contains a restructuring term  $(1 - \lambda)/T$  that drives  $\lambda$  towards the fully structured state, and a destruction term dictated by the local shear rate  $\tilde{\gamma}$ . Restructuring is characterized by a healing time scale  $T$ , and destruction is parameterized by  $\alpha$ . In some other related models, the rate of destructuring is taken to be proportional to a power of  $\tilde{\gamma}$ , or a power of the stress invariant  $\tilde{\tau}$ ; we use (2.17) in view of its simplicity. We have further included a diffusive term in (2.17) to account for any spatial structural diffusion, with diffusivity  $K$ , although we will be mostly concerned with the limit in which this physical effect is relatively weak.

For the viscosity law, we follow Hewitt & Balmforth (2013) and choose

$$\tilde{\mu}(\lambda) = \frac{\mu_o}{(1 - \lambda)[(1 - \lambda)(1 - a) + a]} = \mu_o \mu(\lambda),\tag{2.18}$$

where  $\mu_o$  is the characteristic viscosity and  $a$  is a parameter with  $0 < a < 1$ . The resulting constitutive law is qualitatively similar to others proposed in the literature, in that it produces comparable flow curves in steady, uniform shear (Coussot *et al.* 2002; Dullaert & Mewis 2006; Møller *et al.* 2006; Alexandrou *et al.* 2009). The precise form, however, proves analytically convenient, as discussed below (and is written slightly differently to that in Hewitt & Balmforth (2013)).

In the shallow limit, following the scalings of § 2.2, the dimensionless version of the constitutive model is

$$\mathcal{T}(\lambda_t + u\lambda_x + w\lambda_z) = 1 - \lambda - \Gamma\dot{\gamma}\lambda + \kappa\lambda_{zz},$$

$$u_z = \tau_{xz}A(\lambda), \quad A(\lambda) \equiv [\mu(\lambda)]^{-1} = (1 - \lambda)[(1 - \lambda)(1 - a) + a], \quad (2.19)$$

where we have used  $(t, x, z)$ -subscripts as shorthand for partial derivatives (except for the shear stress  $\tau_{xz}$ ), and the dimensionless groups,

$$\mathcal{T} = \frac{\mathcal{U}T}{\mathcal{L}}, \quad \Gamma = \frac{\alpha T\mathcal{U}}{\mathcal{H}}, \quad \kappa = \frac{KT}{\mathcal{H}^2}, \quad (2.20)$$

represent a characteristic relaxation time, healing rate and diffusivity. The definition of the reciprocal viscosity function  $A(\lambda)$  proves useful in the further analytical developments of the appendices, where its usage also highlights how the results are insensitive to the detailed analytical choice of the viscosity law.

The addition of diffusion in (2.19) demands the inclusion of further boundary conditions on  $\lambda(x, z, t)$  at the base and surface of the film. Assuming that structure is neither created nor destroyed by interfacial interaction, we adopt the no-flux conditions,

$$\lambda_z(x, 0, t) = \lambda_z(x, h, t) = 0. \quad (2.21)$$

#### 2.4. Flow curves

Viscosity bifurcations are commonly exposed and illustrated using the flow curve of a model fluid; i.e. by considering how the shear stress depends on shear rate under conditions of steady, spatially uniform shear. For the current rheological model, the relations (2.19) imply the flow curve,

$$\lambda = \frac{1}{1 + \Gamma\dot{\gamma}} \quad \text{and} \quad \tau = |\tau_{xz}| = \frac{(1 + \Gamma\dot{\gamma})^2}{\Gamma(a + \Gamma\dot{\gamma})}. \quad (2.22)$$

Consequently,  $\Gamma$  dictates the dimensionless shear rate at which destructuring becomes effective, whereas  $a$  controls the shape of the flow curve, as illustrated in figure 2. For  $\Gamma\dot{\gamma} \gg 1$ , we recover the Newtonian law,  $\tau = \dot{\gamma}$ . Conversely, for  $\Gamma\dot{\gamma} \ll 1$ , we find

$$\tau = \frac{1}{\Gamma a} \left[ 1 + \frac{2a - 1}{a} \Gamma\dot{\gamma} + \dots \right]. \quad (2.23)$$

Unless  $a = 0$ , the flow curve therefore intersects the  $\tau$ -axis at a finite stress,  $\tau_A = (\Gamma a)^{-1}$ . If  $a > (1/2)$ , the flow curve increases monotonically away from this yield point towards higher shear rates, in the manner of a simple (non-thixotropic) yield-stress fluid, see the lower flow curves in figure 2(a). Beginning from fully structured fluid ( $\lambda = 1$  and  $\dot{\gamma} = 0$ ), the threshold stress above which motion must take place is then  $\tau > \tau_A$ .

For  $a < (1/2)$ , on the other hand, the flow curve becomes non-monotonic, first descending to lower stresses for a range of shear rates. The curve subsequently reaches a minimum at  $(\dot{\gamma}, \tau) = (\dot{\gamma}_c, \tau_c)$ , and then ascends to higher stresses. The minimum stress is given by

$$\tau_c = \frac{4(1 - a)}{\Gamma} \quad \left( \dot{\gamma}_c = \frac{1 - 2a}{\Gamma}, \quad \lambda_c = \frac{1}{2(1 - a)} \right), \quad (2.24)$$

and implies an alternative stress threshold for motion of  $\tau > \tau_c$ . The upper four flow curves in figure 2(a) illustrate this alternative behaviour. As illustrated in figure 2(b), such flow

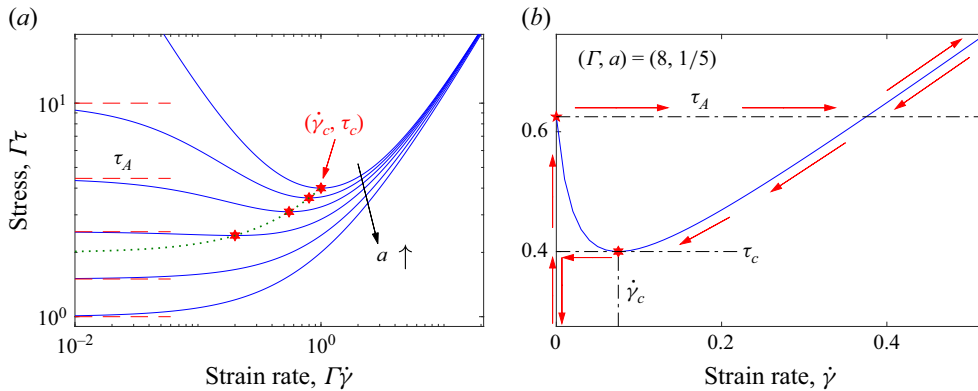


Figure 2. Steady-state flow curves for (a) varying  $a$  (scaling  $\dot{\gamma}$  and  $\tau$  by  $\Gamma$ ), and (b)  $(\Gamma, a) = (8, 1/5)$ . The special values,  $(0, \tau_A)$  and  $(\dot{\gamma}_c, \tau_c)$ , are indicated. The dotted line in (a) shows the locus of  $(\dot{\gamma}_c, \tau_c)$  for varying  $a$ ; the specific flow curves shown have  $a = 0, 0.1, 0.225, 0.4, 0.666$  and  $1$ . The (red) arrows in (b) indicate the path of a hysteretic loop taken on first increasing then decreasing the stress, starting from an initially structured state with  $\Lambda = 1$ .

curves imply excursions along hysteretic loops on first increasing, then decreasing the stress, in the conventional manner of thixotropy; sudden jumps in shear rate, or viscosity bifurcations, arise at the stresses  $\tau = \tau_A$  and  $\tau = \tau_c$ . The multiplicity of possible states for  $\tau_A < \tau < \tau_c$ , also implies a sensitivity to initial preparation or flow history. The limiting case  $a = 0$ , implying  $\tau_A \rightarrow \infty$  and no finite yield stress for the fully structured state, is similar to the models proposed by Coussot *et al.* (2002) and Møller *et al.* (2006).

### 3. Base states

Steady sheet-like flows are given by  $\tau = 1 - z$ ,  $u = U(z)$  and  $\lambda = \Lambda(z)$ , where

$$\begin{aligned} \kappa \Lambda_{zz} &= \Gamma \Lambda U_z - (1 - \Lambda), & U(0) &= \Lambda'(0) = \Lambda'(1) = 0, \\ U_z &= (1 - z)A(\Lambda), \end{aligned} \quad (3.1)$$

Sample solutions to this system are shown in figure 3 for two representative parameter settings, the first case without a viscosity bifurcation, the other case including one.

In the limit that  $\kappa \rightarrow 0$ , (2.19) or (3.1) imply that the solutions follow stress-controlled sections of the flow curve. Consequently, to achieve flow, the stress must exceed one of the flow thresholds,  $\tau_A$  and  $\tau_c$ , somewhere within the layer. Given that  $\tau = 1 - z$ , the maximum stress is unity and occurs at the base. Therefore, flow requires  $\tau_A < 1$  or  $\tau_c < 1$ . For a monotonic flow curve with  $a > (1/2)$ , the relevant criterion is  $\tau_A^{-1} = \Gamma a > 1$ . Conversely, if the flow curve first bends downwards and  $a < (1/2)$ , then the base of the fluid can be destructured and flowing if  $1 > \tau_c$ . Nevertheless, if  $\tau_A > 1 > \tau_c$ , it is also possible that the entire fluid layer is fully structured and plugged up; only when  $\tau_A < 1$  are we assured that flow must take place. For  $\tau_A > 1 > \tau_c$ , we have the potential for two possible states, one flowing and one fully plugged.

