

A one-dimensional model of the evolution of snow-cover characteristics

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ABSTRACT. A one-dimensional model has been developed to simulate the evolution of snow-cover characteristics using meteorological data. This model takes into account the heat balance at the snow surface and heat conduction in the snow cover as well as liquid water flow and densification. The basic variables of the model are snow temperature, liquid water content, snow density and the solid impurities density. With these four variables, the model can calculate albedo, thermal conductivity, liquid water flux, snow depth, water equivalent and the amount of runoff.

Diurnal variation of profiles of snow temperature, water content and snow density, and meteorological elements were observed at Mount Zao Bodaira, Yamagata Prefecture, Japan. Simulated diurnal variation patterns of each component by the model were in good agreement with the observations. Moreover, the snow-cover characteristics were simulated for three 90-day periods with meteorological data and snow pit observations at Sapporo. It was found that the model was able to simulate long-period variations of albedo, snow depth, snow water equivalent and the snow density profile.

INTRODUCTION

The characteristics and structures of snow change continually and influence albedo and thermal conductivity, which are important for climate. Snow-cover characteristics are strongly influenced by meteorological conditions. Therefore, we propose a one-dimensional model using meteorological data to simulate the snow-cover characteristics for the purpose of clarifying the heat balance and water cycle at the Earth's surface.

There were few all-round snow metamorphism models after a pioneer model developed by Anderson (1976). Recently, Brun and others (1989) proposed an energy and mass model for operational avalanche forecasting, and the model was advanced to take into account grain-size and type of snow (Brun and others, 1992). However, there are few models which can directly predict snow albedo including the effects of solid impurities and liquid water.

BASIC EQUATIONS

Figure 1 shows the schematic of the physical processes in the model in this paper. All of the physical variables in this model are described by snow temperature T_s , the

amount of liquid water ρ_{lw} , the dry snow density ρ_{dry} , and the solid impurities density ρ_D for albedo.

- Snow temperature T_s

For a snow surface

$$C_s \rho_{dry} \frac{dT_s}{dt} dz = \lambda_s \left. \frac{\partial T_s}{\partial z} \right|_{z=0} + (\mu I \exp(-\mu z) - l_f F) dz + \epsilon L^\downarrow - \epsilon \sigma T_{sfc}^4 - H - lE. \quad (1)$$

In a snow cover

$$C_s \rho_{dry} \frac{dT_s}{dt} = \frac{\partial}{\partial z} \left(\lambda_s \frac{\partial T_s}{\partial z} \right) + \mu I \exp(-\mu z) - l_f F. \quad (2)$$

C_s : specific heat of snow; λ_s : thermal conductivity of snow; l_f : latent heat of fusion of ice; F : amount of snowmelt per unit time and volume; $I = (1 - A_s) S^\downarrow$; A_s : albedo; S^\downarrow : solar radiation; μ : extinction coefficient of solar radiation; z : depth from the snow surface; L^\downarrow : downward atmospheric radiation; T_{sfc} : snow surface temperature; ϵ : emissivity of snow (= 0.97); σ : Stefan-Boltzmann constant; H : sensible heat flux; lE : latent heat flux.

- Amount of liquid water ρ_{lw}

$$\frac{d\rho_{lw}}{dt} = -\frac{\partial Q}{\partial z} + F. \quad (3)$$

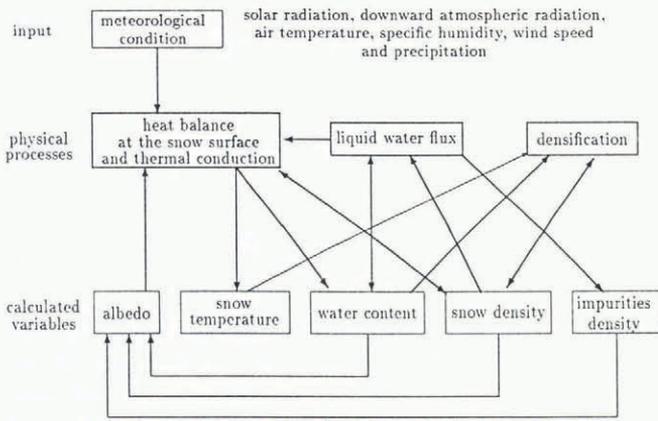


Fig. 1. Schematic of the relation between the physical processes and snow-cover characteristics in this model.