Diffusionless, base-flow solutions therefore trace out a locus on the stress-shear-rate plane which begins at the bottom of the  $\tau$ -axis (i.e. the top of the fluid layer). For  $a > (1/2)$  and  $1 > \tau_A$ , the locus moves up that axis until it reaches the yield point,  $\tau = \tau_A$ , then shifts to finite shear rates along the monotonic flow curve (all the while descending through the fluid layer); the yield point arises at the height  $z = z_A = 1 - \tau_A$ . In other words, the fluid is fully structured above  $z = z_A$ , and is rafted along as a rigid plug by an underlying layer of partially structured material. This leads to profiles for the velocity and shear rate that are



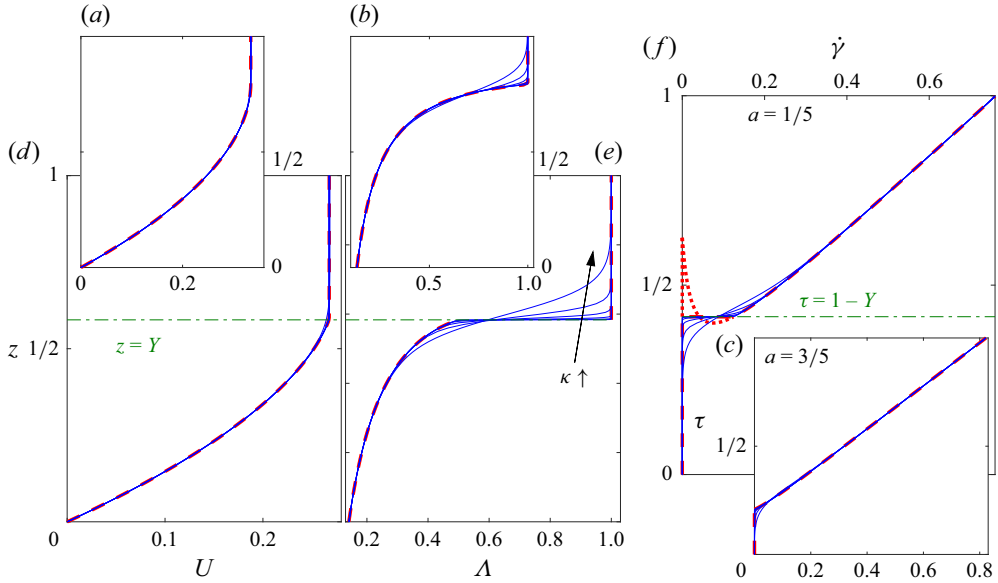


Figure 3. Base states for  $(a,b,c)$   $a = (3/5)$  and  $(d,e,f)$   $a = 1/5$ , with  $\Gamma = 8$  and  $\kappa = 10^{-j}$ ,  $j = 3, 4, \dots, 8$ . In  $(e-f)$ , the green dot-dash line indicates  $z = Y$  and  $\tau = 1 - Y$ , with  $Y$  given by (3.6). The (red) dashed lines indicate the diffusionless solution (computed assuming the same  $Y$  in  $(d-f)$ ); the (red) dotted line in  $(f)$  shows the untraced part of the flow curve.

continuous and similar to those for a Bingham fluid (Balmforth *et al.* 2006). Figure 3(a–c) illustrate such profiles for  $(\Gamma, a) = (10, (3/5))$ . Solutions to (3.1) for  $\kappa > 0$  are also included in this figure, and demonstrate how the switch at  $z > z_A$  becomes smoothed by small diffusion, but otherwise the profiles remain similar. Notably, the upper section of the fluid layer is not fully structured ( $\Lambda < 1$ ), but is, nevertheless, plug-like with  $\Lambda \approx 1$  and  $U_z \approx 0$ .

The other example in figure 3(e–f) displays a case with a non-monotonic flow curve and a viscosity bifurcation. Here, the locus of the base state on the  $(\dot{\gamma}, \tau)$ -plane first moves up the  $\tau$ -axis, but then switches abruptly over to the right-hand part of the flow curve at a stress level  $\tau = 1 - Y$  that lies between the two thresholds,  $\tau_A$  and  $\tau_C$ . Without diffusion, the jump is discontinuous; for  $\kappa > 0$ , the transition becomes smoothed. The abrupt jump leads to a sharper transition from the superficial plug to much less structured material underneath, with repercussions on the velocity and shear-rate profiles.

In principle, any level  $z = Y$  for which  $\tau_A > 1 - Y > \tau_C$  could locate a jump from structured to destructured fluid in the diffusionless problem; the level  $Y$  must be selected as an initial condition (cf. Wilson & Fielding 2006). The choice shown in figure 3(e–f) by the dashed (red) line corresponds to the particular location that is selected for  $\kappa \rightarrow 0$  in the problem with diffusion (solid blue lines). To find this location, we consider (3.1) in more detail: for  $\kappa \ll 1$ , the transition arises over a narrow region with a thickness of  $O(\sqrt{\kappa})$ . Setting  $z = Y + \sqrt{\kappa}\zeta$ , (3.1) then reduces to

$$\kappa \Lambda_{zz} \equiv \Lambda_{\zeta\zeta} \sim \Psi(\Lambda; Y, \Gamma, \text{Bi}) = (1 - \Lambda)\{\Gamma \Lambda[(1 - \Lambda)(1 - a) + a](1 - Y) - 1\}. \quad (3.2)$$

The level  $z = Y$  now follows by imposing the matching conditions,

$$\Lambda \rightarrow 1 \text{ for } \zeta \rightarrow \infty \quad \text{and} \quad \Lambda \rightarrow \Lambda_a \text{ for } \zeta \rightarrow -\infty, \quad (3.3)$$



where

$$\Lambda_a = \frac{1}{2(1-a)} \left[ 1 - \sqrt{1 - \frac{4(1-a)}{\Gamma(1-z)}} \right] \quad (3.4)$$

corresponds to the structure function along the right-hand branch of the flow curve. The exercise is equivalent to demanding that

$$\int_{\Lambda_a}^{\Lambda_*} \Psi(\Lambda; Y, \Gamma, \text{Bi}) \, d\Lambda = 0, \quad (3.5)$$

which implies that

$$Y = 1 - \frac{9(1-a)}{\Gamma(2-a)(1+a)}, \quad (3.6)$$

and successfully locates the transition level in [figure 3\(e–f\)](#).

## 4. Stability theory

### 4.1. Linear equations

Infinitesimal perturbations to the base states, with

$$h = 1 + \check{\eta} e^{ikx + \sigma t}, \quad u = U(z) + \psi_z(z) e^{ikx + \sigma t}, \quad \lambda = \Lambda(z) + \check{\lambda}(z) e^{ikx + \sigma t}, \quad (4.1)$$

wavenumber  $k$  and (complex) growth rate  $\sigma = \sigma_r + i\sigma_i$ , satisfy

$$\begin{aligned} \psi_{zz} &= \frac{U_z \check{\tau}}{1-z} + (1-z) A'(\Lambda) \check{\lambda}, \\ \mathcal{T}[(\sigma + ikU) \check{\lambda} - ik\Lambda_z \psi] &= -(1 + \Gamma U_z) \check{\lambda} - \Gamma \Lambda \psi_{zz} + \kappa \check{\lambda}_{zz}. \end{aligned} \quad (4.2)$$

Here,  $\psi(z)$  represents a stream function such that  $(u, w) = (U + \psi_z e^{ikx + \sigma t}, -ik\psi e^{ikx + \sigma t})$ , and the shear stress perturbation has amplitude

$$\check{\tau} = [1 - ik(1-z)] \check{\eta}. \quad (4.3)$$

The boundary conditions translate to

$$[\sigma + ikU(1)] \check{\eta} = -ik\psi(1), \quad \psi(0) = \psi_z(0) = \check{\lambda}_z(0) = \check{\lambda}_z(1) + \check{\eta} \Lambda_{zz}(1) = 0 \quad (4.4)$$

(after a shift of the moving surface position back to  $z = 1$  in the last one).

The problem in (4.2)–(4.3) can be solved by discretizing in  $z$ , and then using Chebyshev differentiation matrices to turn the eigenvalue problem into a matrix one. Though limited in spatial resolution, this technique expedites the search for unstable modes. Once found, MATLAB's inbuilt solver `bvp4c` can be used to compute those modes with better resolution, and then continue them to different parameter settings. Alternatively, we may take different limits of the problem and reduce the equations further to obtain some more explicit results. That exercise is accomplished in [Appendices B–E](#).

### 4.2. Results

[Figure 4\(a,b\)](#) displays sample numerical solutions to the linear stability problem, plotting growth rates and phase speeds against  $k$  for various values of  $a$ , with  $(\Gamma, \kappa, \mathcal{T}) = (5, 10^{-4}, 1)$ . For the higher values of  $a$ , the flow curve is monotonically increasing, and the flow is stable. When  $a$  is decreased sufficiently into the regime in which a viscosity

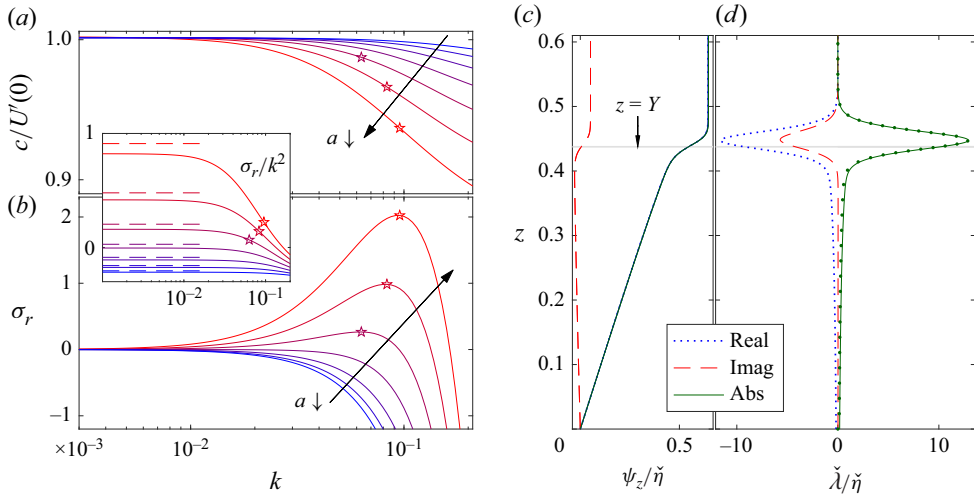


Figure 4. (a) Growth rates  $\sigma_r$  and (b) scaled phase speeds  $c/U_z(0) = -\sigma_r/kU_z(0)$ , for varying  $k$ , with  $a = (1/20)(0, 1, 2, \dots, 6)$  (from red to blue) and  $(\Gamma, \kappa, \mathcal{T}) = (8, 10^{-4}, 1)$ . The most unstable modes for the three lowest values of  $a$  are indicated by stars. The inset compares the growth rates, scaled  $k^2$ , with the predictions of the long-wave analysis of Appendix B (dashed lines). The eigenfunctions,  $\psi_z/\tilde{\eta}$  and  $\tilde{\lambda}/\tilde{\eta}$ , of the most unstable mode for  $a = 0$  are plotted in (c) and (d). The level  $z = Y$  from (3.6) is shown by the light grey line. Also plotted in (d) is  $\Lambda_z$  for the base state, scaled to have the same maximum amplitude as  $|\tilde{\lambda}/\tilde{\eta}|$  (dots).

bifurcation occurs, however, a band of unstable wavenumbers appears, extending from  $k = 0$  up to a critical value  $k_{crit}$ . The phase speeds of the unstable modes are close to  $U_z(0)$ , a feature that can be uncovered from a long-wave analysis (Appendix B).

The eigenfunction of the most unstable mode over all wavenumber  $k$  for the case with  $a = 0$  is plotted in figure 4(c,d). For this mode, an increase in fluid depth enhances downslope flow speed ( $\psi_z$ ; figure 4c), whilst strongly perturbing the structure function over the transition region buffering the destructured lower layer from the overlying plug-like flow (figure 4d). Indeed,  $\tilde{\lambda}$  is opposite in phase to  $\tilde{\eta}$  and its profile is approximately dictated by  $\Lambda_z(z)$ , implying that structural perturbations are mostly due to a vertical shift of the transition region. In other words, the instability operates by destructuring fluid underneath the wave crests, which accelerates flow, enabling the wave to entrain more fluid and thereby amplify. A more detailed interrogation of the instability mechanism follows from the long-wave analysis (Appendix B): to leading order in  $k$ , perturbations take the form of waves propagating with phase speed  $c \sim U_z(0)$ . These waves perturb the flow over the destructured lower layer, where quasisteady viscous perturbations turn out to be stabilizing, but the delay introduced by relaxation contributes to instability. More significant are the associated destabilizing vertical shifts of the transition region. All these effects appear at  $O(k^2)$  in the long-wave expansion, and point to an interfacial-type instability as suggested by Hewitt & Balmforth (2013).

A wider view of the unstable regime is presented in figures 5–7, which plot growth rates as densities over the  $(k, \mathcal{T})$ ,  $(k, a)$  and  $(k, \kappa)$  planes (respectively), each time holding the other parameters fixed. All three figures contain five cases, for varying  $a$  in figure 5, and varying  $\mathcal{T}$  in figures 6 and 7. In every example, the instability has a long-wave character, with  $k_{crit} = O(10^{-1})$  or less. The stability boundaries extracted from the figures are assembled in figure 8, plotting  $k_{crit}$  against  $\mathcal{T}$ ,  $a$  or  $\kappa$  (including some additional cases to better highlight the effect of varying the other parameters).

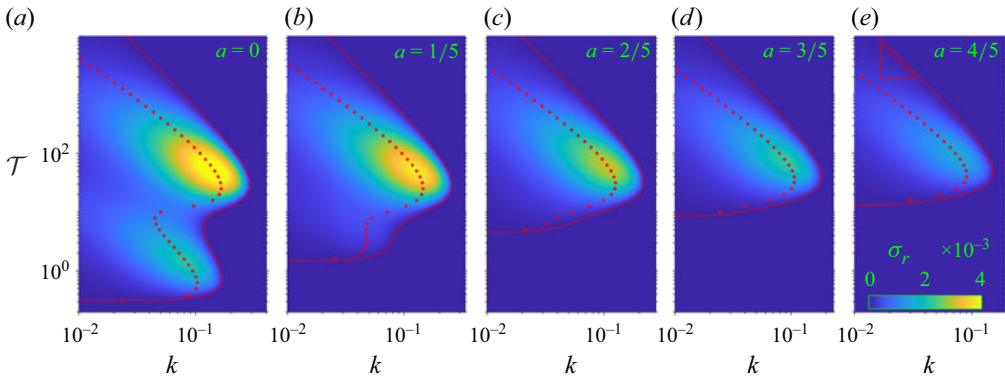


Figure 5. Growth rate as a density over the  $(k, \mathcal{T})$  plane for the values of  $a$  indicated, with  $(\Gamma, \kappa) = (8, 10^{-4})$ . The red contours show the stability boundary, and the dots indicate the most unstable mode over all wavenumber. In (e), the triangle shows the scaling  $\mathcal{T} \propto k^{-2}$ .

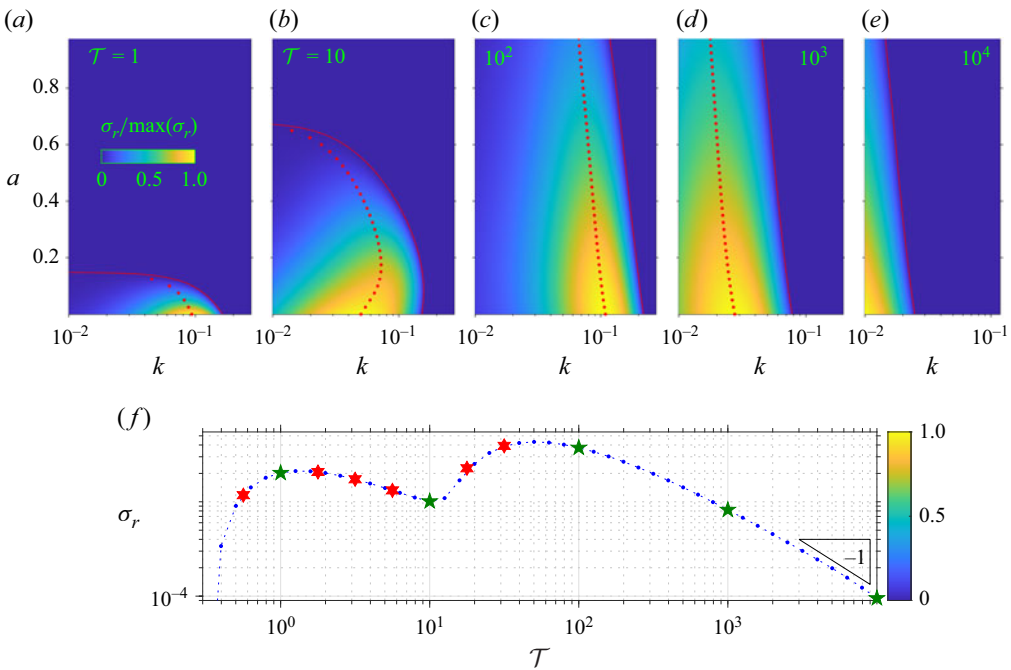


Figure 6. Growth rate as a density over the  $(k, a)$  plane for the values of  $\mathcal{T}$  indicated, all with  $(\Gamma, \kappa) = (8, 10^{-4})$ . The red contours show the stability boundary, and the dots indicate the most unstable mode over all wavenumber. The growth rates are scaled by their maxima; the colour scale can be inferred from (f), which plots the maximum growth rate (achieved at the smallest values of  $a$ ) against  $\mathcal{T}$ . The (green) stars show the specific values of  $\mathcal{T}$  used in panels (a)–(e), whereas the (red) hexagrams show the additional cases that are also presented in figure 8(a). The triangle shows the scaling  $\sigma_r \propto \mathcal{T}^{-1}$ .

A first conclusion that can be drawn from figure 5 is that instability is eventually suppressed for sufficiently small relaxation time  $\mathcal{T}$  when diffusion is not strong, regardless of the value of  $a$ . Indeed, in the limit  $\mathcal{T} \rightarrow 0$  and  $\kappa \ll 1$ , one can further reduce the thin-film model to a nonlinear diffusion equation, as summarized in Appendix C. The base states in this limit can then be shown to be stable (at least in the absence of inertia).

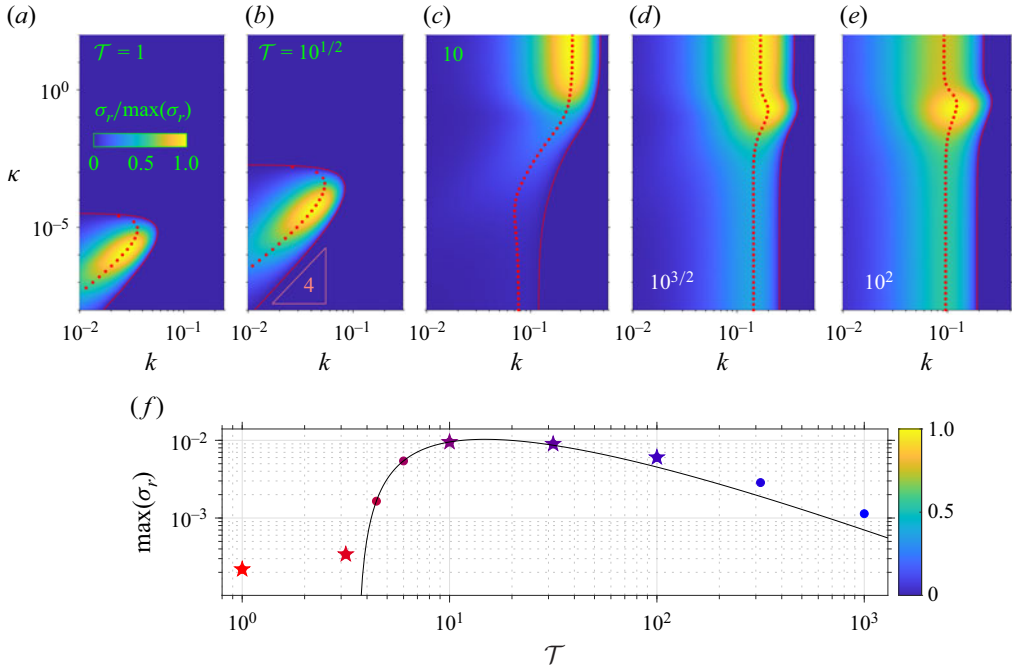


Figure 7. Growth rate as a density over the  $(k, \kappa)$  plane for the values of  $\mathcal{T}$  indicated, all with  $(a, \Gamma) = (1/5, 8)$ . The red contours show the stability boundary, and the dots indicate the most unstable mode over all wavenumber. The triangle in (b) shows the scaling  $\kappa \propto k^4$ . The growth rates are scaled by their maxima; the colour scale can be inferred from (f), which plots the maximum growth rate against  $\mathcal{T}$ . The stars show the specific values of  $\mathcal{T}$  used in panels (a)–(e), whereas the filled circles show additional cases that are also presented in figure 8(c). The solid line shows the prediction in the limit of large diffusion  $\kappa \gg 1$  (Appendix E).