ρ_{lw} : mass of liquid water per unit volume; Q : downward liquid water flux (Colbeck, 1978; Shimizu, 1970).

- Dry snow density ρ_{dry}

$$\frac{d\rho_{dry}}{dt} = \frac{W_s}{\eta} \rho_{dry} - F. \tag{4}$$

W_s : load; η : compactive viscosity coefficient of snow.

- Solid impurities density ρ_D

$$\frac{d\rho_D}{dt} = -\frac{\partial}{\partial z} \left(f_D \frac{\rho_D}{\rho_{wet}} Q \right). \tag{5}$$

ρ_D : mass of solid impurities per unit volume of snow; f_D : rate of impurities flow; ρ_{wet} : wet snow density ($= \rho_{dry} + \rho_{lw}$).

In practice, Equations (1)–(5) are written in differential forms to calculate the profiles of the variables. (A simple version was described in the

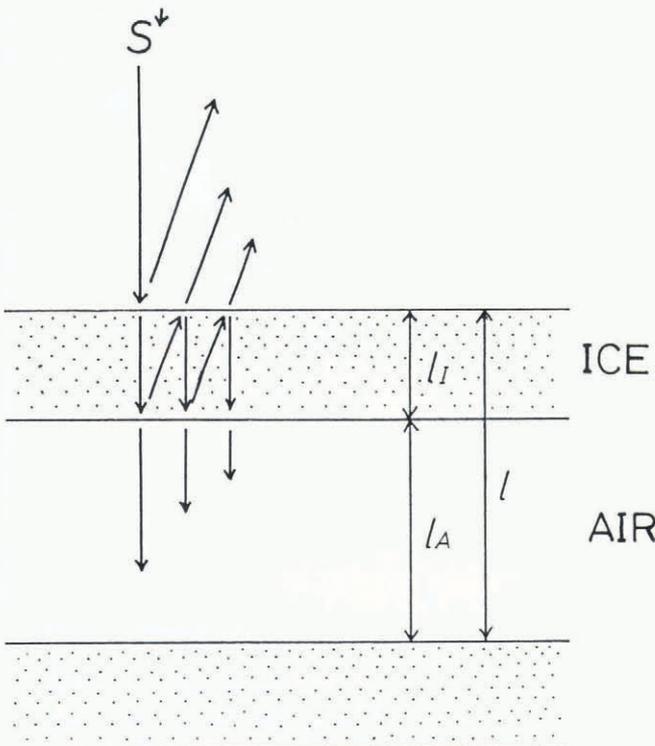


Fig. 2. Schematic of snow albedo submodel.

appendix in Kondo and Yamazaki (1990).) The input data are solar and downward radiation, air temperature, specific humidity, wind speed and precipitation. Snowfall and rainfall are distinguished by air temperature (2°C) in the model. The density of new snow is assumed to be 70 kg m^{-3} .

ALBEDO

The albedo of pure dry snow is obtained from profiles of dry snow density and the optical absorption coefficient of ice (Kondo and others, 1988). The multiple reflection is considered with an assumption that snow is constructed by ice plates and air layers (Fig. 2).

The albedo, A_s , is obtained by two-stream model as

$$A_s = r_1 + \frac{(1 - r_1)^2 (\beta_1 D_1 + \alpha_1)}{1 + D_1 - r_1 (\beta_1 D_1 + \alpha_1)}, \tag{6}$$

where

$$D_i = \frac{\left(\frac{\alpha_i - \beta_{i+1}}{\beta_{i+1} - \beta_i} D_{i+1} \exp(2i \Delta z \mu_{i+1}) + \alpha_i - \alpha_{i+1} \right)}{\left(\exp(2i \Delta z \mu_i) \right)} \quad (i = 1, \dots, n - 1),$$