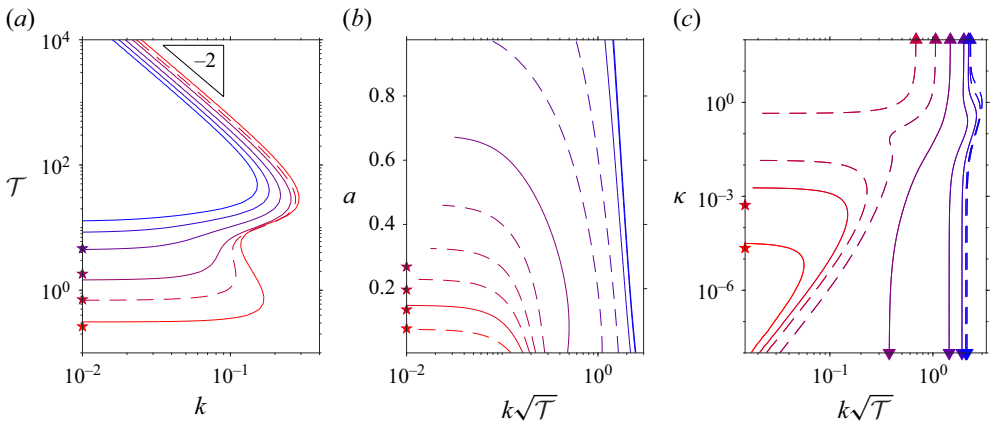


Figure 8. Stability boundaries on the (a)  $(k\sqrt{\mathcal{T}}, a)$ , (b)  $(k, \mathcal{T})$  and (c)  $(k\sqrt{\mathcal{T}}, \kappa)$  planes. The panels correspond to figures 5–7, with the stability boundaries shown from red to blue for increasing  $\mathcal{T}$ ,  $a$  and  $\mathcal{T}$ , respectively. The dashed lines show additional cases, corresponding to  $a = 0.1$  for panel (b), or the extra points plotted in figures 6(f) and 7(f) (for panels (b) and (c)). The stars along the left-hand axes show the predictions of the long-wave, small  $\kappa$  analysis of Appendix B. In (c), the triangles for  $\kappa = 10^2$  indicate predictions using the large diffusion theory of Appendix E; the triangles along  $\kappa = 10^{-8}$  indicate predictions in the zero-diffusion limit (Appendix D).

More curiously, [figures 5 and 6](#) also demonstrate that instability extends into the regime without a viscosity bifurcation ( $a > (1/2)$ ), provided the relaxation time  $\mathcal{T}$  is long enough. This result is also apparent in [figures 6 and 8](#). The rescaling used in the latter figure emphasizes how stability eventually depends on the combination  $k\sqrt{\mathcal{T}}$  for  $\mathcal{T} \gg 1$ . Evidently, when  $\mathcal{T}$  becomes sufficiently large, the destabilizing effect of viscous relaxation overwhelms stabilization by quasistatic viscous effects, even when there is no viscosity bifurcation and the base state possesses no sharp interface. Instabilities associated with the bulk of the fluid, rather than a sharp interface, have also been observed for other shear flows of complex fluids (Renardy & Renardy 2017; Castillo & Wilson 2020).

Finally, [figure 7](#) illustrates the impact of varying the diffusion coefficient  $\kappa$ . Earlier figures display results for  $\kappa = 10^{-4}$ , which is sufficiently small that diffusion does not have a dramatic effect on the base states (other than broadening the interface-like transition region). For low relaxation time ( $\mathcal{T} \lesssim 4$  in [figure 7](#)) the impact of diffusion on the linear stability is more subtle: instability becomes restricted to a low-wavenumber band with  $k_{crit} \propto \kappa^{1/4}$ . Instability therefore becomes suppressed for  $\kappa \rightarrow 0$ . By contrast, with higher  $\mathcal{T}$ , growth rates converge to finite values. The limit of small diffusion is considered in [Appendix D](#); corresponding predictions for the position of the stability boundary are included in [figure 8\(c\)](#).

[Figure 7](#) also highlights how instability persists even with relatively strong diffusion. For  $\kappa \gg 1$ , the structure function becomes uniform across the film, and the evolution equations in (2.19) and (2.15) simplify further, as outlined in [Appendix E](#). The prediction for the large- $\kappa$  limit of the stability boundary are again shown in [figure 8\(c\)](#). Note that the uniform profile of the structure function implies that, in this limit, instability cannot be the result of interfacial dynamics, but solely due to bulk viscous relaxation.

## 5. Nonlinear dynamics

To explore the nonlinear dynamics of unstable waves, we solve the thin-film equations (2.15) and (2.19) numerically in periodic-in- $x$  domains with length  $\ell = 2\pi/k$  (some details of the numerical scheme are provided in [Appendix F](#)). A sample solution for a case in which a viscosity bifurcation occurs ( $a = 1/5$ ) and vertical diffusion is relatively small ( $\kappa = 10^{-4}$ ) is shown in [figure 9](#). The initial perturbation to the base flow seeds the growth of an unstable wave, which amplifies according to linear theory. The instability subsequently saturates at finite amplitude to generate a steadily propagating nonlinear wave. The final wave travels slightly faster than the original unstable linear mode, as evident from the snapshots in [figure 9\(c\)](#), which plots the wave height profile in the linear wave frame (with phase speed  $c$ ). Also shown ([figure 9d](#)), are snapshots of the interface between structured and destructured fluid (identified as the contour where  $\lambda(x, Y, T) = (4/5)$ ). In line with the spatial structure of the linear mode, the interface elevates below the rise to the crest of the wave, as fluid locally destructures due to increased shear stresses.

The final nonlinear wave is shown in more detail in [figure 10](#), which presents the distribution of the structure function, together with a selection of streamlines (in the frame of the wave). Also shown (in [figure 10b](#)) is the final wave for a numerical solution with  $a = (3/5)$ . Although this second example does not feature a viscosity bifurcation, and the division between structured and destructured fluid is smoother, the dynamics of the instability is similar, with linear growth again saturating to create the nonlinear wave illustrated (see also [figure 9b](#)).

A wider suite of computations is shown in [figure 11](#). This suite corresponds to traversing a vertical section at  $k = 0.1$  through [figure 5\(b\)](#). Waves are unstable within a band of relaxation times  $\mathcal{T}$  over this section, and [figure 11](#) shows the corresponding wave

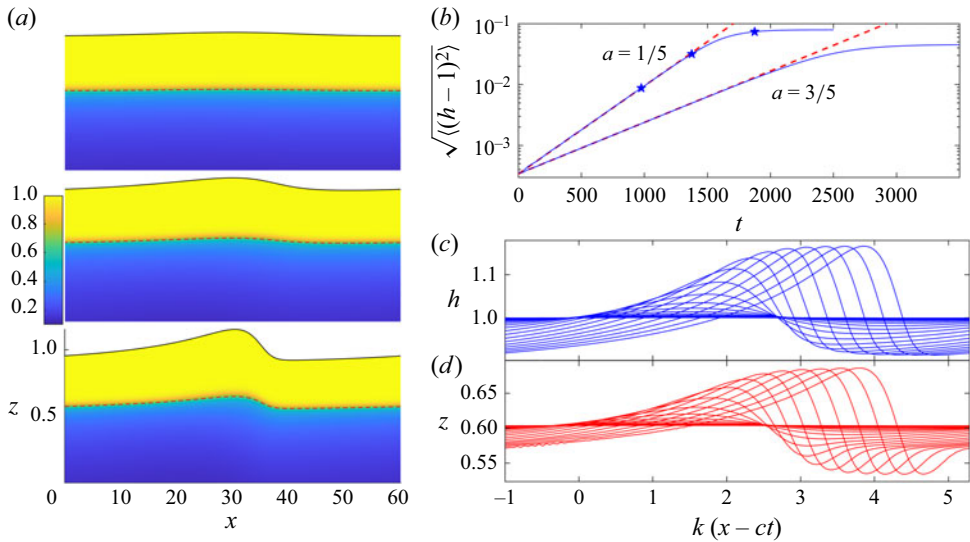


Figure 9. Numerical solution to (2.14), (2.15) and (2.19), for  $(a, \Gamma, \mathcal{T}, \kappa) = (1/5, 8, 10^2, 10^{-4})$  in a periodic domain of length  $20\pi$ . In (a), we present snapshots of the evolving profiles of  $h(x, t)$  and  $\lambda(x, z, t)$ . The times of the snapshots are indicated by the stars in (b), which plots the time series of  $\sqrt{\langle (h-1)^2 \rangle}$ ; the dashed line shows the expected linear growth. Also shown is another numerical solution with  $a = (3/5)$ . Snapshots of  $h$  and the level at which  $\lambda = (4/5)$  (dashed lines in (a)) are plotted in (c) and (d) for the first solution (with  $a = 1/5$ ), in the frame of linearly unstable wave (which travels at phase speed  $c$ ). The snapshots are spaced by 100 time units.

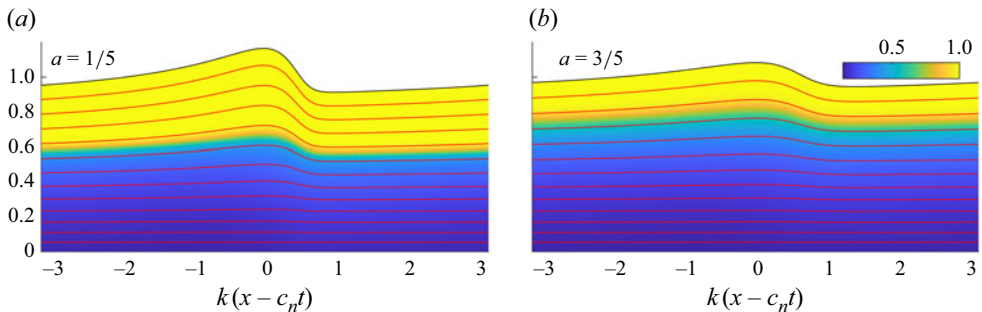


Figure 10. Final nonlinear wave solutions for (a)  $a = 1/5$  and (b)  $a = (3/5)$ , with  $(\Gamma, \mathcal{T}, \kappa, k) = (8, 10^2, 10^{-4}, 0.1)$ . Shown are density plots of  $\lambda(x, z, t)$ , with a superposed selection of streamlines (red lines, in the frame of the final wave, which has speed  $c_n$ ).

amplitudes for the final, saturated states. Those amplitudes decrease continuously to zero at the edges of the band, illustrating how the transition to instability is supercritical. The nonlinear waves travel at speeds that are a per cent or so higher than the linear phase speed  $c$  (also plotted in figure 11c), which in turn exceeds the mean flow speed  $U_* = 0.207$  by a factor of approximately three or more.

## 6. Discussion

This paper has focussed on the dynamics of instabilities in thin films of thixotropic fluid flowing down an inclined plane. A previously suggested interfacial instability (Hewitt & Balmforth 2013) has been confirmed to arise, and its details have been interrogated.



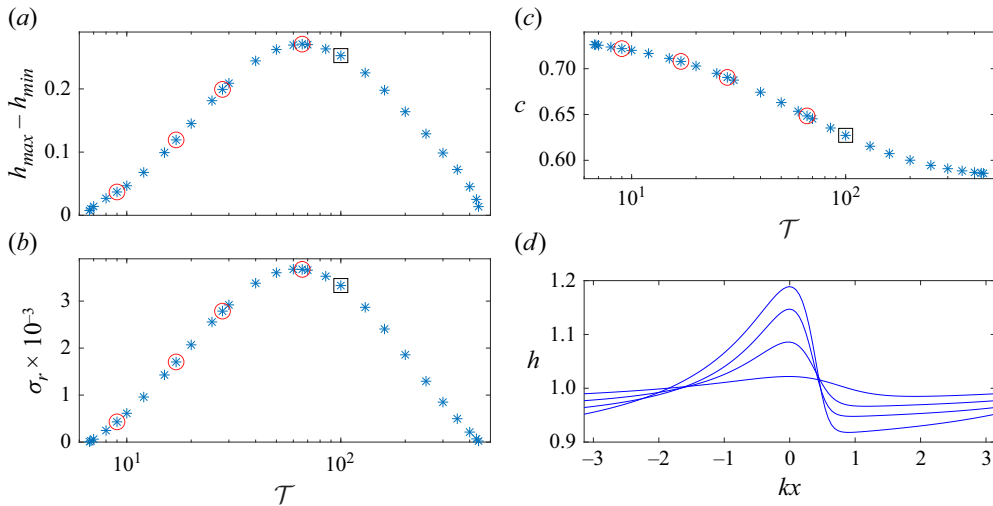


Figure 11. (a) Wave amplitudes  $(h_{\max} - h_{\min})$ , (b) linear growth rates  $\sigma_r$  and (c) phase speeds  $-\sigma_i/k$ , plotted against  $\tau$  for a suite of computations with  $(\Gamma, a, \kappa, k) = (8, 1/5, 10^{-4}, 0.1)$ . The wave profiles for the cases shown by (red) circles are plotted in (d) (shifted horizontally to align their maxima). The squares indicate the computation also shown in figures 9 and 10(a).

The instability has a long-wave character and is weak, in the sense that the time scale for growth is rather longer than that for propagation. However, instability arises over a wide choice of the settings of the problem parameters; only when the time scale for microstructural relaxation becomes relatively short is instability suppressed. The instability persists even when there are no viscosity bifurcations in the underlying rheological model, or when there is a relatively large vertical diffusion of the order parameter representing microstructure. Both results are surprising given that the discontinuous interface hypothesized by Hewitt & Balmforth (2013) to be key to instability is then completely absent. Instead, the phase lag introduced by the microstructural relaxation primarily drives instability (cf. Renardy & Renardy 2017; Castillo & Wilson 2020).

An exploration of the nonlinear dynamics (in spatially periodic domains) reveals that instability saturates into steadily propagating nonlinear waves that travel close to linear phase speeds and faster than the mean flow. The transition to instability is supercritical, with wave amplitudes reaching a fraction (20 % or so) of the fluid depth. Interactions and secondary instabilities of the nonlinear waves have not been explored.

One key ingredient of the current exploration is that it is based on a thin-film reduction of the original governing equations. In this reduction, the dominant resistance to fluid motion arises through shear stresses across the depth of the film; the extensional stresses in the film's plane are omitted from the force balance equations. One awkward consequence is that the two-layer structure of the flow becomes suspicious: the upper layer is assumed to be strongly structured and plug-like, yet is simultaneously able to deform within the plane of the film. This is permitted in the model by letting the viscosity become sufficiently large over the upper layer to render the flow profile plug-like, but not so large that the extensional stresses impact force balance (cf. Balmforth *et al.* 2003). This constraint translates to a thickness-dependent limit on the viscosity: in the dimensionless notation of § 2.2, the terms involving the extensional stresses appear at  $O(\varepsilon^2)$  in the thin-film limit. Therefore, as long as the viscosity  $\mu$  remains much smaller than  $\varepsilon^{-2}$ , there is no issue with neglecting those stresses.



Nevertheless, a more careful approach would be to solve the full, Orr–Sommerfeld-like stability problem, relaxing the thin-film approximation whilst simultaneously including a finite Reynolds number. This extension would permit one to identify precisely how the extensional stresses eventually rigidify the upper layer and arrest any deformation of the free surface, whilst gauging the impact of inertia.

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## Appendix A. Instantaneous, non-diffusive adjustment

Hewitt & Balmforth (2013) consider a (rather drastic) simplification of the thixotropic model of § 2.3 in which there is no diffusion ( $\kappa = 0$ ) and the fluid adjusts instantaneously to the steady-shear flow curve ( $\mathcal{T} = 0$ ). Without diffusion, the two-layer structure of the base states, in which a superficial structured plug lies above a destructured shear layer (§ 3), continues to apply even when flow becomes unsteady. As long as the stress at the interface remains between the special values  $\tau_A$  and  $\tau_C$ , that division is imprinted by the initial state of the fluid and acts as a material surface. In addition, if the microstructure adjusts instantaneously to the flow dynamics ( $\mathcal{T} = 0$ ), the upper layer remains plug-like and fully structured whereas the lower layer lies along the flow curve, with

$$\lambda = \frac{1 - \sqrt{1 - 4(1-a)(\Gamma\tau)^{-1}}}{2(1-a)}, \quad \tau = (1 - h_x)(h - z). \quad (\text{A1})$$

The thin-film model now devolves to two mass conservation equations; one for the whole film and one for the destructured layer,

$$\frac{\partial h}{\partial t} + \frac{\partial}{\partial x} F(h, h_x, Y) = 0, \quad \frac{\partial Y}{\partial t} + \frac{\partial}{\partial x} G(h, h_x, Y) = 0, \quad (\text{A2})$$

where the flux functions,

$$F(h, h_x, Y) = \int_0^h u \, dz = (1 - h_x) \int_0^Y (h - z)^2 (1 - \lambda) [(1 - \lambda)(1 - a) + a] \, dz, \quad (\text{A3})$$

and

$$G(h, h_x, Y) = \int_0^Y u \, dz = (1 - h_x) \int_0^Y (h - z) (Y - z) [(1 - \lambda)(1 - a) + a] \, dz, \quad (\text{A4})$$

with  $\lambda$  given by (A1), can be evaluated analytically although the explicit formulae are convoluted and not very informative.

Equations (A2) have the uniform equilibrium solution  $h = 1$  and  $Y = Y_0$ , with  $0 < Y_0 < 1 - 4\Gamma^{-1}(1 - a)$  (ensuring  $\tau_C < \tau(z = Y) < \tau_A$ ). Normal-mode perturbations to this base state of the form  $(h, Y) = (1, Y_0) + (\check{h}, \check{Y})e^{\sigma t + i k x}$ , with wavenumber  $k$  and growth rate  $\sigma$ , satisfy a quadratic dispersion relation. It follows from this relation that the uniform flow is either stable, or one of the modes is unstable over all wavenumbers, with a growth rate that increases monotonically with  $k$  and converges to a constant for  $k \rightarrow \infty$  (see Hewitt & Balmforth 2013).

Typical solutions of the dispersion relation are shown in figure 12. For the parameter settings chosen,  $(a, \Gamma) = ((1/5), 5)$ , all of the possible choices for the interface position

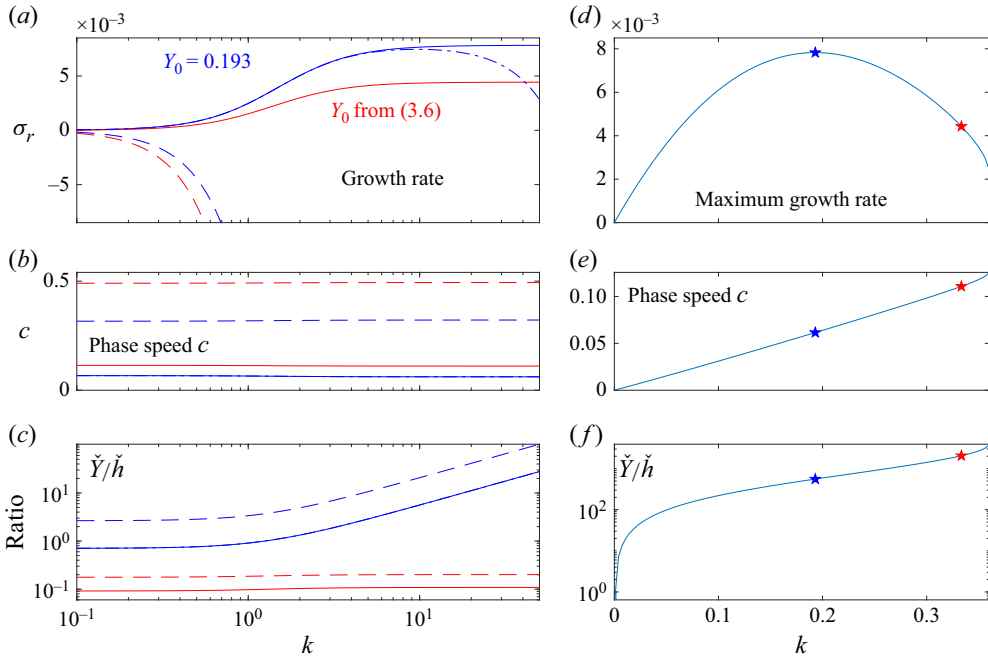


Figure 12. (a) Growth rate  $\sigma_r = \text{Re}(\sigma)$ , (b) phase speed  $c$  and (c) amplitude ratio  $\check{Y}/\check{h}$  for  $Y_0 = 0.193$  (blue) and (3.6) (red), with  $(a, \Gamma) = (1/5, 5)$ . The unstable (stable) modes are plotted by the solid (dashed) lines. Panels (d)–(e) show corresponding plots for the unstable mode, with  $k = 10^3$  and varying  $Y_0$ ; the stars indicate the two cases in (a) and (b). The dash–dot line in (a) indicates how the growth rates are modified when linear diffusion terms are added to equations (A2), with a diffusivity of  $2 \times 10^{-6}$ .