$$D_n = 0,$$

$$\mu_i = \sqrt{A_i^2 - B_i^2},$$

$$\alpha_i = \frac{A_i - \mu_i}{B_i},$$

$$\beta_i = \frac{A_i + \mu_i}{B_i},$$

$$A_i = \frac{1 - T_{li} \rho_{dry,i}}{l_{li} \rho_I},$$

$$B_i = \frac{r_{li} \rho_{dry,i}}{l_{li} \rho_I},$$

$$R_{li} = r_1 + \frac{(1 - r_1)^2 r_{li} \exp(-2k_I l_{li})}{1 - (r_1 \exp(-k_I l_{li}))^2},$$

and

$$T_{li} = \frac{(1 - r_1)^2 \exp(-k_I l_{li})}{1 - (r_1 \exp(-k_I l_{li}))^2}.$$

Here, μ_i is the extinction coefficient of solar radiation in i -th snow layer, r_1 the reflectivity of ice ($= 0.018$), ρ_I the density of ice and k_I the absorption coefficient of ice (assumed to be 10 m^{-1}). The thickness of an ice layer l_{li} is obtained as

$$l_{li} = \frac{2}{\rho_I S_i^*}, \tag{7}$$

$$\log_{10} S_i^* = -15.32 \rho_{dry,i}^3 + 16.65 \rho_{dry,i}^2 - 7.30 \rho_{dry,i} + 2.23, \tag{8}$$

where S_i^* is the specific surface area (the area of the surface of the ice particles in unit volume of snow) in i -th snow layer. The units of $\rho_{dry,i}$ and S_i^* are g cm^{-3} and m^2kg^{-1} , respectively. Equation (8) is an experimental equation based on the data in Narita (1971).

In the model, it is considered that albedo is decreased by the impurities and liquid water content in snow. As the density of the impurities increases, optical absorption coefficient increases. The increase of effective absorption coefficient due to impurities, k_D , is assumed to be equal to the cross-section of the impurities per unit volume of ice. Based on a few assumptions for characteristics of impurities, the following equation can be obtained:

$$k_D \approx 46\rho_D \frac{\rho_I}{\rho_{wet}} \quad (9)$$

The units of k_D and ρ_D are m^{-1} and kg m^{-3} , respectively. The amount of aerosol fallout is given by $(3.14 \times 10^{-8})\beta$ ($\text{kg m}^{-2}\text{s}^{-1}$), which is obtained from an assumption of the aerosol-size distribution, where β is the atmospheric turbidity defined by Yamamoto and others (1968).

The effect of liquid water on albedo is described through a decrease in the specific surface area. That is

$$S^* = S^*(\rho_{wet}) \cdot f(w), \quad (10)$$

where

$$f(w) = 1 - \gamma w + (\gamma - 1)w^2. \quad (11)$$

w is water content ($= \rho_w/\rho_{wet}$) and $\gamma = 1.9$ (Yamazaki and others, 1991). The value of $S^*(\rho_{wet})$ is obtained from Equation (8) using ρ_{wet} instead of ρ_{dry} .

SENSIBLE AND LATENT HEAT FLUX

Sensible heat H and latent heat lE are written as

$$H = C_P \rho C_H U (T_{sfc} - T_a) \quad (12)$$

and

$$lE = l\rho C_E U (q_{sat}(T_{sfc}) - q_a). \quad (13)$$

Here, C_P and ρ are specific heat at constant pressure and density of air, respectively, and U , T_a and q_a are wind speed, air temperature and specific humidity, respectively. The value $q_{sat}(T_{sfc})$ is the saturated specific humidity at surface temperature T_{sfc} . Bulk coefficients C_H and C_E are set at 0.002 and 0.0021 at a reference height of 1 m, respectively (Kondo and Yamazawa, 1986).