$Y_0$  lead to instability. The choice  $Y \approx 0.193$  is most unstable; the base flow selected by diffusion, with  $Y$  given by (3.6), is slightly less unstable. As highlighted by the amplitude ratios  $\check{Y}/\check{h}$  also plotted, the unstable mode perturbs  $Y$  more strongly than  $h$ . In other words, the mode has an interfacial character. By contrast, the damped mode has a relatively strong surface signature.

The system (A2) can be solved numerically with periodic boundary conditions to explore the nonlinear dynamics of the interfacial instability, starting from a small perturbation to the uniform base flow. To ease this task, we add linear diffusion terms to both equations in (A2) (with equal diffusivities of  $2 \times 10^{-6}$ ). These diffusion terms control the linear instability and ensure that the nonlinear solutions remain smooth. As illustrated figure 12(a), for  $(\Gamma, a, Y_0) = (5, 1/5, 0.193)$ , a broad, but finite, band of unstable modes then arises, with maximum growth for  $k \approx 10$ .

Figure 13 displays the results of such initial-value computations, starting with two different initial conditions, in domains of length  $2\pi/5$ . In the first example, the initial condition is given by  $(h, Y) = (1, Y_0 + 10^{-4} \sin 10x)$ , where  $Y_0 = 0.193$ . For the second example, the initial perturbation to the interface  $z = Y_0$  corresponds to a random superposition of the first 10 Fourier modes, with mean amplitudes of  $10^{-4}$ .

For the case initialized with a  $k = 10$  perturbation, the unstable mode develops as predicted by linear theory. In the nonlinear regime, the instability saturates to form two nonlinear, shock-like waves. The second solution displays a richer dynamics: the initial condition seeds the growth of five waves. On reaching finite amplitude, these waves interact, leading to a sequence of coarsening events, somewhat like that seen for roll waves in inertial viscous films (Balmforth & Mandre 2004). Eventually, a single wave remains.

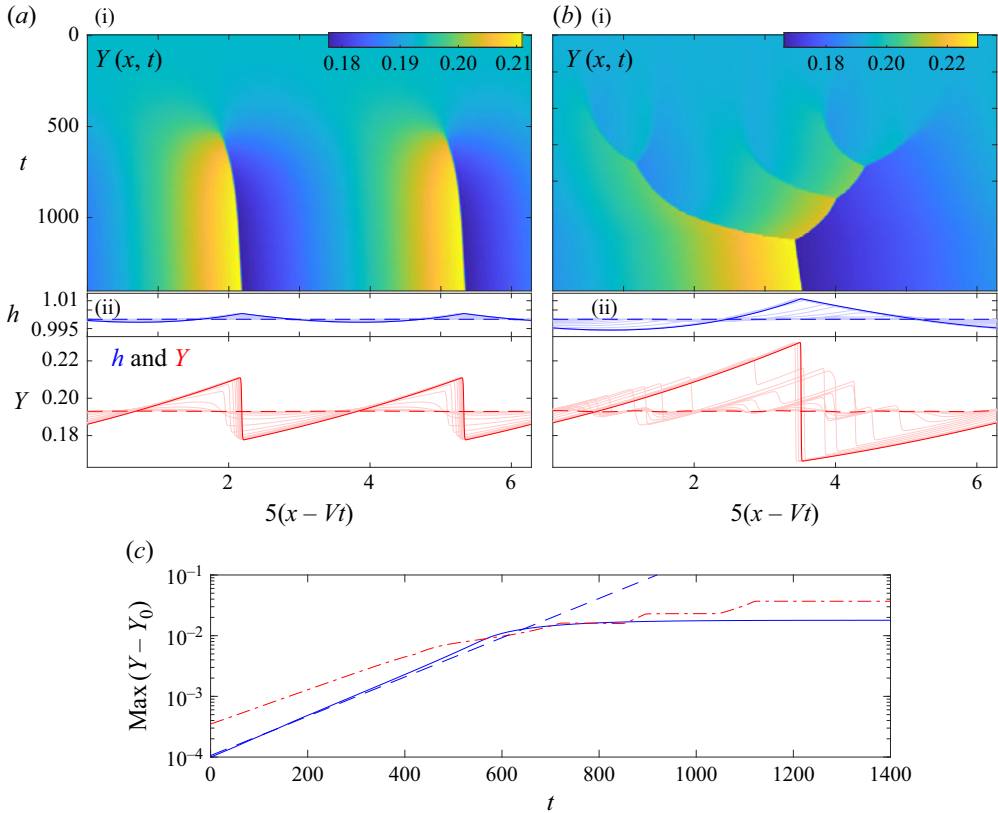


Figure 13. Nonlinear computations with (A2), including linear diffusion terms with equal diffusivities of  $2 \times 10^{-6}$ . The periodic domain has length  $2\pi/5$ ;  $(\Gamma, a) = (5, 1/5)$  and  $Y_0 = 0.193$ . Panels (a i) and (b i) show density plots of  $Y(x, t)$ ; panels (a ii) and (b ii) are plots of the initial (dashed) and final (solid) profiles of  $h$  (blue) and  $Y$  (red); the lighter lines show intermediate snapshots (every 100 time units). In each plot, the solution is shown in a frame translating close to that of the final nonlinear waves. In (a), the initial perturbation to  $Y = Y_0$  is  $10^{-4} \sin 10x$ ; for (b), that perturbation is a random superposition of the first ten Fourier modes, with mean amplitudes of  $10^{-4}$ . Panel (c) displays  $\text{Max}(Y - Y_0)$  against time (solid blue line for the solution in (a); dot-dash red line for that in (b)). The dashed line shows the growth expected for the linear  $k = 10$  mode.

Note that there is an awkward issue hidden in this reduced model: the upper layer is assumed to be fully structured, but it is also able to deform along the plane of the film, despite the implied infinite viscosity. This issue reflects an assumption inherent in the thin-film model, as discussed at the end of § 6 and Appendix D, and can be rationalized in the same manner as the pseudoplug of thin films of yield-stress fluids (Walton & Bittleston 1991; Balmforth & Craster 1999).

## Appendix B. Small $k$

After differentiating the base-state equations (3.1) in  $z$ , and some algebraic manipulations, the linear stability equations can be recast in the form

$$\begin{aligned} (\psi + \check{\eta}U)_{zz} &= -ik(1-z)A\check{\eta} + (1-z)A'(\check{\lambda} + \check{\eta}\Lambda_z), \\ \mathcal{T}[(\sigma + ikU)\check{\lambda} - ik\Lambda_z\psi] &= -(1 + \Gamma U_z)(\check{\lambda} + \check{\eta}\Lambda_z) - \Gamma A(\psi + \check{\eta}U)_{zz} + \kappa(\check{\lambda} + \check{\eta}\Lambda_z)_{zz}, \end{aligned} \quad (\text{B1})$$

where  $A = A(\Lambda)$  and  $A' = A'(\Lambda)$  are evaluated for the base state. In the limit  $k \ll 1$ , we may then introduce the sequences

$$\sigma = k\sigma_1 + k^2\sigma_2 + \dots, \quad \psi = \psi_0 + k\psi_1 + \dots, \quad \check{\lambda} = \check{\lambda}_0 + k\check{\lambda}_1 + \dots \quad (\text{B2})$$

to find a long-wave solution in which we select a normalization that fixes  $\check{\eta}$ . Here, we adopt  $\check{\eta} = 1$ .

When  $\kappa$  is small, the fact that  $\check{\lambda}(z)$  and  $\Lambda_z(z)$  satisfy different conditions at  $z = 0$  is not significant. The leading-order solution is then

$$\sigma_1 = -iU_z(0), \quad \check{\lambda}_0 = -\Lambda_z, \quad \psi_0 = -[U - zU_z(0)]. \quad (\text{B3})$$

At the following order of  $k$ , we then have

$$\begin{aligned} \psi_{1zz} &= -i(1-z)A + (1-z)A'\check{\lambda}_1, \\ i\mathcal{T}(1-z)U_z(0)\Lambda_z &= -(1+\Gamma U_z)\check{\lambda}_1 - \Gamma\Lambda\psi_{1zz} + \kappa\check{\lambda}_{1zz}, \end{aligned} \quad (\text{B4})$$

with boundary conditions

$$\sigma_2 = -i\psi_1(1), \quad \psi_1(0) = \psi_{1z}(0) = \check{\lambda}_{1z}(0) = \check{\lambda}_{1z}(1) = 0. \quad (\text{B5})$$

The growth is therefore determined at  $O(k^2)$ , and contains two contributions when  $\kappa \ll 1$  and  $a < 1/2$  (parameter settings we focus on here). The first contribution is from the destructured layer in  $0 < z < Y$ : here, we omit the diffusion term in (B4) and solve algebraically for  $\psi_{1zz}$ . Then,

$$\sigma_2^{(D)} \sim -i \int_0^Y (1-z)\psi_{1zz} dz = - \int_0^Y \frac{\mathcal{T}U_z(0)(1-z)A'\Lambda\Lambda_z + A}{1+\Gamma(1-z)A'\Lambda^2} (1-z)^2 dz, \quad (\text{B6})$$

in which  $\Lambda \sim \Lambda_a$  from (3.4). Note that  $A' < 0$  but  $1+\Gamma(1-z)A'\Lambda^2 > 0$ . Hence,  $\sigma_2^{(D)}$  contains two contributions: the first is proportional to  $\mathcal{T}$  and positive; the second is negative. In other words, over the lower-lying destructured layer, quasisteady viscous effects are stabilizing, but relaxation is destabilizing.