THERMAL CONDUCTIVITY

The thermal conductivity is parameterized using porosity P ($= 1 - \rho_{dry}/\rho_I$) as follows.

$$\lambda_s = P\lambda_a + (1 - P)\lambda_b, \quad (14)$$

where λ_a is the thermal conductivity of the transverse structure piled by ice plates and air layers same as Figure 1 (the smallest theoretical conductivity), and λ_b is that of the longitudinal structure (the largest theoretical conductivity). They are written as

$$\lambda_a = \frac{1}{P/\lambda'_A + (1 - P)/\lambda_I} \quad (15)$$

and

$$\lambda_b = P\lambda'_A + (1 - P)\lambda_I, \quad (16)$$

where

$$\lambda'_A = \lambda_A + LD_v \frac{dC}{dT}. \quad (17)$$

Here, λ_I is the thermal conductivity of ice ($2.2 \text{ W m}^{-1}\text{K}^{-1}$), λ_A the thermal conductivity of air ($2.14 \times 10^{-2} \text{ W m}^{-1}\text{K}^{-1}$), λ'_A the effective thermal conductivity of air corrected for vapor diffusion, L the latent heat of sublimation of ice (2.83 MJ kg^{-1}), D_v the diffusion coefficient of water vapor ($6.5 \times 10^{-5} \text{ m}^2\text{s}^{-1}$) and C the saturated vapor density.

COMPACTIVE VISCOSITY

The compactive viscosity coefficient of wet snow is obtained from the equation for dry snow (Kojima, 1957; Shinojima, 1967) using a multiplicative factor which describes the decrease of the compactive viscosity coefficient due to liquid water. That is

$$\eta = A(w)\eta_0 \exp(K\rho_{dry} - \alpha_s T_s), \quad (18)$$

where $A(w)$ is assumed as

$$A(w) = \frac{\exp(-\beta_s w) - \exp(-\beta_s)}{1 - \exp(-\beta_s)}. \quad (19)$$

Here, η_0 ($6.9 \times 10^5 \text{ kg s m}^{-2}$), K ($2.1 \times 10^{-3} \text{ m}^3 \text{ kg}^{-1}$), α_s ($9.58 \times 10^{-2} \text{ }^\circ\text{C}^{-1}$) and β_s ($= 18$) are constants.

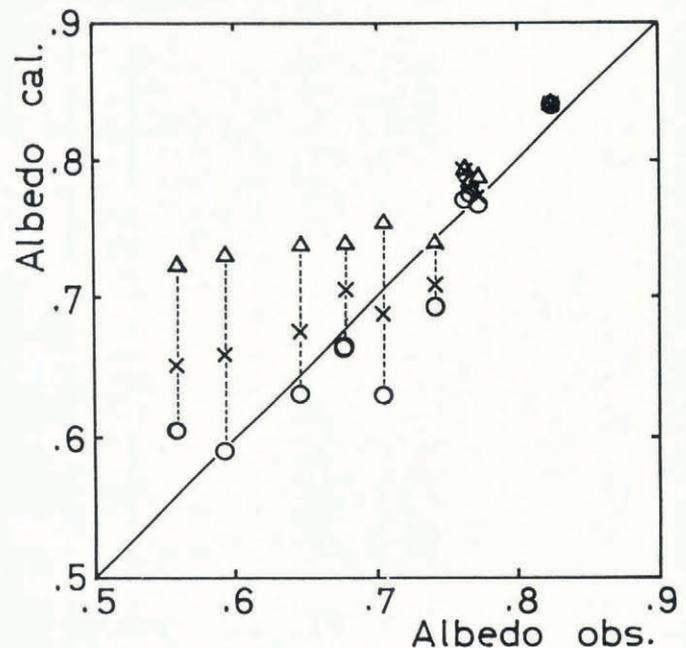


Fig. 3. Comparison of calculated and observed snow albedo at Zao Bodaira. Δ : effects of impurities or liquid water are not considered; \times : taking only impurities into account; \circ : effects of impurities and liquid water are considered.