The second contribution arises from adjustments over the thin transition region around  $z = Y$ . If we again introduce the inner coordinate  $\zeta = (z - Y)/\sqrt{\kappa}$  to resolve this region, then we observe that

$$\mathcal{L}\check{\lambda}_1 \sim i\kappa^{-\frac{1}{2}}\mathcal{T}(1-Y)U_z(0)\Lambda_\zeta + O(1), \quad (\text{B7})$$

where

$$\mathcal{L} = \frac{\partial^2}{\partial \zeta^2} - 1 - \Gamma(1-z)(A + A'\Lambda). \quad (\text{B8})$$

But (3.1) implies that

$$\mathcal{L}\Lambda_\zeta = -\sqrt{\kappa}\Gamma\Lambda A. \quad (\text{B9})$$

Hence, on multiplying (B7) by  $\Lambda_\zeta$  and integrating over the transition region, we find

$$i\kappa^{-\frac{1}{2}}\mathcal{T}(1-Y)U_z(0) \int_{-\infty}^{\infty} \Lambda_\zeta^2 d\zeta + O(1) \sim -\sqrt{\kappa}\Gamma \int_{-\infty}^{\infty} \Lambda\Lambda\check{\lambda}_1 d\zeta, \quad (\text{B10})$$

given the matching conditions for  $\zeta \rightarrow \pm\infty$  (which indicate that  $\Lambda$  and  $\check{\lambda}_1$  and their derivatives in  $z$  are all order one). The balance in (B10) demands that  $\check{\lambda}_1 = O(\kappa^{-1})$  over the transition region. Given (B9) and (B7), the solution for  $\check{\lambda}_1$  must therefore be some

multiple of  $\Lambda_\zeta$  at leading order:  $\check{\lambda}_1 \sim -i\alpha\Lambda_\zeta$ . Equation (B10) then implies that

$$\alpha \sim \frac{\mathcal{T}(1-Y)U_z(0) \int_{-\infty}^{\infty} \Lambda_\zeta^2 d\zeta}{\kappa \Gamma \int_{-\infty}^{\infty} A\Lambda\Lambda_\zeta d\zeta}. \quad (\text{B11})$$

Moreover, from the first relation in (B4),

$$\psi_{1\zeta\zeta} \sim \alpha\kappa(1-Y)A'\Lambda_\zeta, \quad (\text{B12})$$

and so the transition region makes a contribution to the growth rate of

$$\sigma_2^{(J)} \sim -i(1-Y) \int_{-\infty}^{\infty} \psi_{1\zeta\zeta} \frac{d\zeta}{\sqrt{\kappa}} \sim \sqrt{\kappa}\alpha(1-Y)^2 A(Y^-), \quad (\text{B13})$$

where  $A(Y^-)$  denotes the reciprocal viscosity function evaluated as  $z \rightarrow Y$  from below. Note that  $\sigma_2^{(J)}$  is positive and always contributes towards instability. Moreover,  $\check{\lambda}_1 \sim -i\alpha\Lambda_\zeta$  represents a vertical shift of the transition layer due to the translation of wave-like perturbations with speed  $-\text{Im}(\sigma_1) = U_z(0)$ . In other words, the motion of the transition region is destabilizing.

### Appendix C. Fast relaxation with small diffusion

When  $\mathcal{T} \rightarrow 0$ , the structure function satisfies

$$\kappa\lambda_{zz} = (1-\lambda)\{\Gamma\tau(1-\Lambda)[(1-\Lambda)(1-a)+a]-1\}. \quad (\text{C1})$$

In the further limit  $\kappa \ll 1$ , we then arrive at the structure function,

$$\lambda = \begin{cases} \Lambda_a, & 0 < z < Y, \\ 1, & Y < z < h, \end{cases} \quad (\text{C2})$$

where

$$\Lambda_a(\tau) = \frac{1}{2(1-a)} \left[ 1 - \sqrt{1 - \frac{4(1-a)}{\Gamma\tau}} \right], \quad Y = h - \frac{9(1-a)}{\Gamma(1-h_x)(2-a)(1+a)}, \quad (\text{C3})$$

which corresponds to a generalization of the solution to (3.2)–(3.6), but applying for the full nonlinear dynamics of the film. Armed with this profile, we may compute the flux

$$\int_0^h (h-z)\dot{\gamma} dz = \frac{h^2}{\tau_b^2} \int_{\tau_y}^{\tau_b} \hat{\tau}^2 \mathcal{A}(\hat{\tau}) d\hat{\tau} = h^2 G(\tau_b), \quad (\text{C4})$$

where  $\tau_b = h(1-h_x)$  is the basal shear stress,

$$\tau_y = (h-Y)(1-h_x) = \frac{9(1-a)}{\Gamma(2-a)(1+a)}, \quad (\text{C5})$$

and  $\mathcal{A}(\tau) = (1-\Lambda_a)[(1-\Lambda_a)(1+a)+a]$  is the reciprocal of the viscosity function, rewritten as a function of  $\tau$  using (C3). Introducing this flux into the evolution equation  $h_t + Q_x = 0$ , gives the nonlinear diffusion problem,

$$h_t + [h^2 G(\tau_b)]_x = 0. \quad (\text{C6})$$

Linear stability is dictated by the dispersion relation,

$$\sigma = -ik[2G(1) + G'(1)] - k^2 G'(1). \quad (\text{C7})$$

But

$$G'(1) \equiv \tau_Y^2 \Gamma(\tau_Y) + \int_{\tau_Y}^1 \tau^2 \Gamma'(\tau) d\tau, \quad (\text{C8})$$

where  $\Gamma(\tau) \equiv \tau \mathcal{A}(\tau)$  denotes the inverse of the ascending (right-hand) branch of the flow curve in (2.22). Thus, as  $\tau_Y^2 \Gamma(\tau_Y) \equiv \tau_c^2 \dot{\gamma}_c > 0$  and  $\Gamma'(\tau) > 0$ , we conclude  $G'(1) > 0$ . The film is therefore stable in this limit. Note that the situation may be different if the base state were to contain sections of the descending (left-hand) branch of the flow curve.

#### Appendix D. Vanishing diffusion

When  $\kappa \rightarrow 0$  and there is a viscosity bifurcation ( $a < 1/2$ ), the interface  $z = Y(x, t)$  evolves as a material surface. Mass conservation over the plug-like structured layer then demands that

$$(h - Y)_t + [(h - Y)u_p]_x = 0, \quad (\text{D1})$$

where  $u_p \equiv u(x, Y, t)$  is the plug speed.

The base states arising in the  $\kappa \rightarrow 0$  limit of the diffusive problem have interface positions given by (3.6), and flow profiles following the flow curve. Base states are given by  $(u, \lambda, h, Y) = (U, \Lambda, 1, Y_0)$ . With  $\kappa \rightarrow 0$ , the linearized structure function equation (4.2) simplifies, reducing to an algebraic relation for  $\check{\lambda}$ . One must then integrate only the stream function equation to solve the linear problem over  $0 < z < Y_0$ . The overlying plug-like flow can be taken into account by applying a boundary condition at  $z = Y_0$ : a linearization of (D1) indicates

$$\check{Y} = \check{\eta} + \frac{ik(1 - Y_0)\check{u}_p}{\sigma + ikU_p}, \quad (\text{D2})$$

whereas the continuity of the velocity at  $z = Y$  indicates that

$$\check{u}_p = \psi_z(Y_0) + U_z(Y_0)\check{Y}. \quad (\text{D3})$$

Rewriting the kinematic condition at the free surface as

$$(\sigma + ikU_p)\check{\eta} = -ik\psi(1) = -ik[\psi(Y_0) + (1 - Y_0)\check{u}_p], \quad (\text{D4})$$

and then eliminating  $\check{Y}$  and  $\check{u}_p$  from (D2)–(D4) furnishes the condition needed at  $z = Y_0$ .

Note that the plug-like layer is again able to deform in this limit, despite its apparently fully structured state. Once more, this reflects the omission of the extensional stresses from the shallow-film model. Therefore, even though  $\kappa \ll 1$ , diffusion is assumed sufficient to prevent  $\lambda$  from truly reaching unity. The viscosity function is thereby prevented from diverging, and simply becomes sufficiently large to suppress vertical shear, but not horizontal extension. In other words, the limit implicitly assumes that  $\varepsilon^2 \mu(\Lambda) \ll 1$  (given that the extensional stresses impact the force balance equations at  $O(\varepsilon^2)$ ).

#### Appendix E. Strong diffusion

In the limit  $\kappa \gg 1$ , the structure function becomes locally uniform across the film:  $\lambda \sim \bar{\lambda}(x, t)$ . The velocity profile is then parabolic and a reduction of the thin-film model follows after integrating the dimensionless structure–function equation in (2.19) over the

film thickness,

$$h_t + (hU)_x = 0, \quad (\text{E1})$$

$$\mathcal{T}(\bar{\lambda}_t + U\bar{\lambda}_x) = 1 - \bar{\lambda} - \frac{3\Gamma U\bar{\lambda}}{2h}, \quad (\text{E2})$$

$$U \equiv \frac{1}{h} \int_0^h (h-z)u_z \, dz = \frac{1}{3}h^2(1-h_x)A(\bar{\lambda}). \quad (\text{E3})$$

Base states exist for  $\Gamma > 8(1-a)$  and are given by

$$h = 1, \quad \bar{\lambda} = \Lambda = \frac{1 - \sqrt{1 - 8\Gamma^{-1}(1-a)}}{2(1-a)}, \quad U = U_* = \frac{1}{3}A(\Lambda), \quad (\text{E4})$$

corresponding to a point on the right-hand branch of the flow curve, with shear rate  $U_*$  and unit shear stress. Linear perturbations with growth rate  $\sigma$  and wavenumber  $k$  have the dispersion relation,

$$\left[ \mathcal{T}(\sigma + ikU_*) + 1 + \frac{3\Gamma}{2}(U_* + \Lambda U_\lambda) \right] \left[ \sigma + ik(3-ik)U_* \right] - \frac{3}{2}ik(1-ik)\Gamma\Lambda U_* U_\lambda = 0, \quad (\text{E5})$$

with

$$U_\lambda = \frac{1}{3}A'(\Lambda) = -\frac{1}{3}[2(1-\Lambda)(1-a) + a]. \quad (\text{E6})$$

Solutions to this dispersion relation are illustrated in [figure 14](#). Flow is again unstable for sufficiently long relaxation time, and the stability characteristics are similar to those found for finite  $\kappa$ .