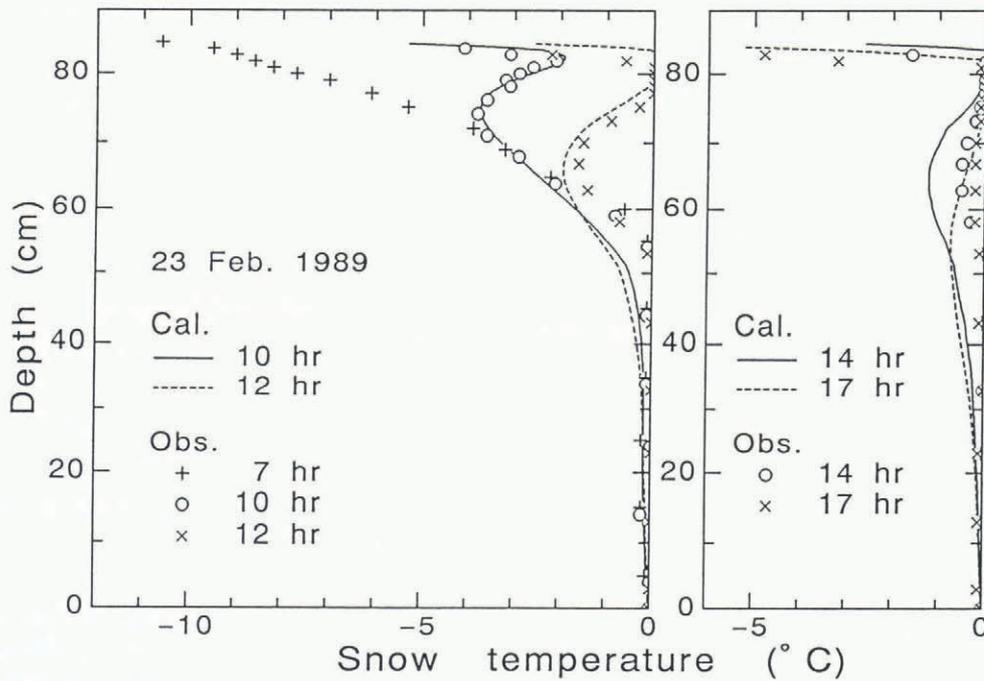


Fig. 4. An example of calculated and observed snow temperature profiles.

SHORT-PERIOD SIMULATION

Diurnal variation of profiles of temperature, water content and snow density were simulated for the following observation. The detail of the observation has been described in Yamazaki and others (1991).

Period: 23–28 February and 9–15 March 1989.

Place: Mount Zao Bodaira, Yamagata Prefecture, Japan (a flat soil tennis court).

Observations: air temperature, humidity, wind speed, solar radiation, albedo, snow depth, snow type, snow temperature, water content, density and solid impurities density.

Solid impurities density was measured using a method of light absorption (Kondo and others, 1988). The impurity particles are almost mineral. The range of measured absorption coefficients, k_D , in the top 5 cm of the snow cover is from 0.1 m^{-1} (26 February) to 9.8 m^{-1} (15 March). Figure 3 displays the values of observed and calculated albedo.

Figure 4 shows the simulated and observed snow temperature profiles for 23 February. The snow temperature was measured using a thermistor thermometer. The solar radiation was shut off with a board at the moment of measurement. The initial profiles of this simulation are given at 0700 h. Diurnal variation patterns of water content are also in agreement with the observations (figure not shown).

LONG-PERIOD SIMULATION

Period: 1986–1988 (3 winters).

Place: Sapporo, Hokkaido, Japan.

Data: Meteorological data and snow-pit observations at the Institute of Low Temperature Science, Hokkaido University (e.g. Endo and others, 1986; Ishikawa and

Motoyama, 1986) and meteorological data at Sapporo District Meteorological Observatory.

Figure 5 shows the time series of albedo in 1986. The values of important parameters are listed in Table 1. In this calculation it is assumed that the impurities do not flow out because the value of f_D is set to zero for the snowmelt season. However, the estimated albedo is smaller than the observations (Ishikawa and Motoyama, 1986) in the later period. The actual amount of aerosol fallout may be larger than the value which is used in this simulation. At the start of the season, the albedo is slightly underestimated. The reason for this is unclear, however, the observed values in this year are higher than usual.

In Figures 6 and 7 the calculated snow depth and snow water equivalent are compared with the observations (Ishikawa and Motoyama, 1986; Endo and others,

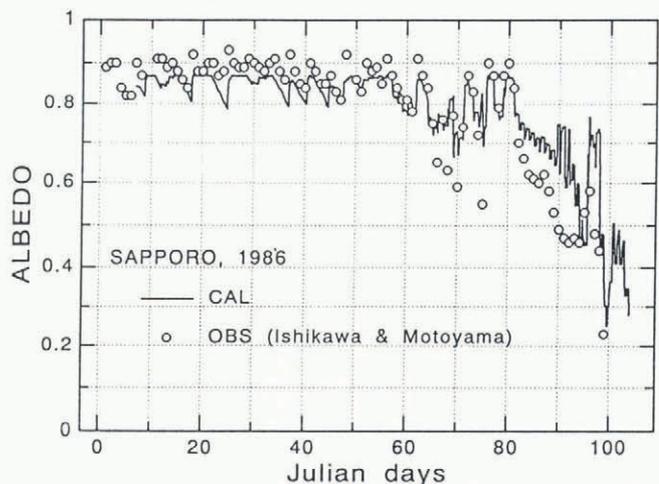


Fig. 5. Comparison of calculated and observed snow albedo for 1986. The observed values are averaged from 1100 to 1200 h (wave length: $0.29\text{--}3.0 \mu\text{m}$).

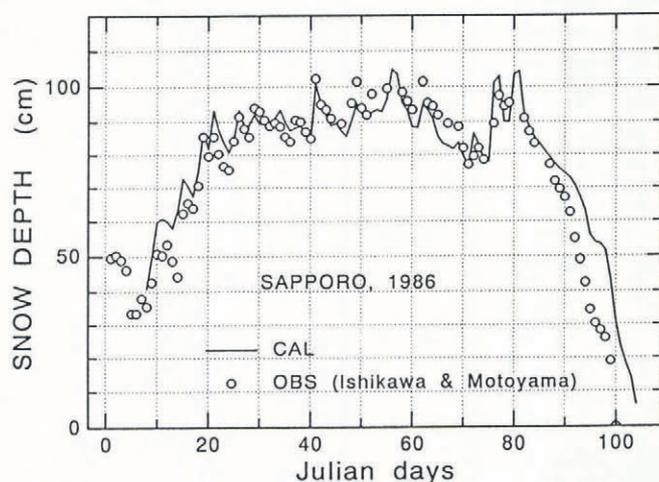


Fig. 6. Comparison of calculated and observed snow depth for 1986.

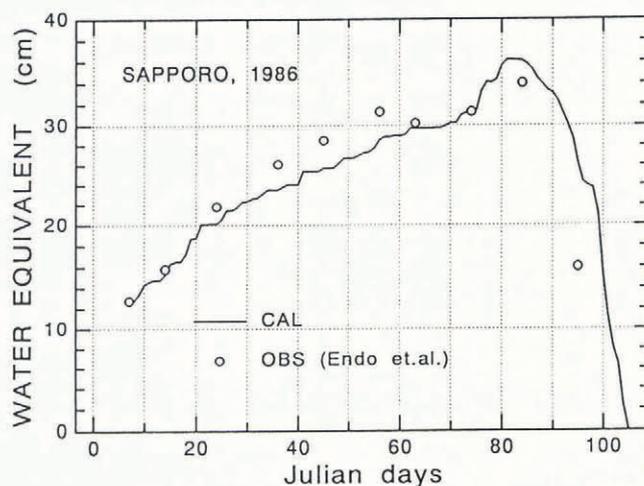


Fig. 7. Comparison of calculated and observed snow water equivalent for 1986.

Table 1. The list of the main parameters

parameter	eq. no.	value	
C_H	bulk coefficient (sensible)	(12)	0.002
C_E	bulk coefficient (latent)	(13)	0.0021
f_D	rate of impurities flow	(5)	0
k_I	absorption coefficient of ice	(6)	10 m^{-1}
β	atmospheric turbidity		0.1
μ	extinction coefficient	(1)	40 m^{-1}

1986). The calculated values are overestimated in snowmelt season, because the albedo is large.

CONCLUDING REMARKS

The evolution of snow-cover characteristics was simulated with a one-dimensional energy balance model. This model includes new parameterizations of the albedo, thermal conductivity and compactive viscosity. In particular, snow albedo was predicted taking into account the effects due to solid impurities and liquid water. The agreement between observed and calculated components was obtained for short- and long-period simulations. However, the handling of impurities requires much more study.

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