For long waves, the dispersion relation simplifies further: we find  $\sigma \sim -ikc + \sigma_2 k^2$ , where

$$c = 3U_* \left[ 1 - \frac{\Gamma\Lambda U_\lambda}{2 + 3\Gamma(U_* + \Lambda U_\lambda)} \right], \quad \sigma_2 = \frac{2\mathcal{T}(c - U_*)(c - 3U_*) - U_*(2 + 3\Gamma U_*)}{2 + 3\Gamma(U_* + \Lambda U_\lambda)}. \quad (\text{E7})$$

The  $O(k^2)$  growth rate again exposes the destabilizing effect of relaxation ( $c < 3U_*$  and  $2 + 3\Gamma(U_* + \Lambda U_\lambda) > 0$ ) and the stabilization of quasisteady viscous effects.

As shown in [figure 15](#), nonlinear solutions to (E3) in periodic spatial domains initially demonstrate the growth predicted by (E5), but then saturate into steady nonlinear waves. The initial condition used here seeds the growth of the most unstable linear mode (with  $k = 0.2$ ; see [figure 15a](#)). The nonlinear waves that emerge, as illustrated in [figure 15\(b,c\)](#), display destructuring underneath the rise of the wave crests, and structural recovery over the fall to the following trough. These nonlinear waves appear in a supercritical bifurcation as  $a$  is lowered through the stability threshold.

## Appendix F. Details of the numerical scheme used to compute nonlinear solutions

We first map the fluid domain to a rectangle by transforming to the new spatial variables  $(x, \zeta)$ , where  $\zeta = z/h(x, t)$ . After discretizing the new variables, spatial derivatives are evaluated using spectral differentiation matrices (supplementing Chebyshev matrices for  $\partial/\partial\zeta$  with matrices for  $\partial/\partial x$  based on the fast Fourier transform (Weideman & Reddy 2000)). The discrete spatial grid in  $(x, \zeta)$  is then an  $N \times M$  collection of collocation points, where practically we take  $N = M = 128$  or more. The resulting set of



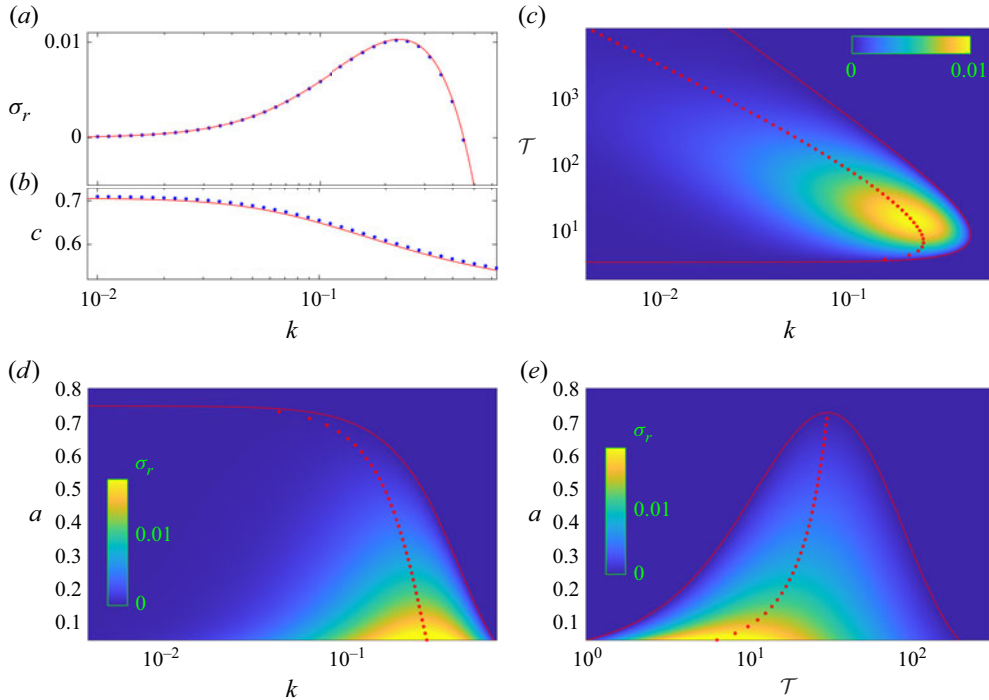


Figure 14. (a) Growth rates and (b) phase speeds as functions of  $k$  in the strong-diffusion limit for  $(a, \Gamma, T) = (1/5, 8, 14)$ . The (red) solid lines show the predictions of (E5), the (blue) points show numerical solutions of the full linear stability problem with  $\kappa = 10$ . The remaining panels show density plots of growth rate (from (E5)) over the (a)  $(k, T)$  ( $a = 1/5$ ), (b)  $(k, a)$  ( $T = 14$ ) and (c)  $(T, a)$  planes ( $k = 0.2$ ), all with  $\Gamma = 8$ . The (red) solid lines in (c), (d) and (e) show the stability boundaries and the dots show the maximum growth over all  $k$  or  $T$ .

coupled ordinary differential equations are solved using MATLAB's ODE15s. As initial conditions, we adopt  $h(x, 0) = 1 + A \sin kx$  and  $\lambda(x, \zeta, 0) = \Lambda(\zeta)$ , where  $A$  is typically chosen to be  $5 \times 10^{-4}$  and  $\Lambda(z)$  is one of the base-flow solutions of § 3.

To examine the effect of spatial resolution, solutions with different choices for  $N$  and  $M$  (but setting  $N = M$ ) were computed and compared. For the same two solutions of figure 9, the final amplitude of  $\sqrt{\langle (h - 1)^2 \rangle}$  changes by less than a per cent when halving or even quartering the number of grid points; the changes to the final nonlinear wave speed are smaller still.

Note that MATLAB's ODE15s uses preset relative and absolute error tolerances of  $10^{-3}$  and  $10^{-6}$ , respectively, by default. These were reset to  $10^{-5}$  and  $10^{-9}$  in order to provide additional assurance about the fidelity of the time integration. Nevertheless, the two solutions of figure 9 changed by less than a tenth of a per cent when recomputed with the original tolerances.

Figure 9(b) also compares the two nonlinear computations for  $N = M = 128$  with the predictions from linear theory; over the period of exponential growth, the computations match the linear predictions. In more detail, the growth rate extracted from the time series of the nonlinear solution agrees with the linear eigenvalue to better than a per cent. In summary, there was no evidence of any issue with spatial resolution or time integration error.

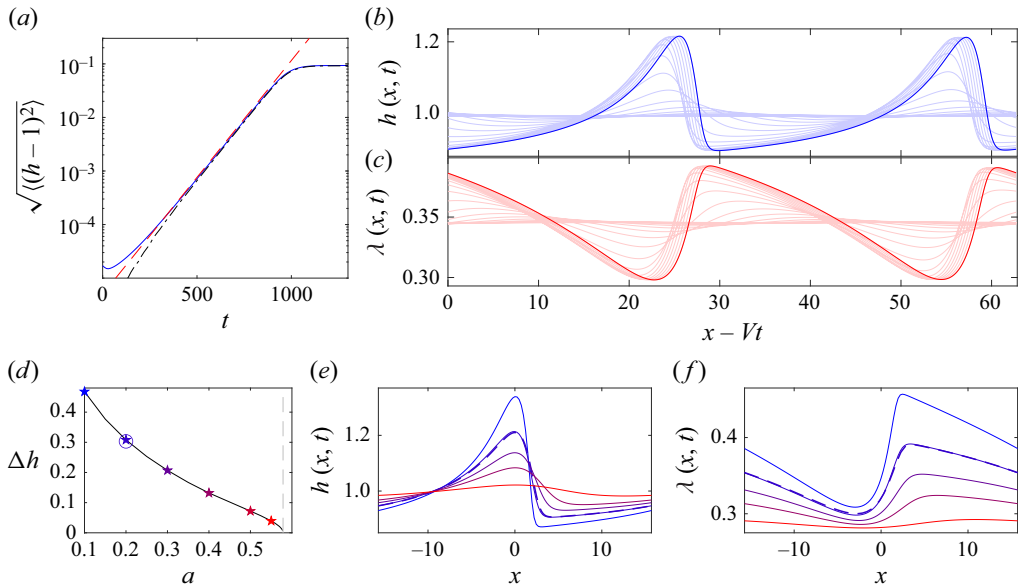


Figure 15. A strong-diffusion solution to (E3) in a periodic domain of length  $20\pi$ , with  $(a, \Gamma, \mathcal{T}) = (1/2, 8, 14)$ . The initial condition is a random superposition of the first 10 Fourier modes with mean amplitudes of  $10^{-5}$ . Shown are (a) a time series of  $\sqrt{(h-1)^2}$ , and snapshots of (b)  $h(x, t)$  and (c)  $\lambda(x, t)$  (every five time units, with the final profile shown darker). The dashed line in (a) indicates the growth expected for the most unstable mode (with  $k = 0.2$ ). The snapshots are shown in a moving frame with speed  $V = 0.64$ . The final wave profiles from a wider suite of computations with varying  $a$  are shown below, plotting (d) wave amplitude  $\Delta h \equiv h_{\max} - h_{\min}$  against  $a$ , and (e)  $h$  and (f)  $\lambda$  for the values of  $a$  indicated by the stars in (d). The grey dashed line shows the stability boundary in (d), and the profiles are shifted to align the wave crests (i.e.  $h_{\max}$ ) in (e) and (f). The dot-dash line in (a), circle in (d) and dashed lines in (e) and (f) show corresponding results from the full thin-film model, with  $\kappa = 10$  (plotting  $\langle \lambda \rangle$  in (f)); the most obvious differences arise during the initial transients.

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